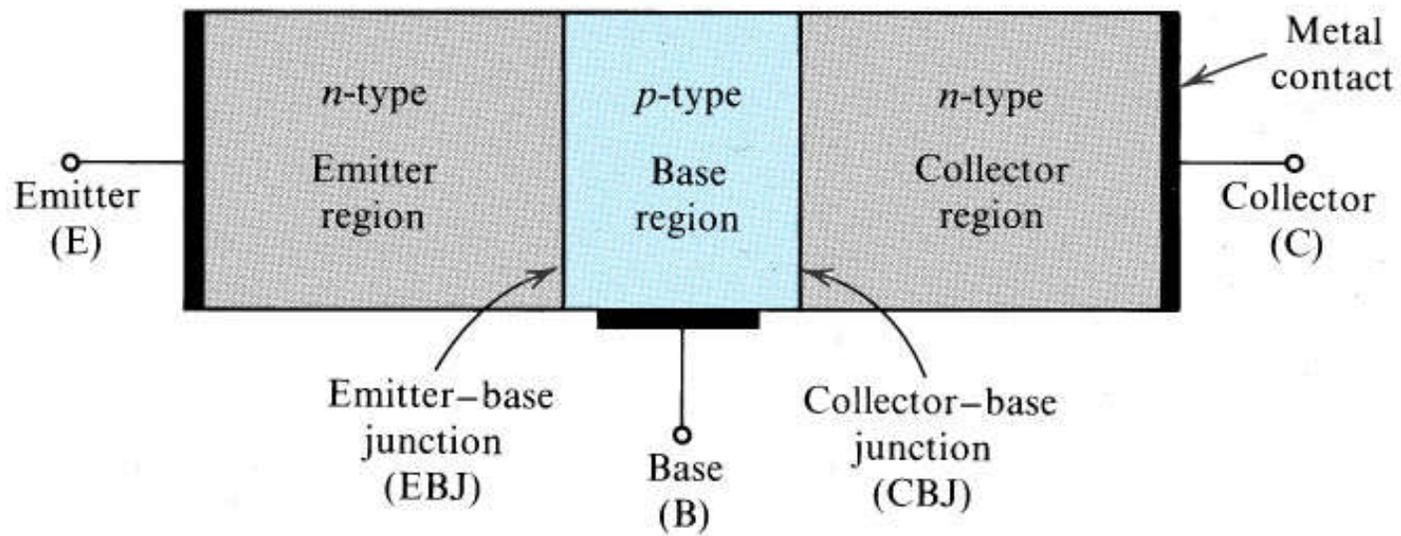


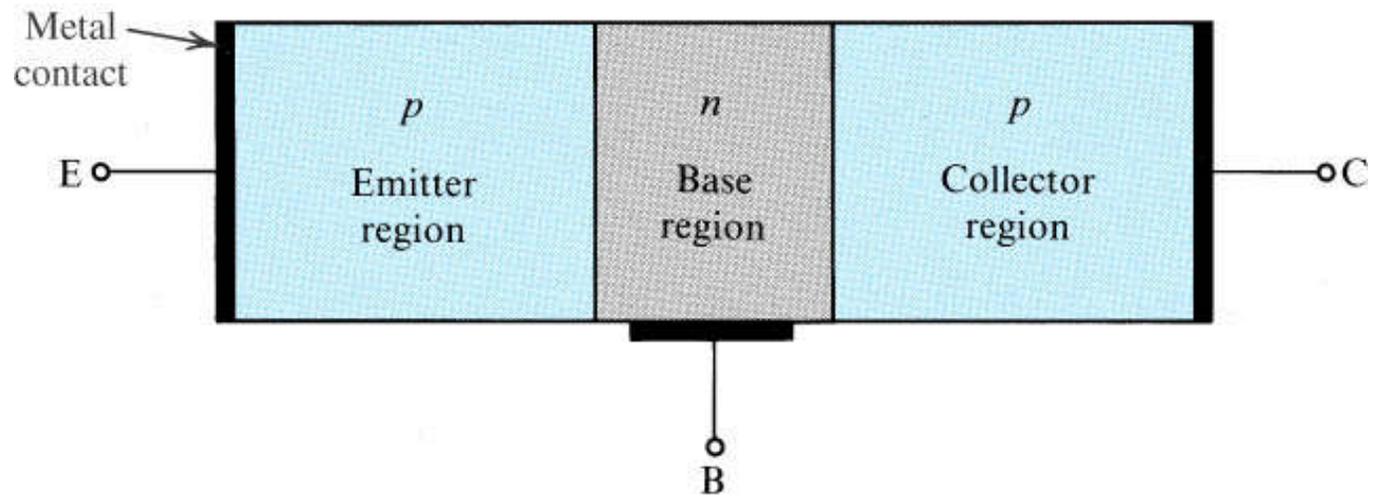


CHAPTER 5

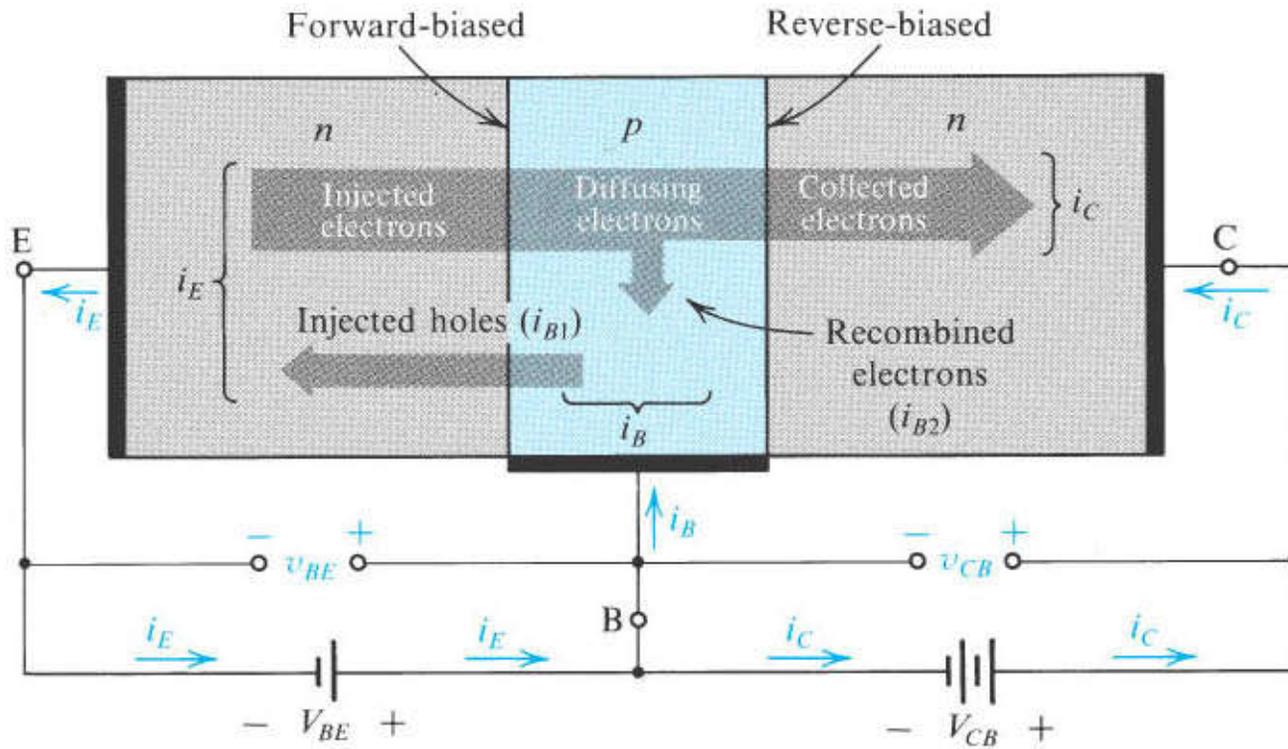
# Bipolar Junction Transistors (BJTs)



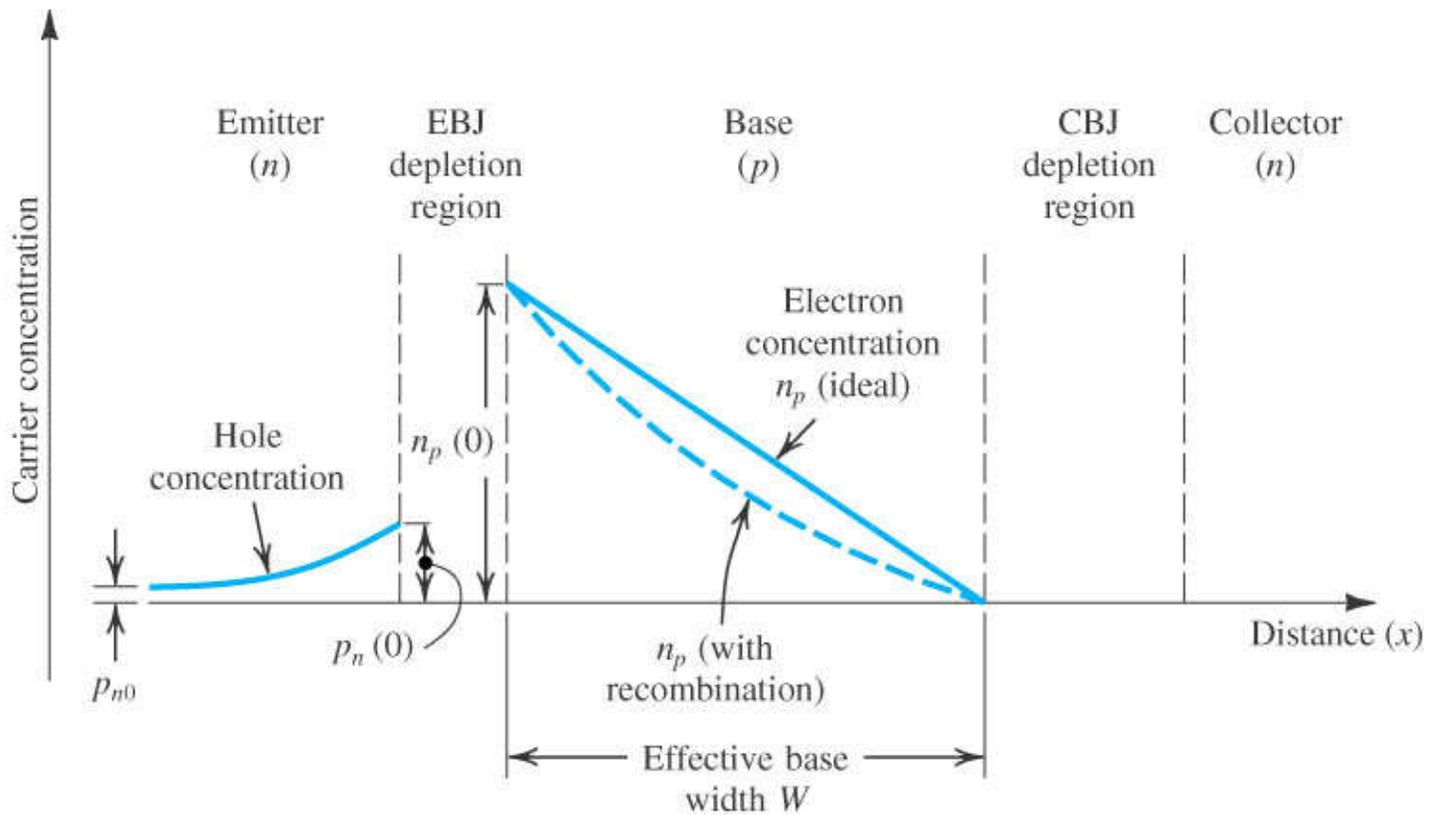
**Figure 5.1** A simplified structure of the *npn* transistor.



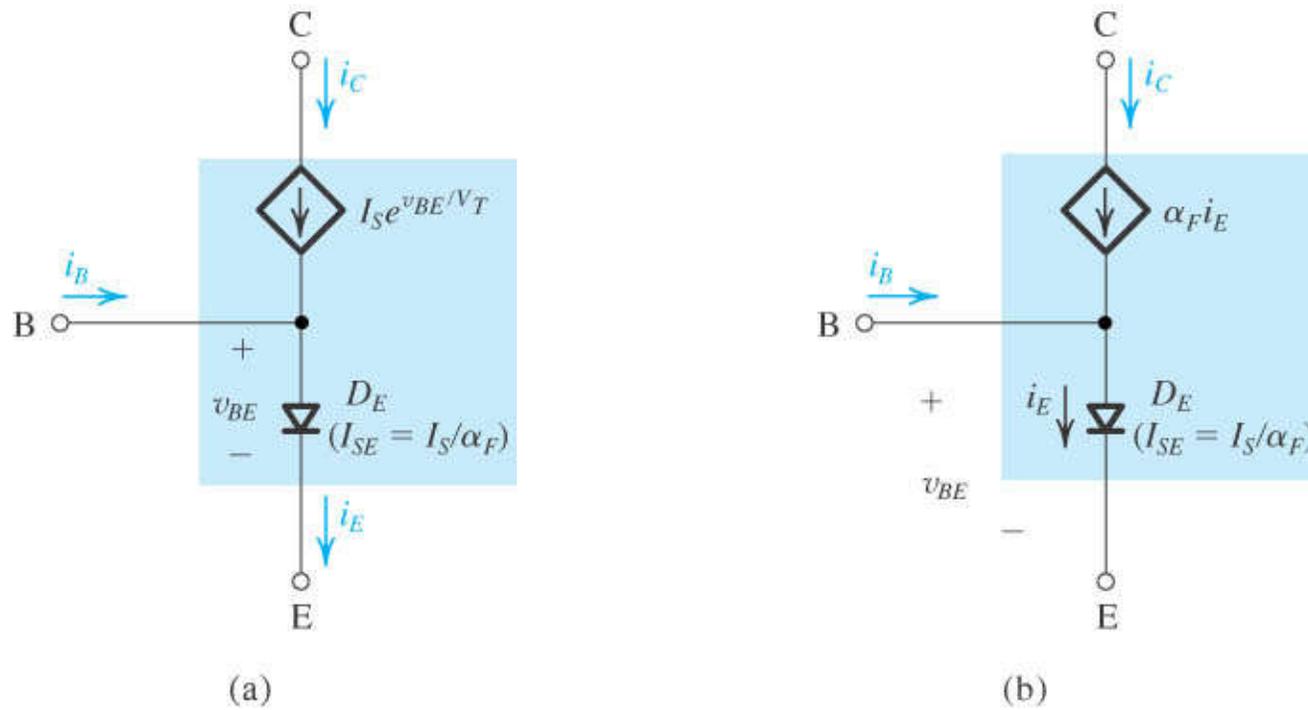
**Figure 5.2** A simplified structure of the *pnp* transistor.



**Figure 5.3** Current flow in an *npn* transistor biased to operate in the active mode. (Reverse current components due to drift of thermally generated minority carriers are not shown.)

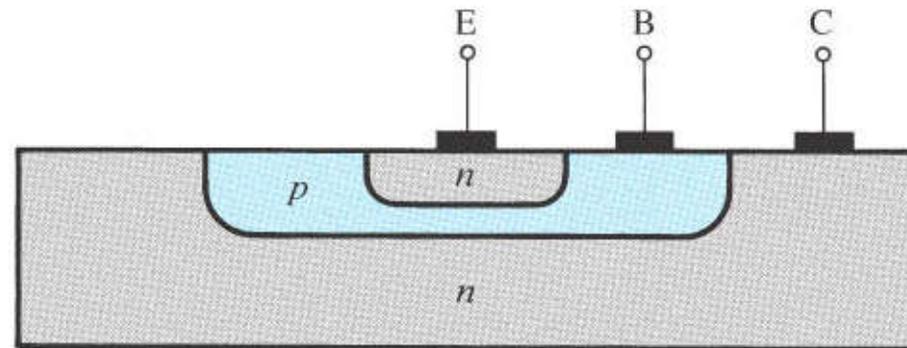


**Figure 5.4** Profiles of minority-carrier concentrations in the base and in the emitter of an *npn* transistor operating in the active mode:  $v_{BE} > 0$  and  $v_{CB} \geq 0$ .

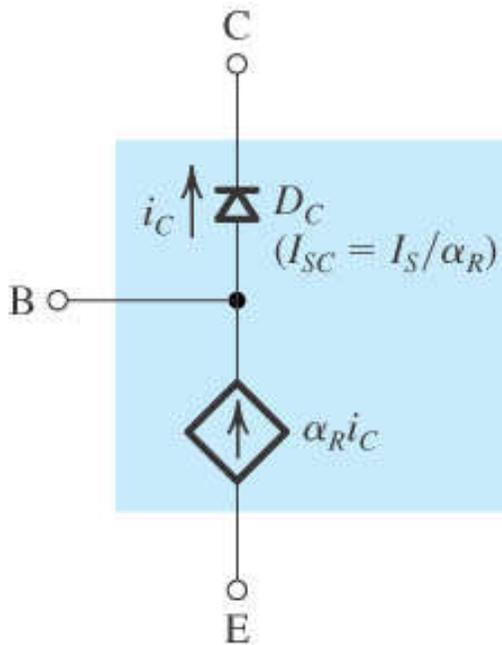


**Figure 5.5** Large-signal equivalent-circuit models of the *npn* BJT operating in the forward active mode.

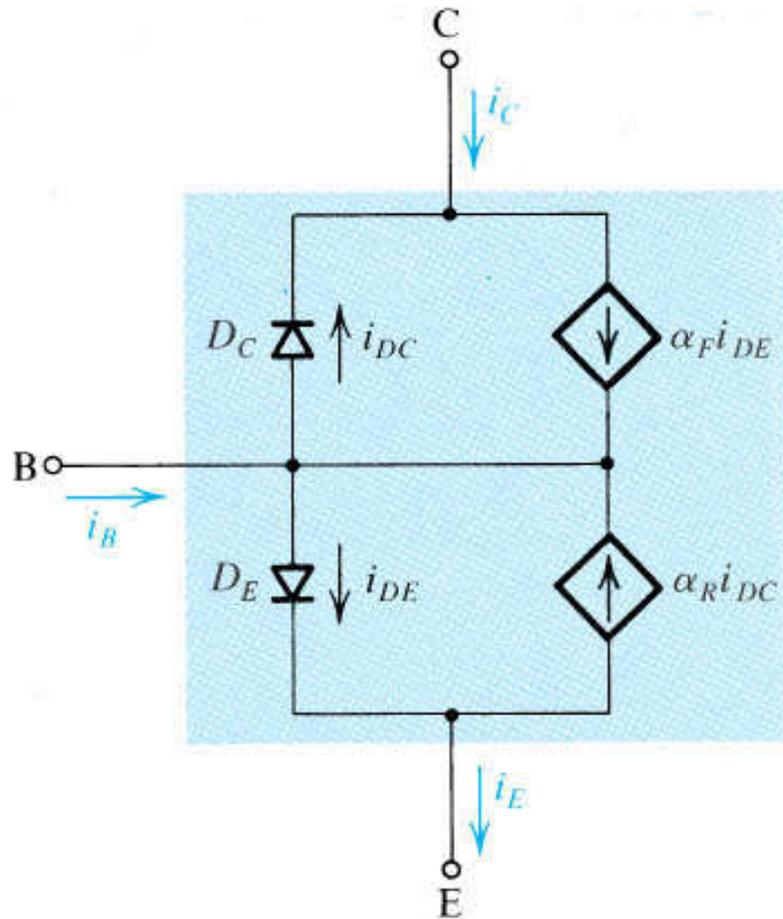
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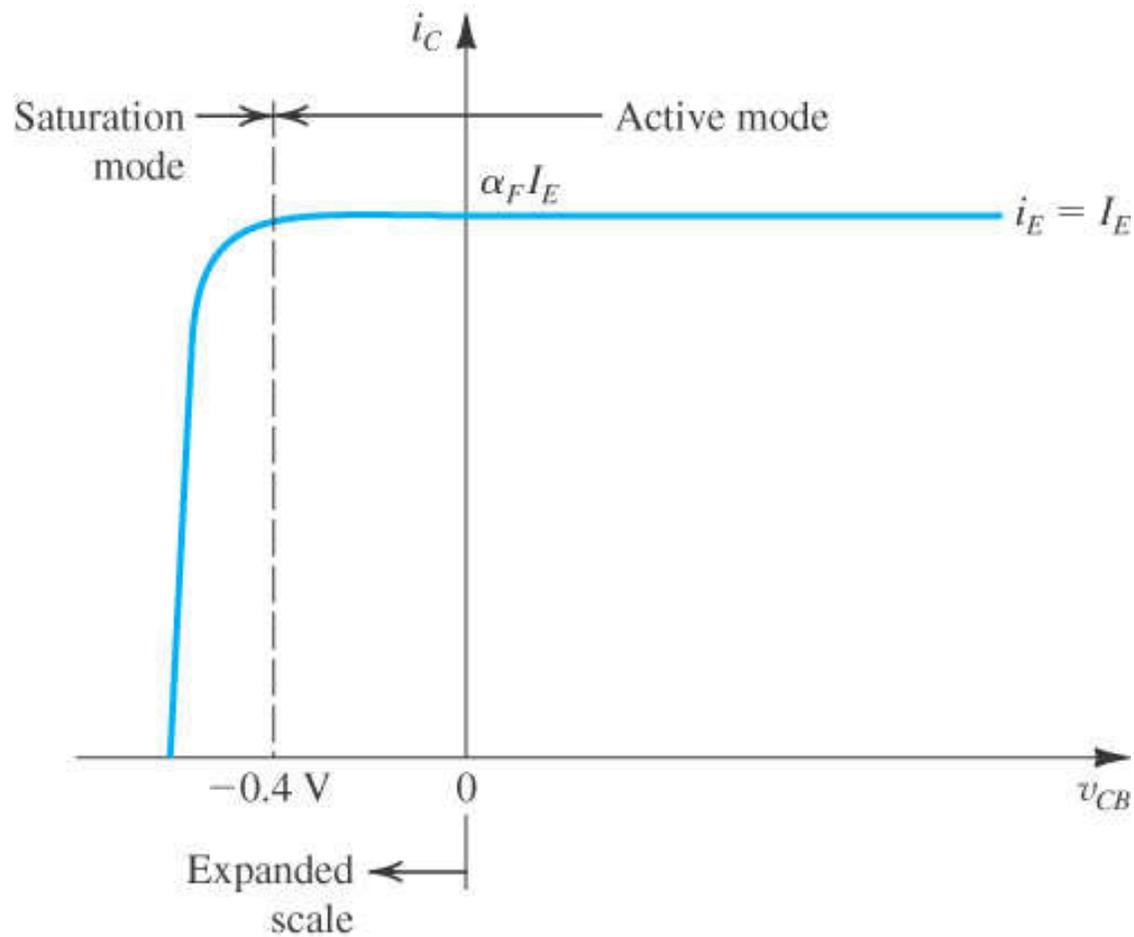
**Figure 5.6** Cross-section of an  $npn$  BJT.



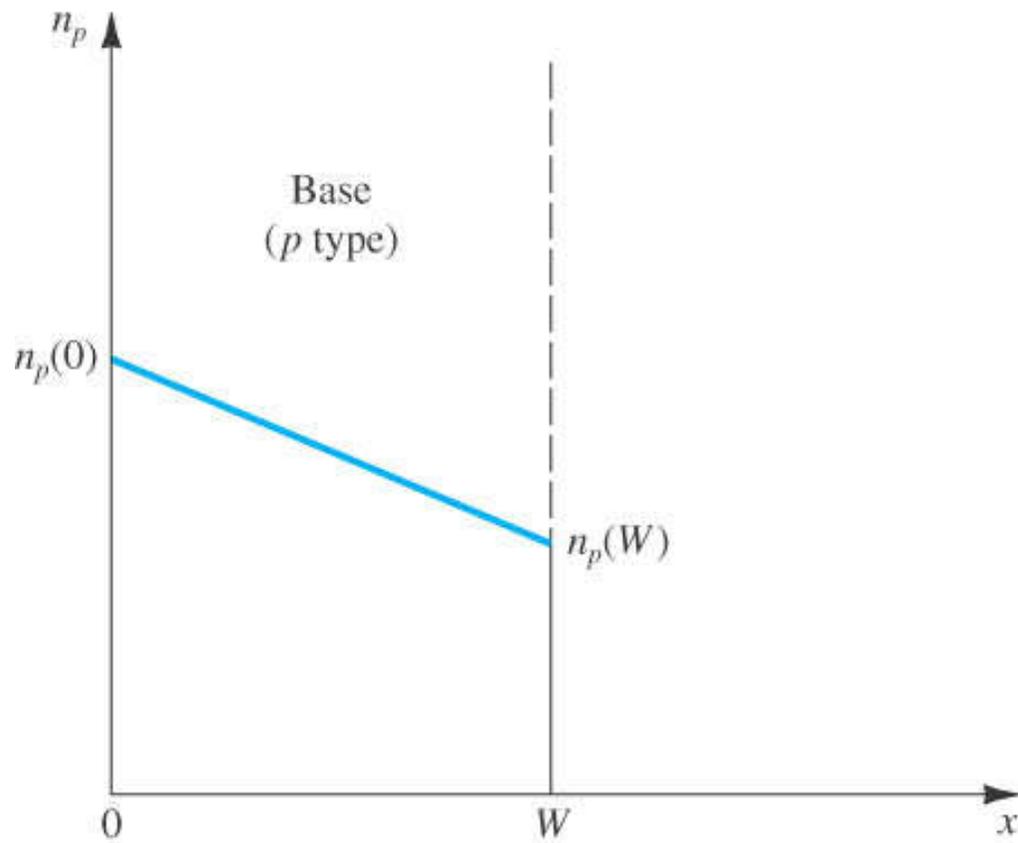
**Figure 5.7** Model for the *npn* transistor when operated in the reverse active mode (i.e., with the CBJ forward biased and the EBJ reverse biased).



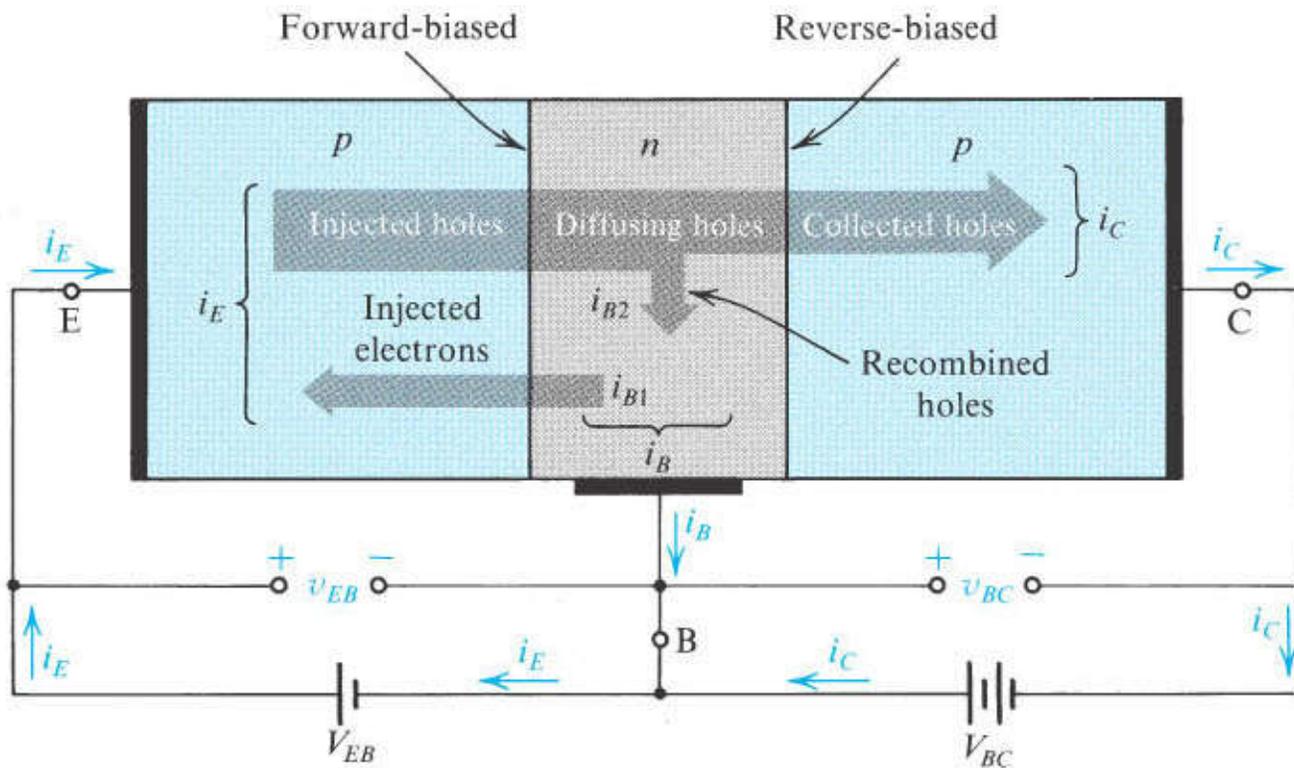
**Figure 5.8** The Ebers-Moll (EM) model of the *npn* transistor.



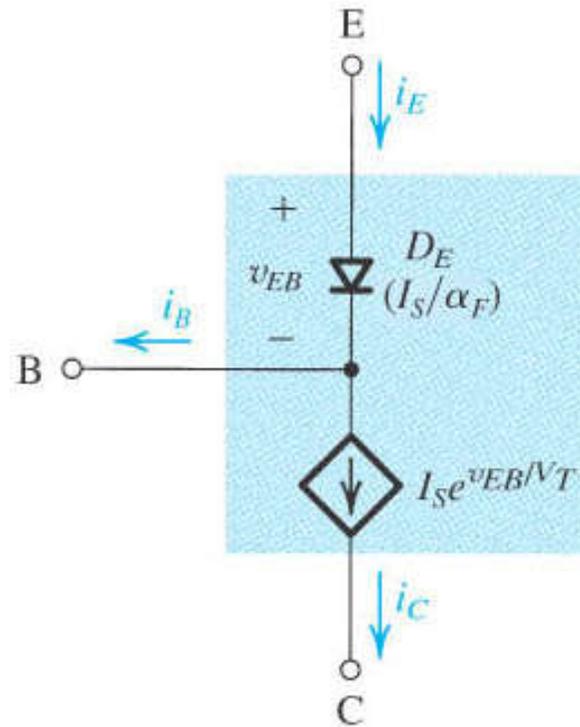
**Figure 5.9** The  $i_C$ - $v_{CB}$  characteristic of an *npn* transistor fed with a constant emitter current  $I_E$ . The transistor enters the saturation mode of operation for  $v_{CB} < -0.4$  V, and the collector current diminishes.



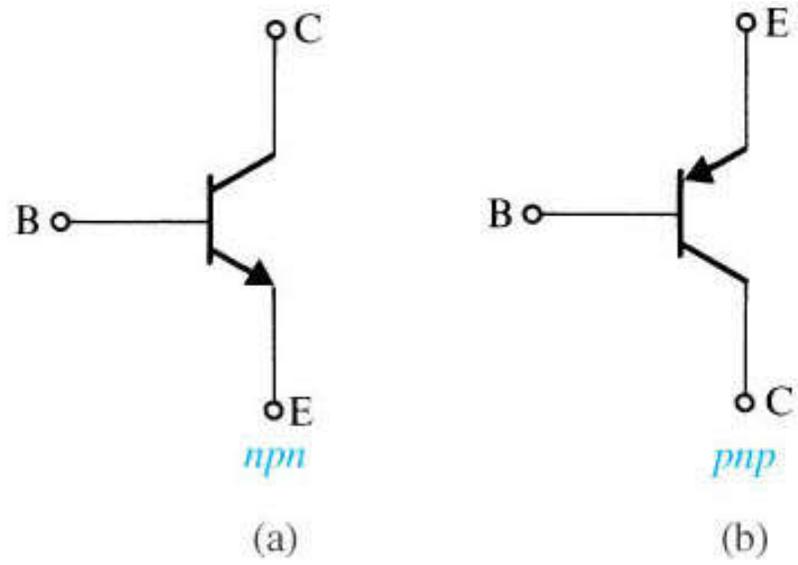
**Figure 5.10** Concentration profile of the minority carriers (electrons) in the base of an *npn* transistor operating in the saturation mode.



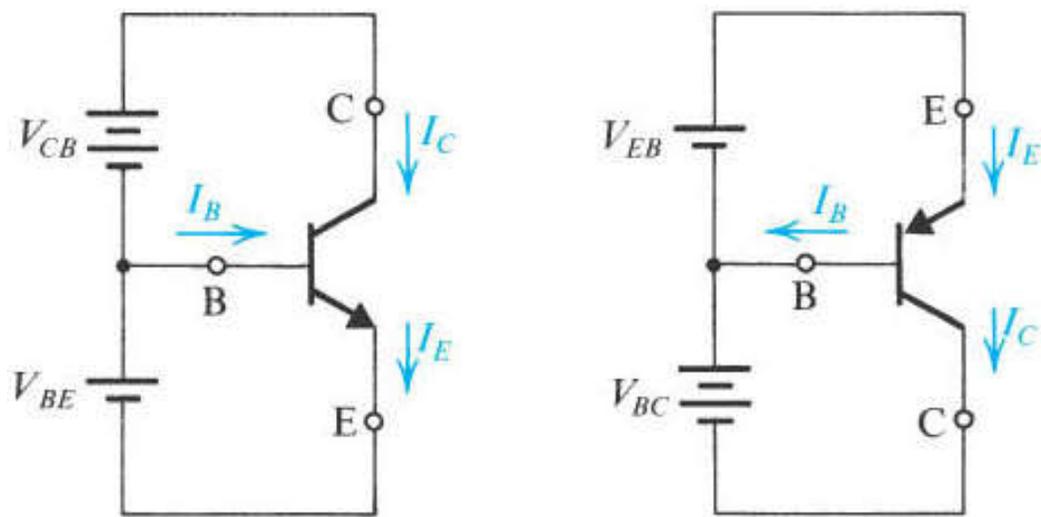
**Figure 5.11** Current flow in a *pnp* transistor biased to operate in the active mode.



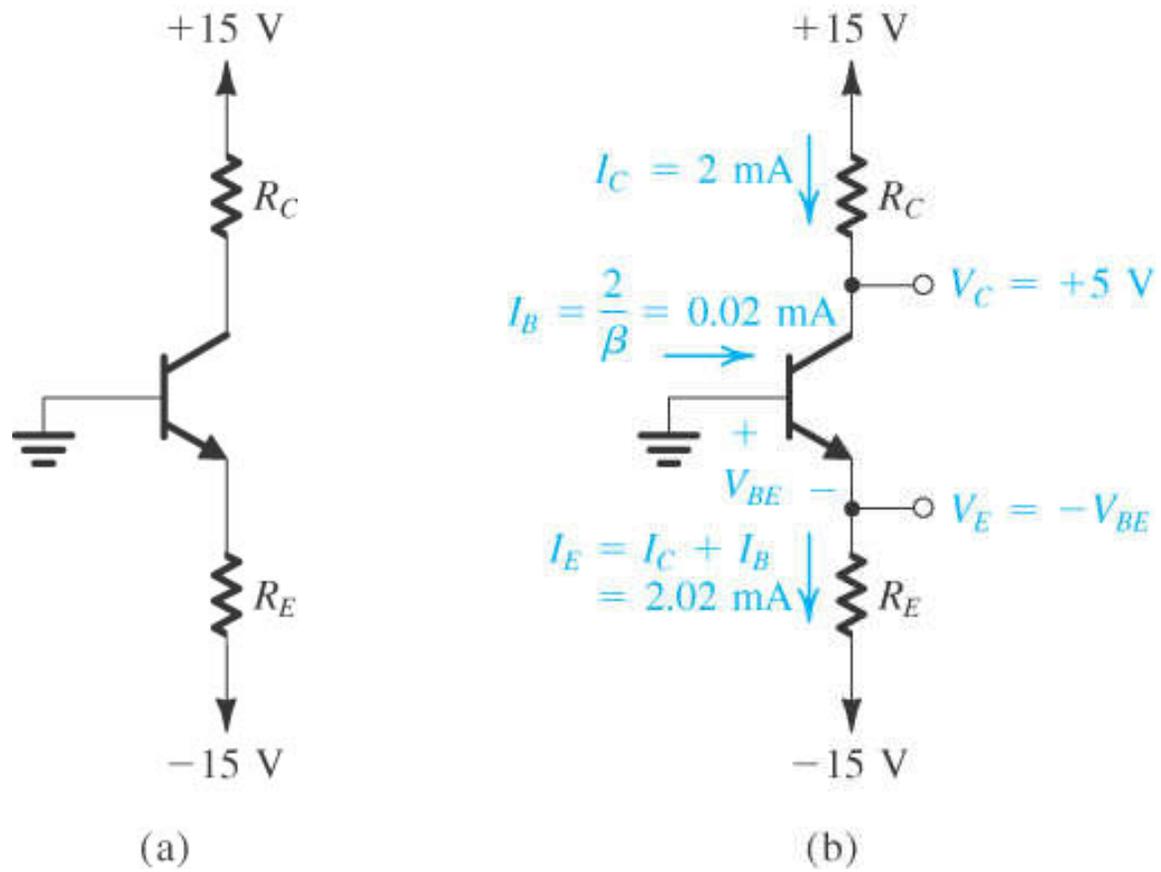
**Figure 5.12** Large-signal model for the *pnp* transistor operating in the active mode.



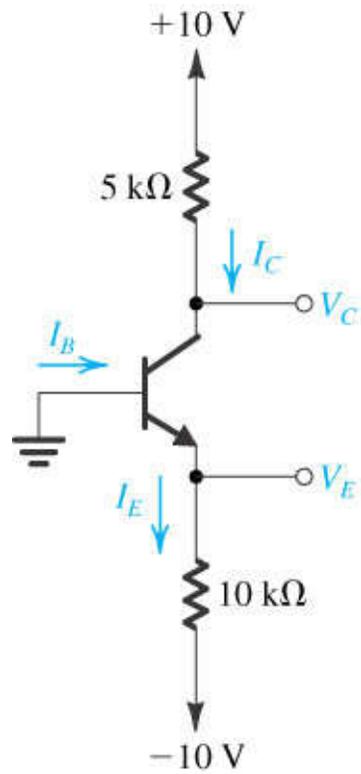
**Figure 5.13** Circuit symbols for BJTs.



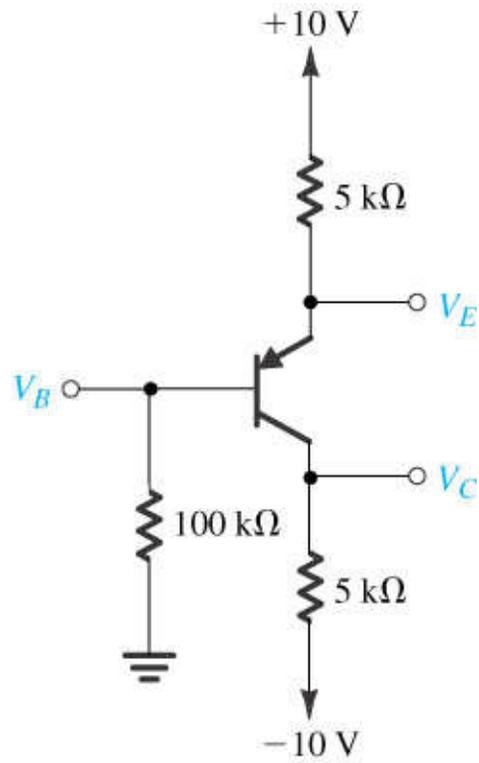
**Figure 5.14** Voltage polarities and current flow in transistors biased in the active mode.



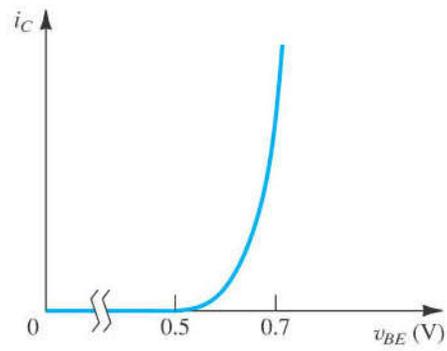
**Figure 5.15** Circuit for Example 5.1.



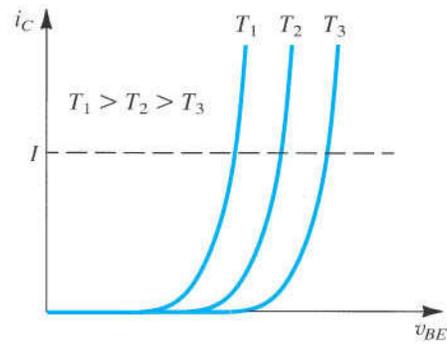
**Figure E5.10**



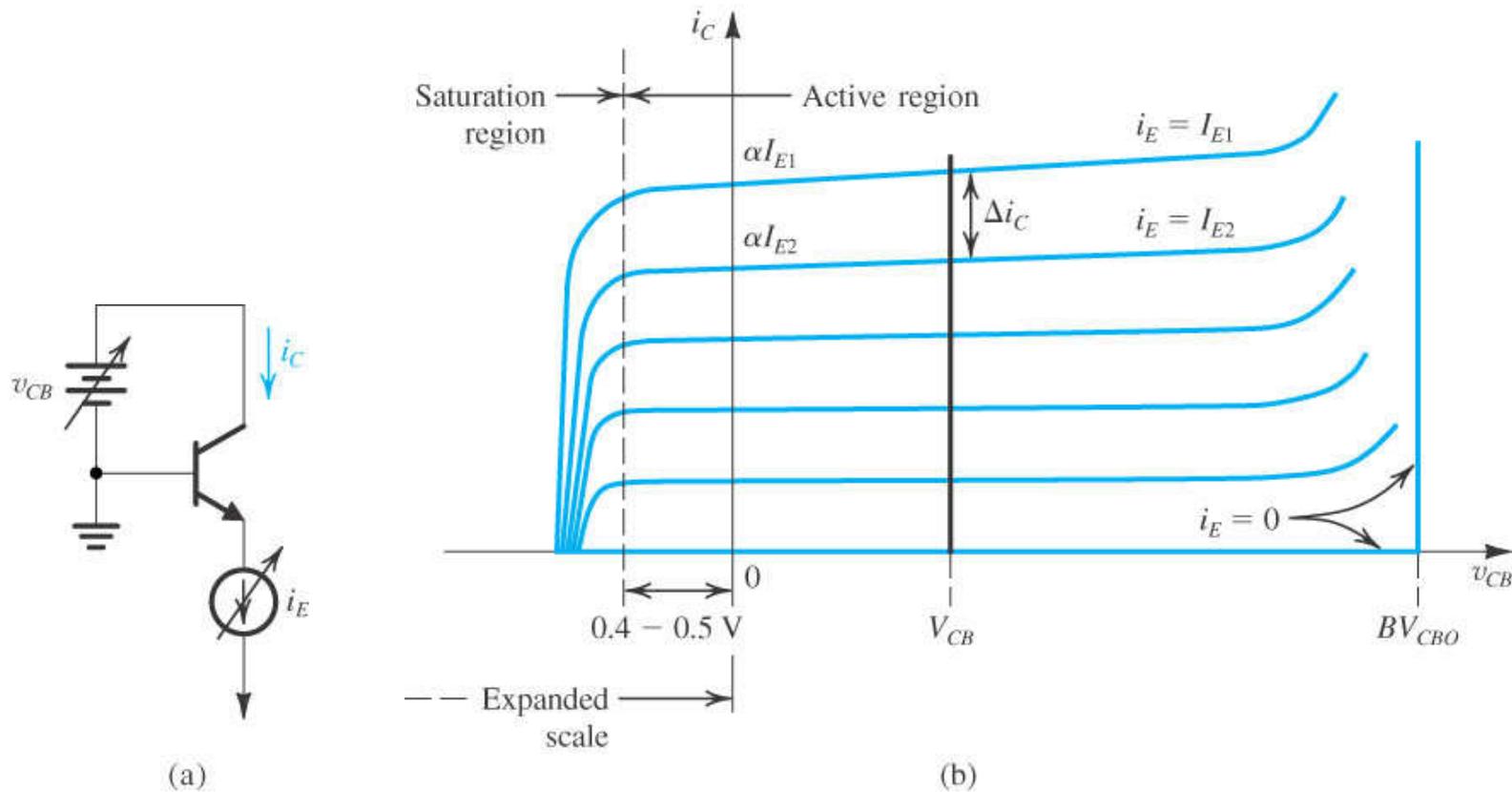
**Figure E5.11**



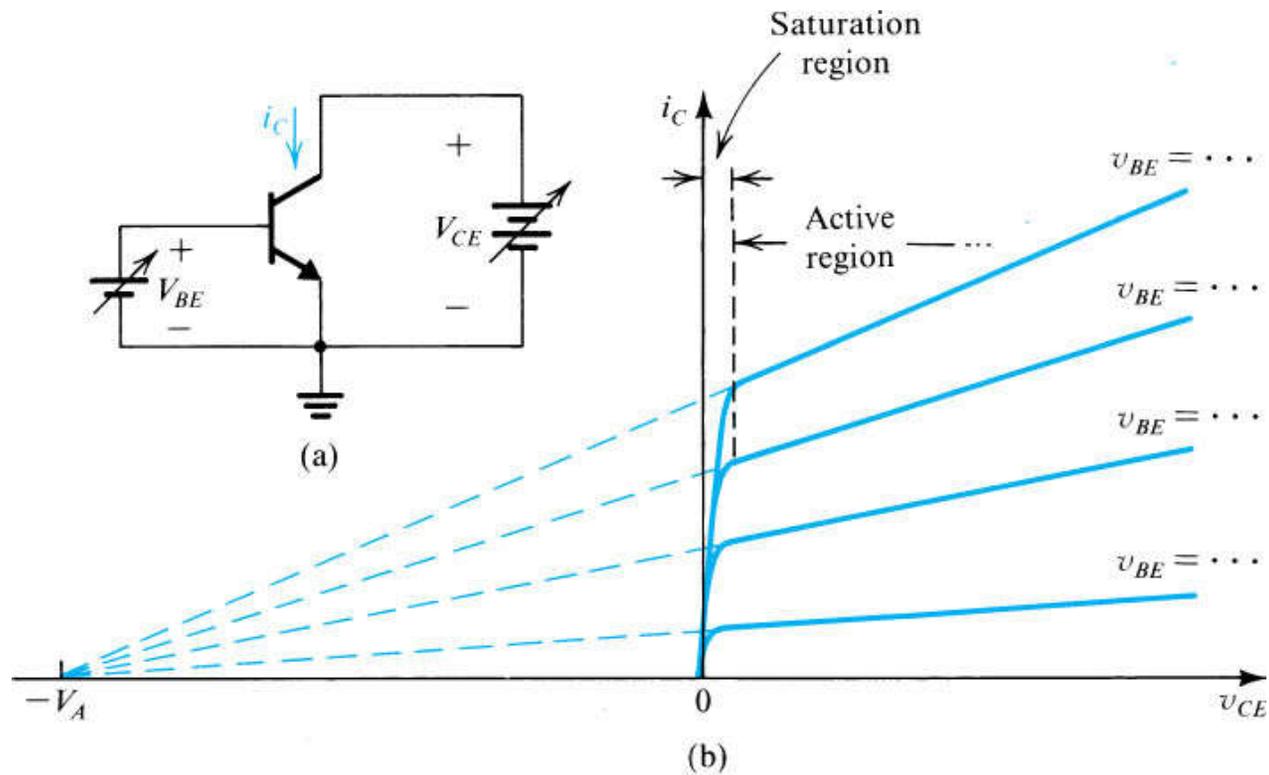
**Figure 5.16** The  $i_C$ - $v_{BE}$  characteristic for an *npn* transistor.



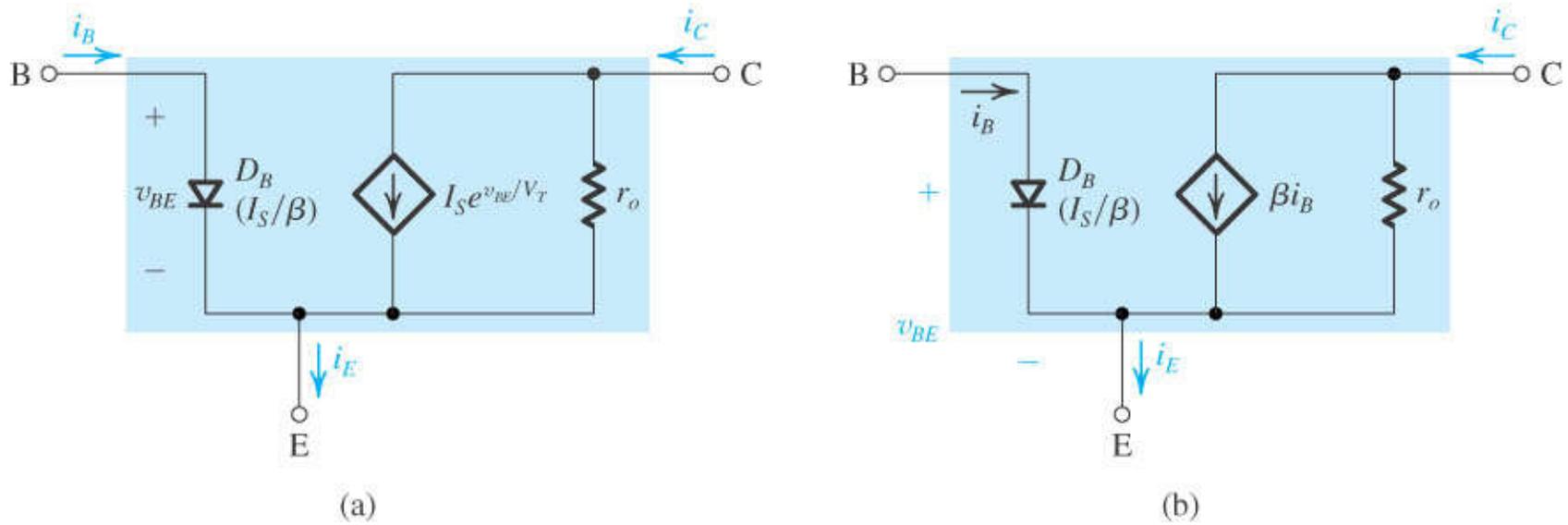
**Figure 5.17** Effect of temperature on the  $i_C$ - $v_{BE}$  characteristic. At a constant emitter current (broken line),  $v_{BE}$  changes by  $-2 \text{ mV}/^\circ\text{C}$ .



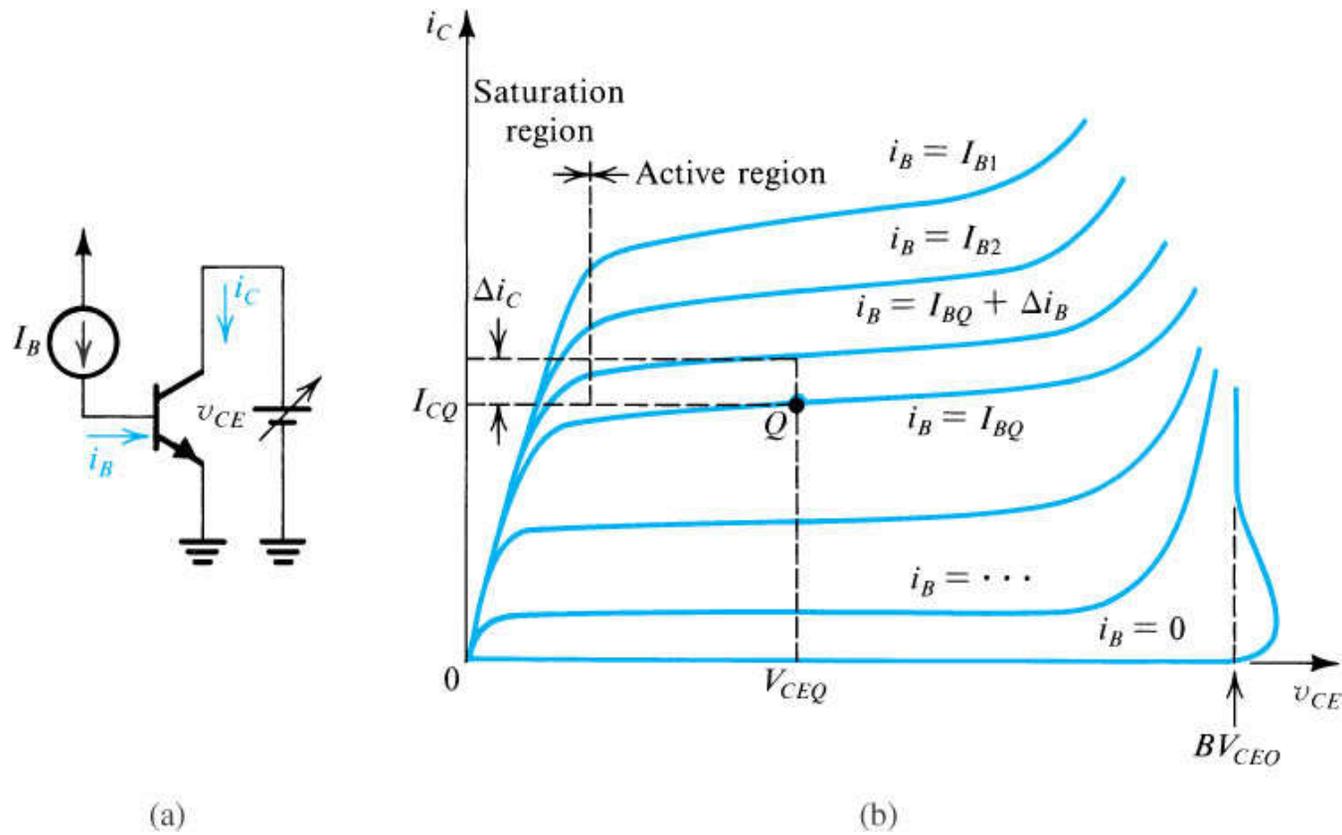
**Figure 5.18** The  $i_C$ - $v_{CB}$  characteristics of an *npn* transistor.



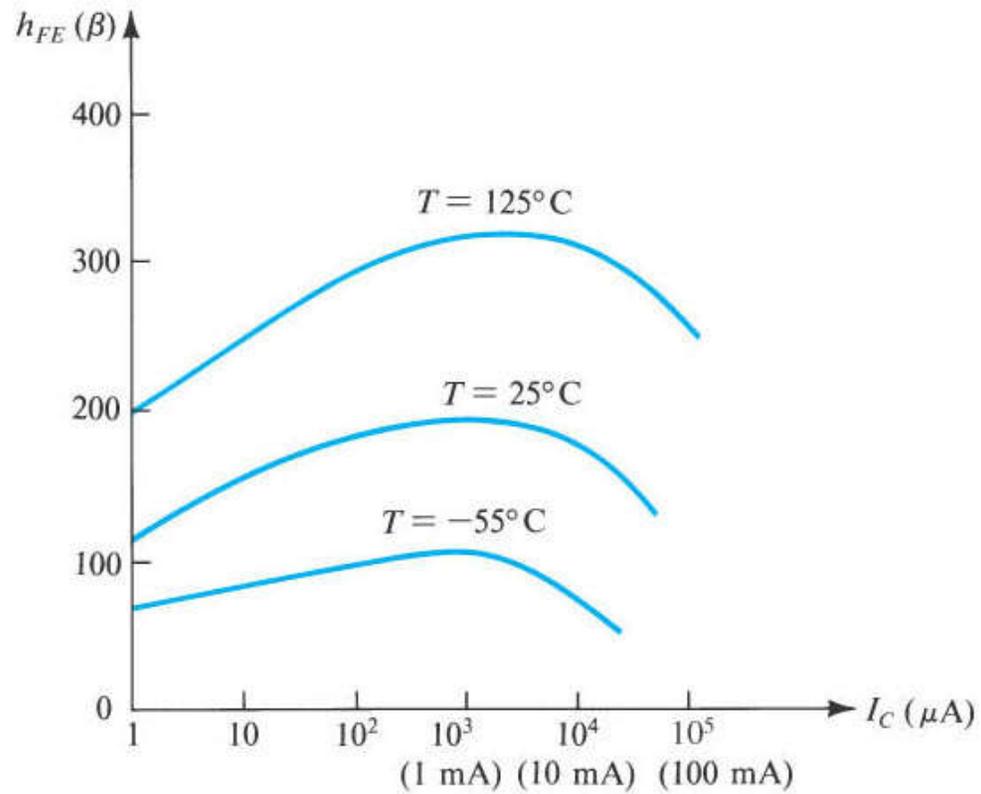
**Figure 5.19** (a) Conceptual circuit for measuring the  $i_C-v_{CE}$  characteristics of the BJT. (b) The  $i_C-v_{CE}$  characteristics of a practical BJT.



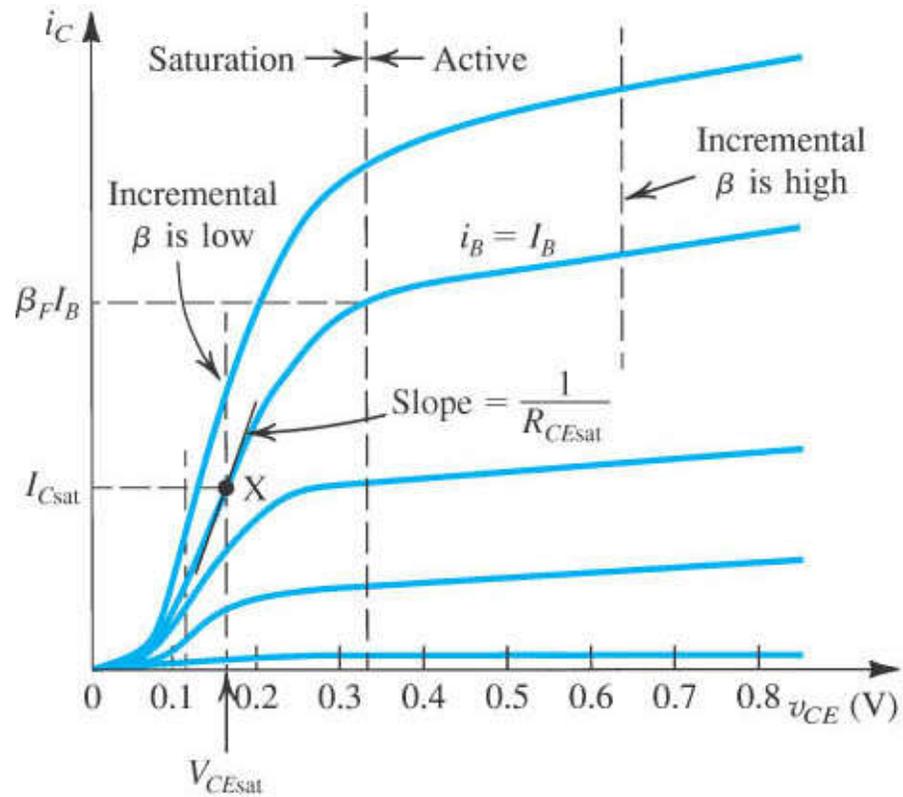
**Figure 5.20** Large-signal equivalent-circuit models of an *npn* BJT operating in the active mode in the common-emitter configuration.



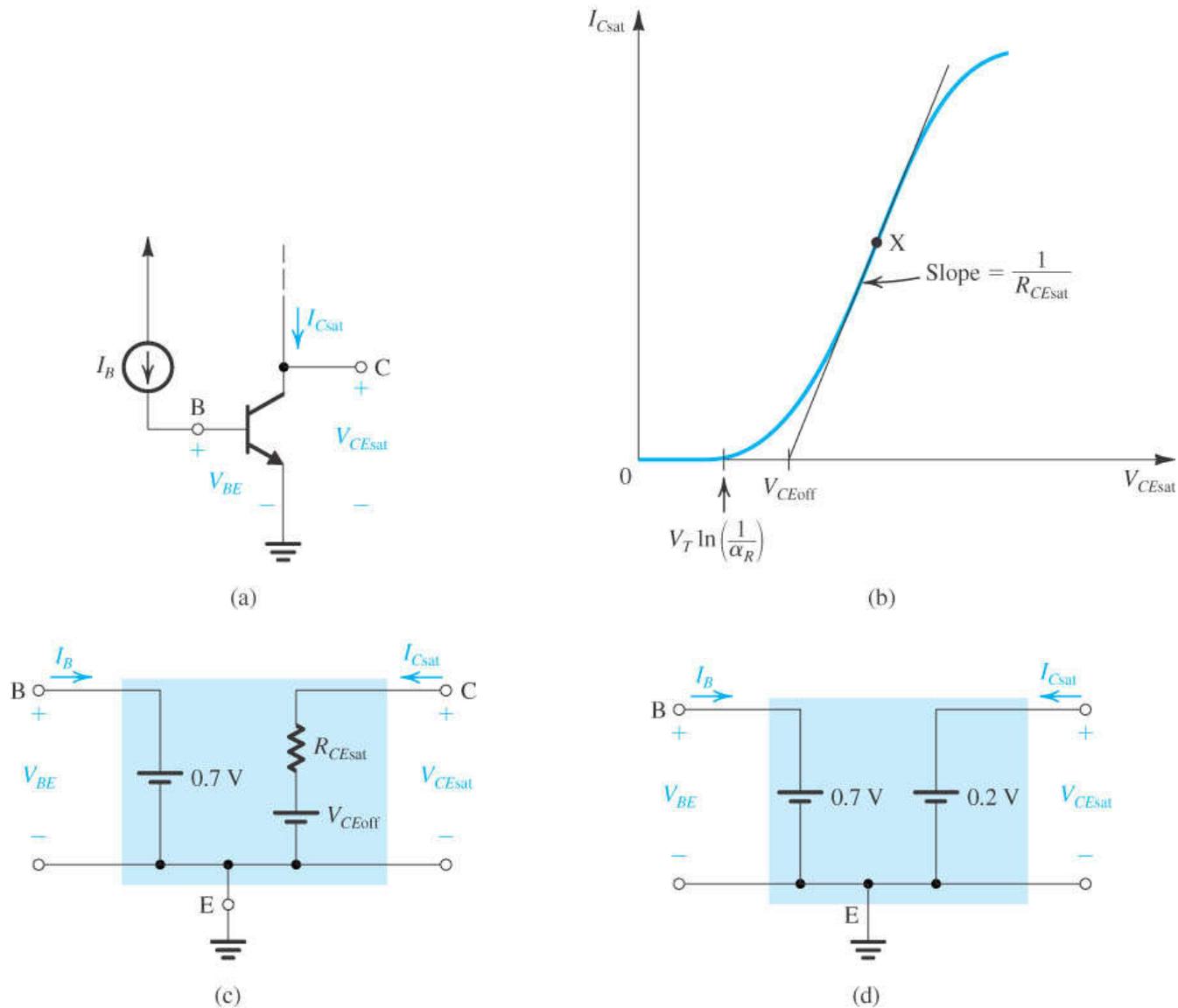
**Figure 5.21** Common-emitter characteristics. Note that the horizontal scale is expanded around the origin to show the saturation region in some detail.



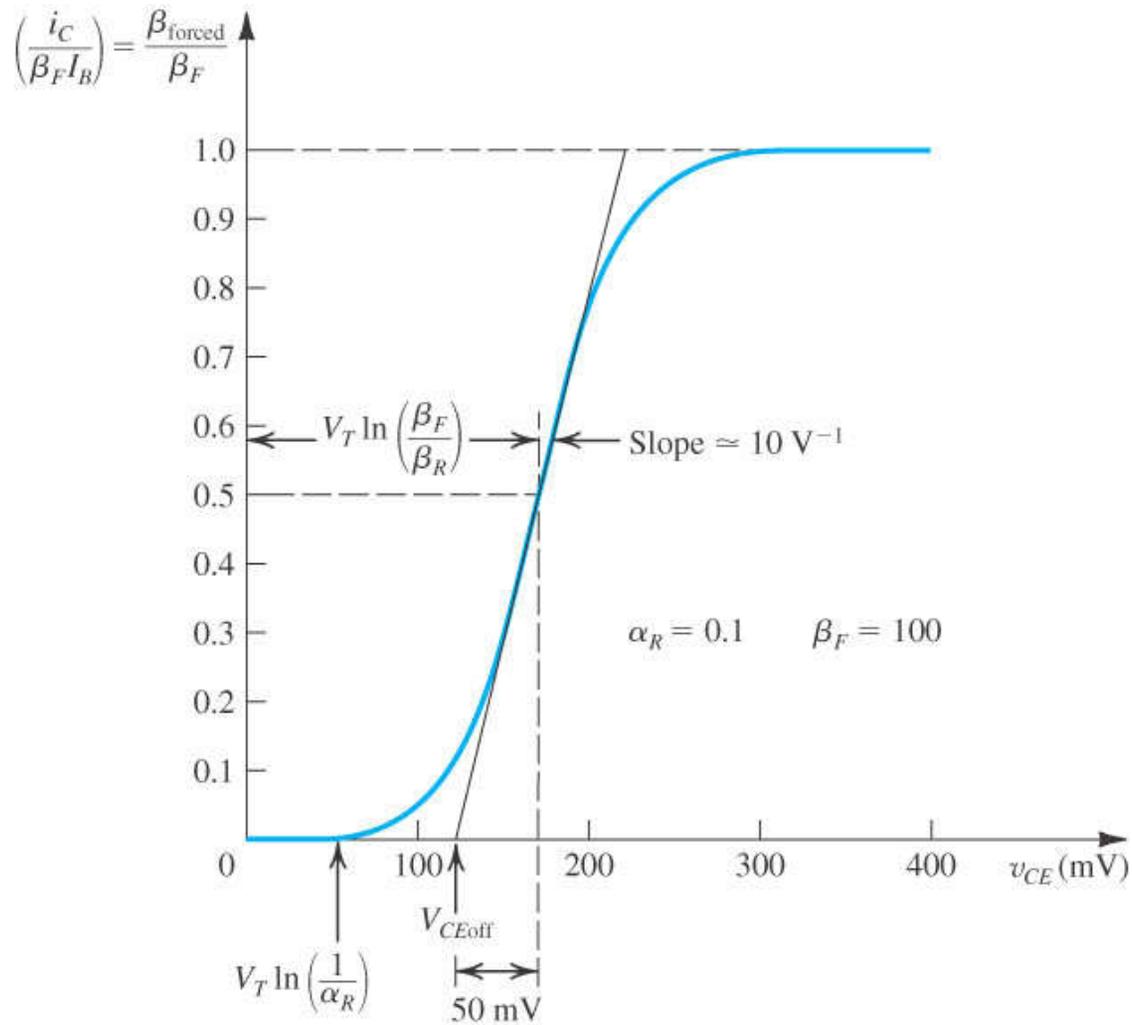
**Figure 5.22** Typical dependence of  $\beta$  on  $I_C$  and on temperature in a modern integrated-circuit *npn* silicon transistor intended for operation around 1 mA.



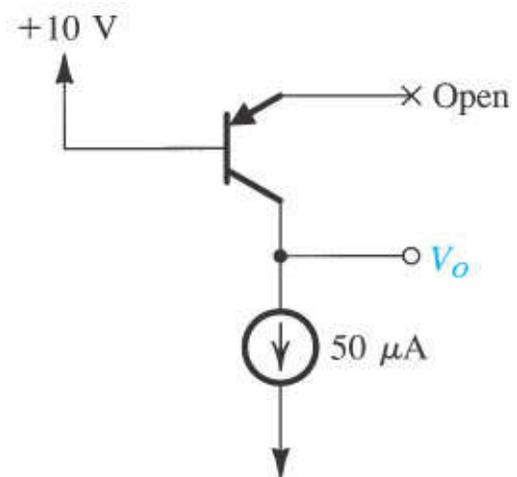
**Figure 5.23** An expanded view of the common-emitter characteristics in the saturation region.



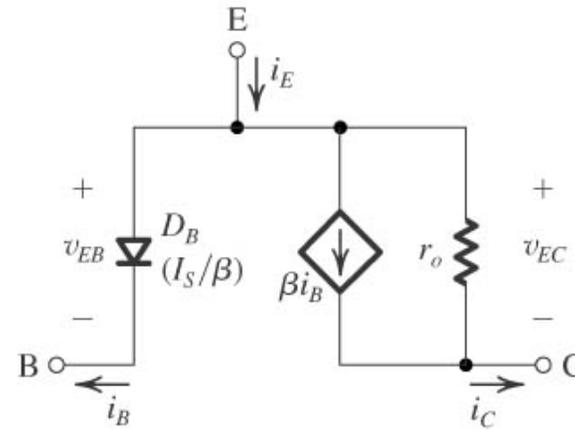
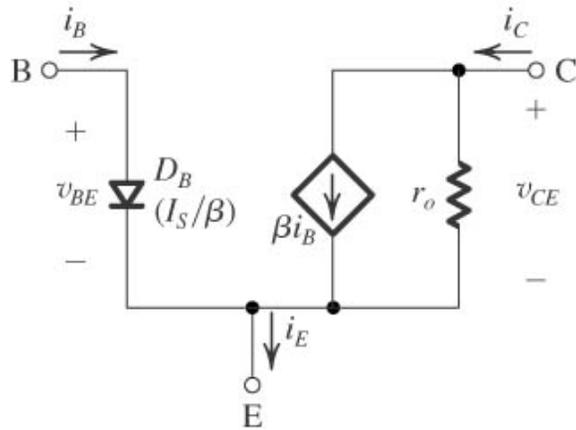
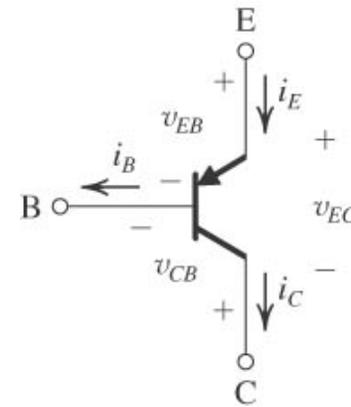
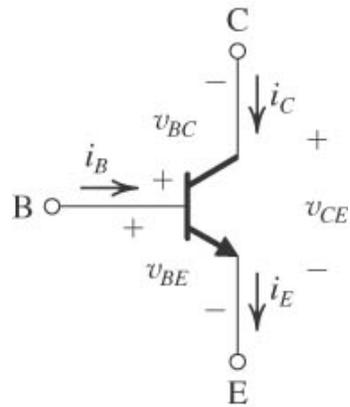
**Figure 5.24** (a) An *npn* transistor operated in saturation mode with a constant base current  $I_B$ . (b) The  $i_C$ - $v_{CE}$  characteristic curve corresponding to  $i_B = I_B$ . The curve can be approximated by a straight line of slope  $1/R_{CEsat}$ . (c) Equivalent-circuit representation of the saturated transistor. (d) A simplified equivalent-circuit model of the saturated transistor.



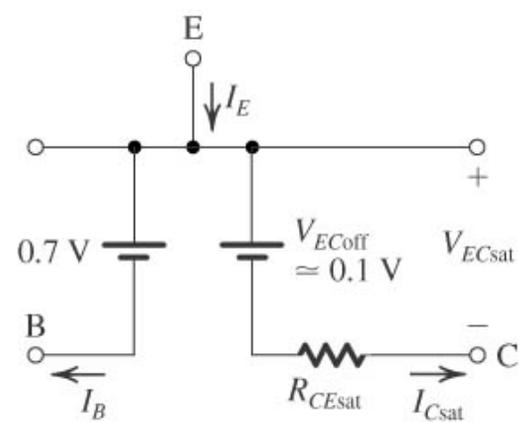
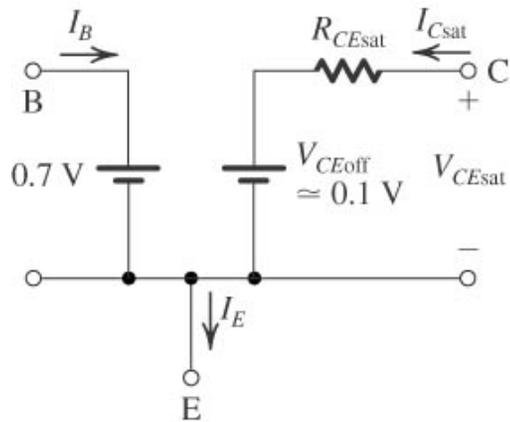
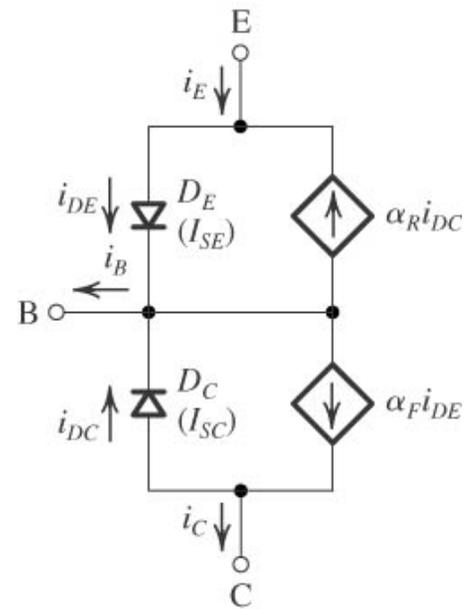
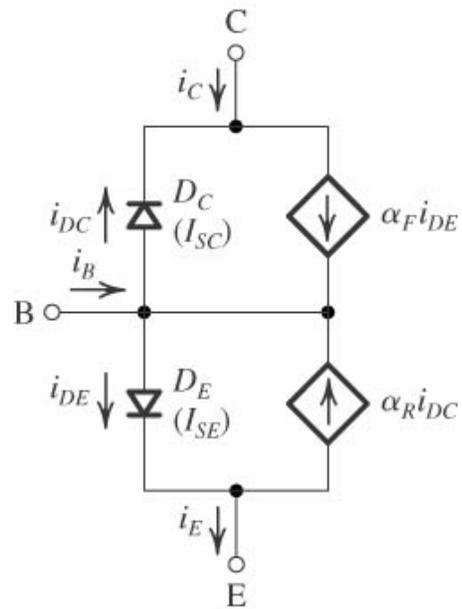
**Figure 5.25** Plot of the normalized  $i_C$  versus  $v_{CE}$  for an *npn* transistor with  $\beta_F = 100$  and  $\alpha_R = 0.1$ . This is a plot of Eq. (5.47), which is derived using the Ebers-Moll model.



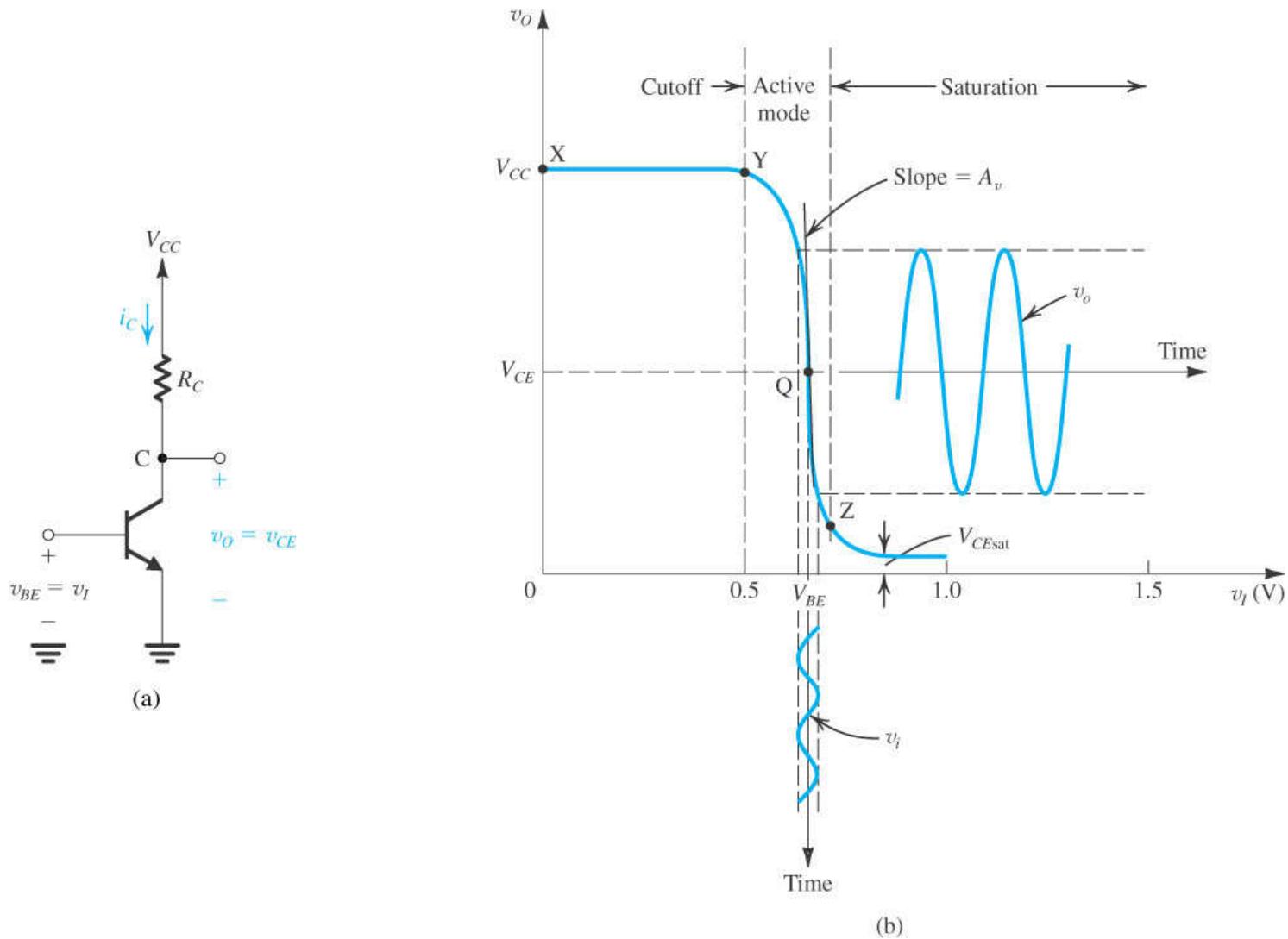
**Figure E5.18**



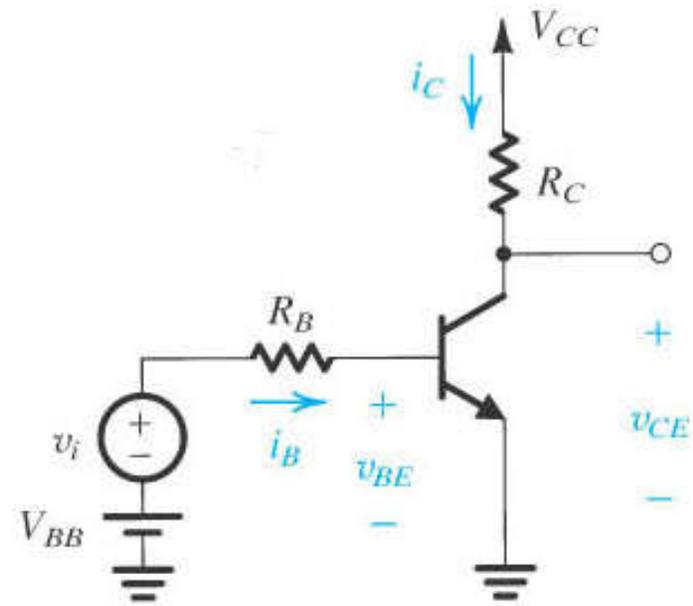
**Table 5.3**



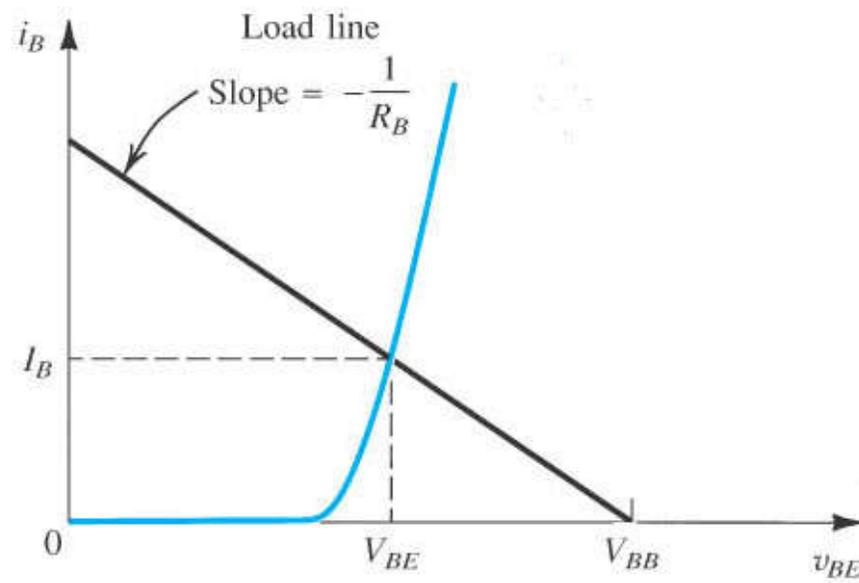
**Table 5.3** (Continued)



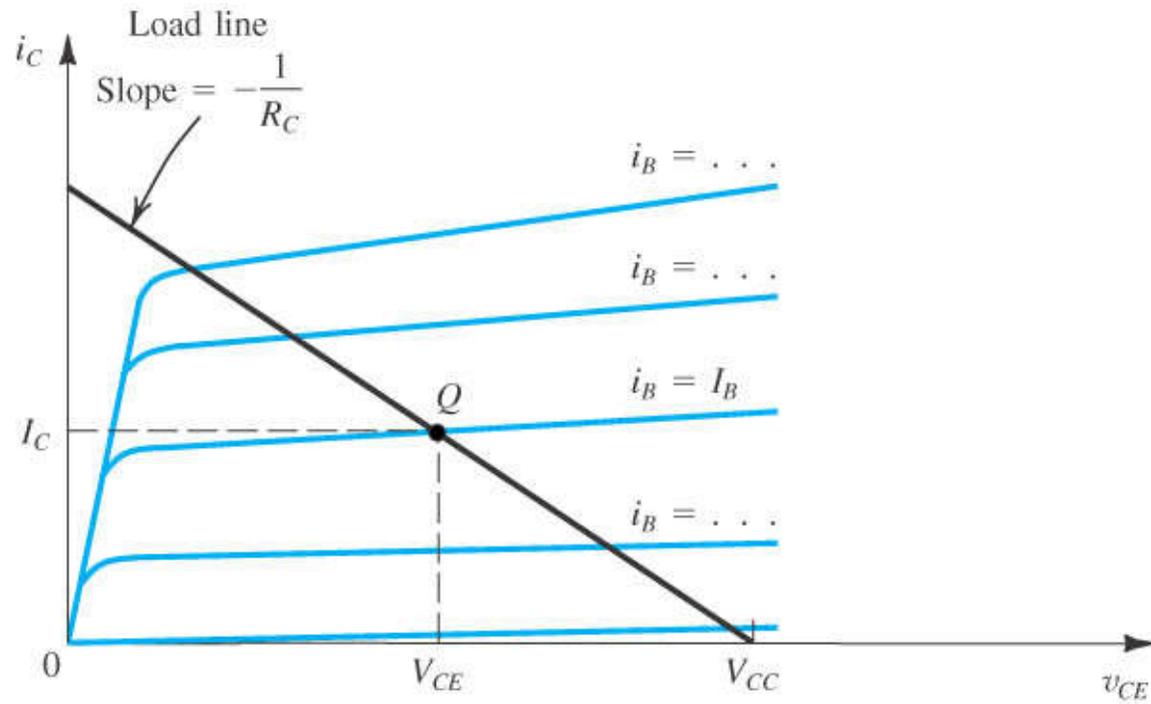
**Figure 5.26** (a) Basic common-emitter amplifier circuit. (b) Transfer characteristic of the circuit in (a). The amplifier is biased at a point Q, and a small voltage signal  $v_i$  is superimposed on the dc bias voltage  $V_{BE}$ . The resulting output signal  $v_o$  appears superimposed on the dc collector voltage  $V_{CE}$ . The amplitude of  $v_o$  is larger than that of  $v_i$  by the voltage gain  $A_v$ .



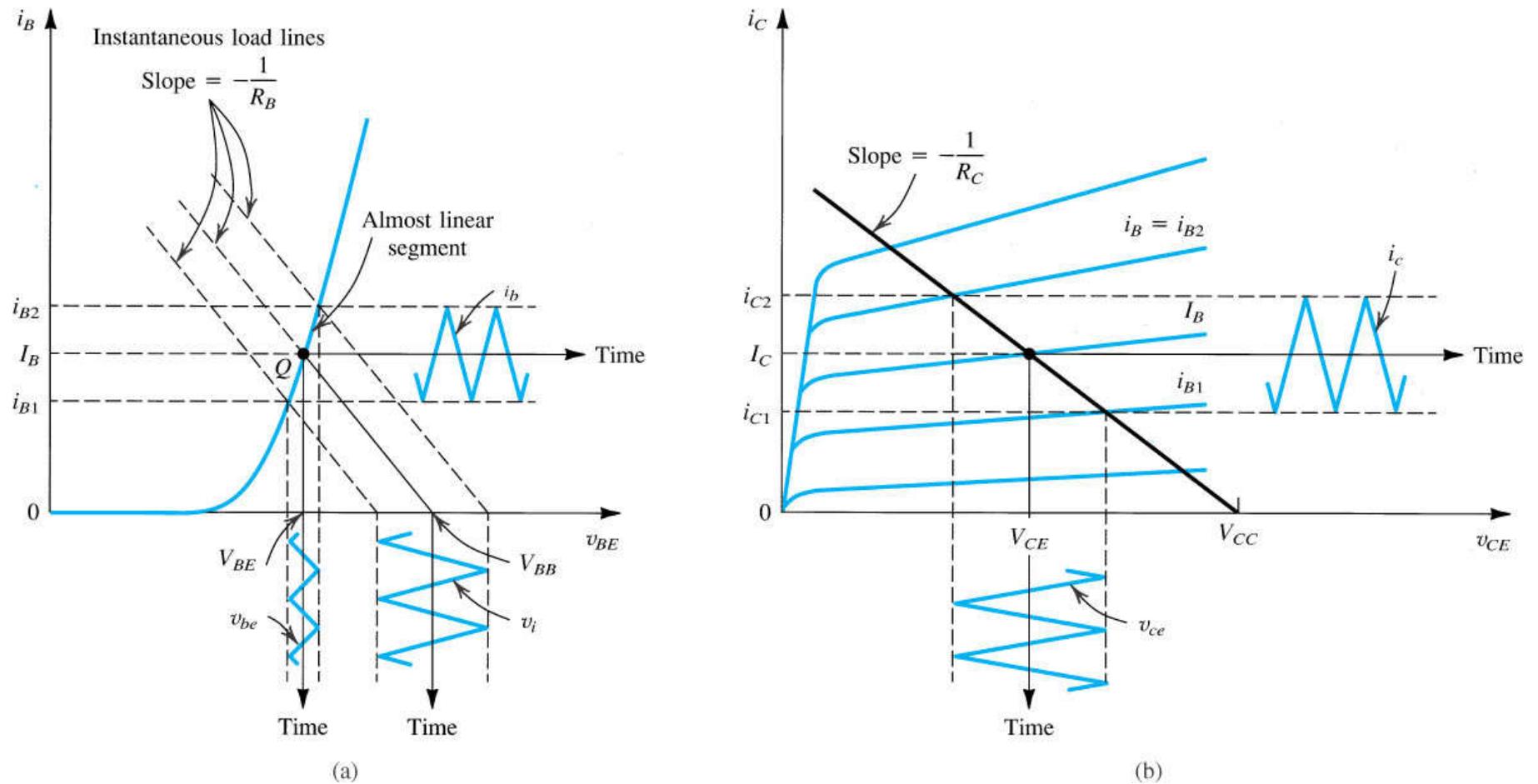
**Figure 5.27** Circuit whose operation is to be analyzed graphically.



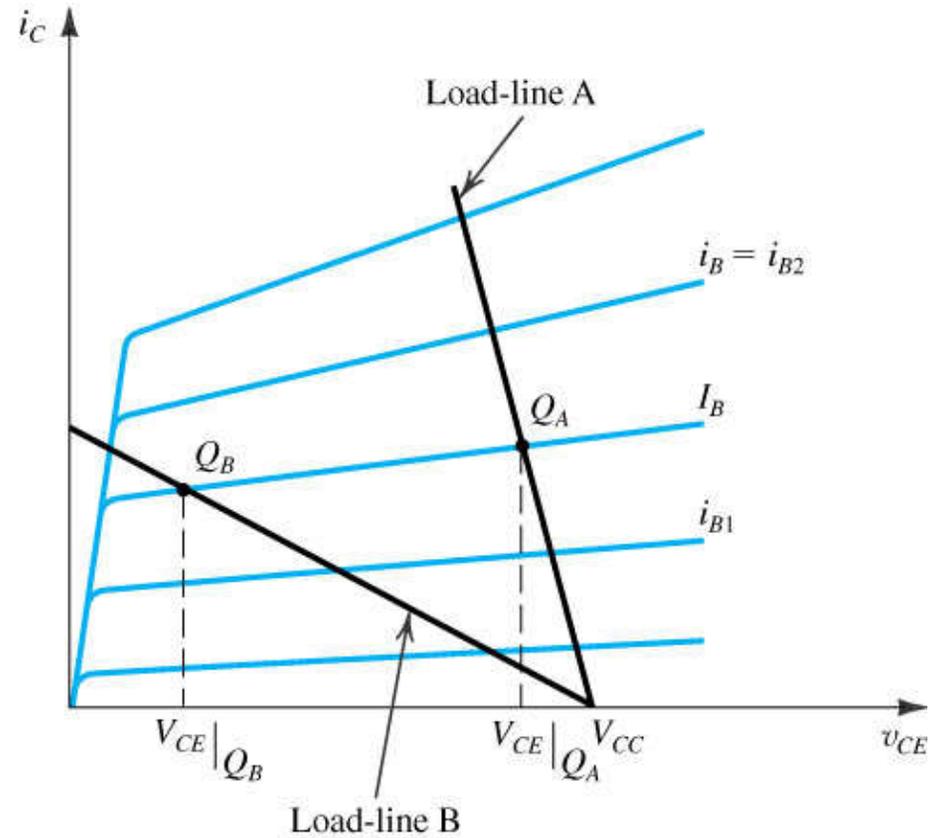
**Figure 5.28** Graphical construction for the determination of the dc base current in the circuit of Fig. 5.27.



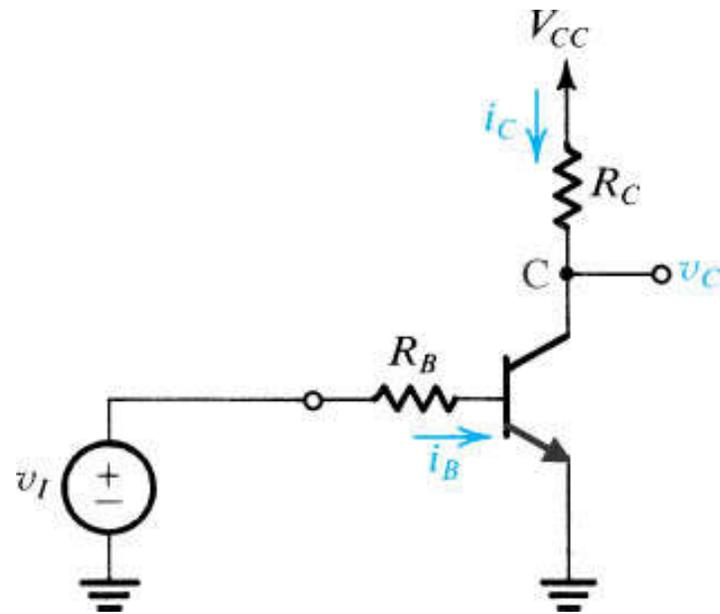
**Figure 5.29** Graphical construction for determining the dc collector current  $I_C$  and the collector-to-emitter voltage  $V_{CE}$  in the circuit of Fig. 5.27.



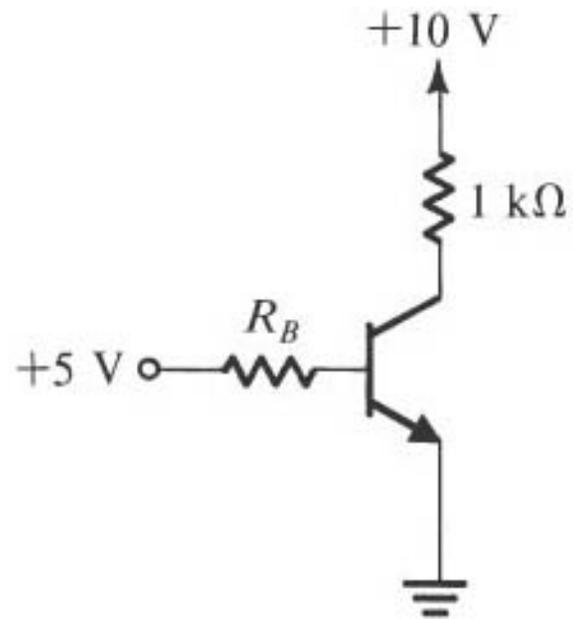
**Figure 5.30** Graphical determination of the signal components  $v_{be}$ ,  $i_b$ ,  $i_c$ , and  $v_{ce}$  when a signal component  $v_i$  is superimposed on the dc voltage  $V_{BB}$  (see Fig. 5.27).



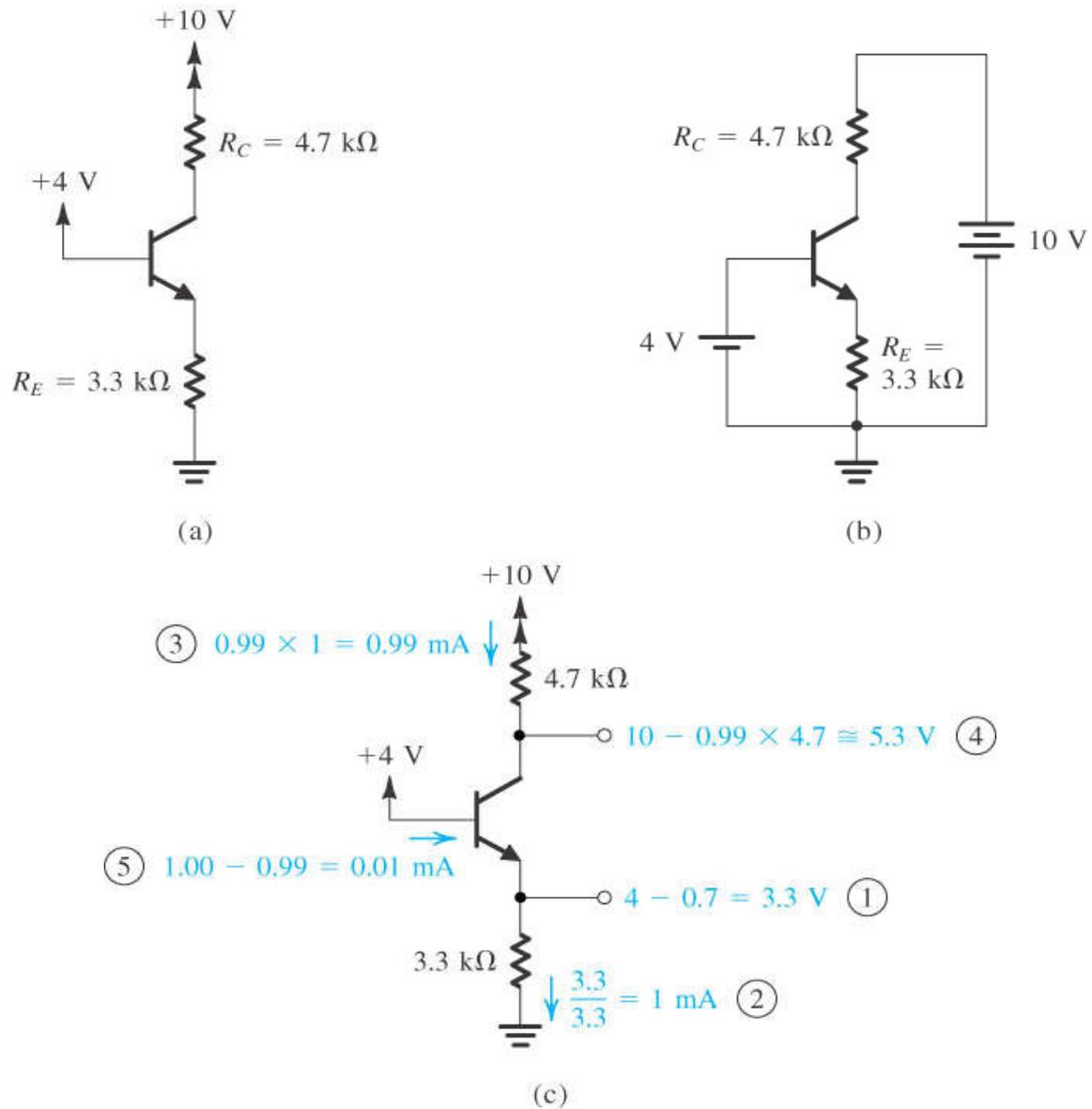
**Figure 5.31** Effect of bias-point location on allowable signal swing: Load-line A results in bias point  $Q_A$  with a corresponding  $V_{CE}$  which is too close to  $V_{CC}$  and thus limits the positive swing of  $v_{CE}$ . At the other extreme, load-line B results in an operating point too close to the saturation region, thus limiting the negative swing of  $v_{CE}$ .



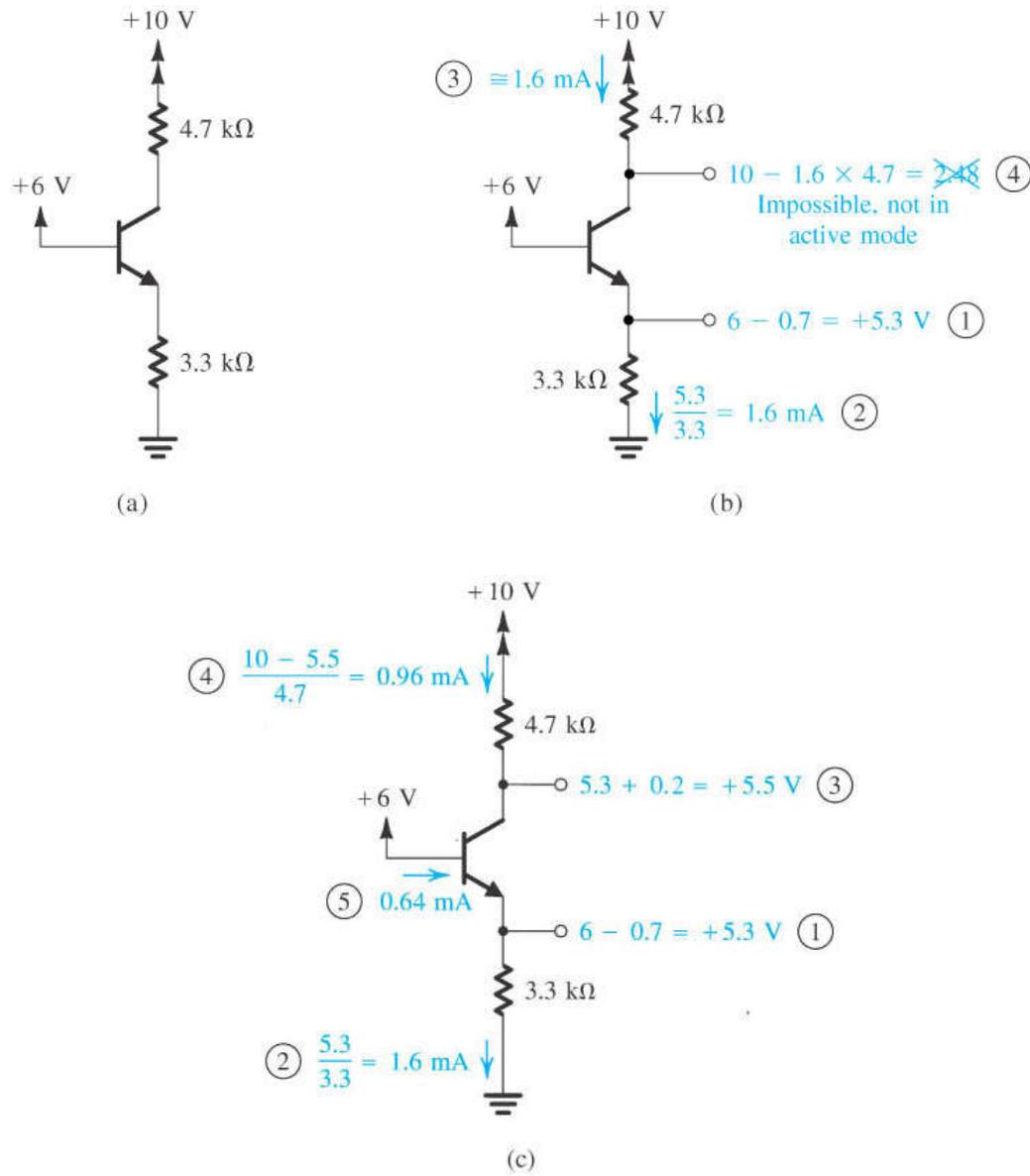
**Figure 5.32** A simple circuit used to illustrate the different modes of operation of the BJT.



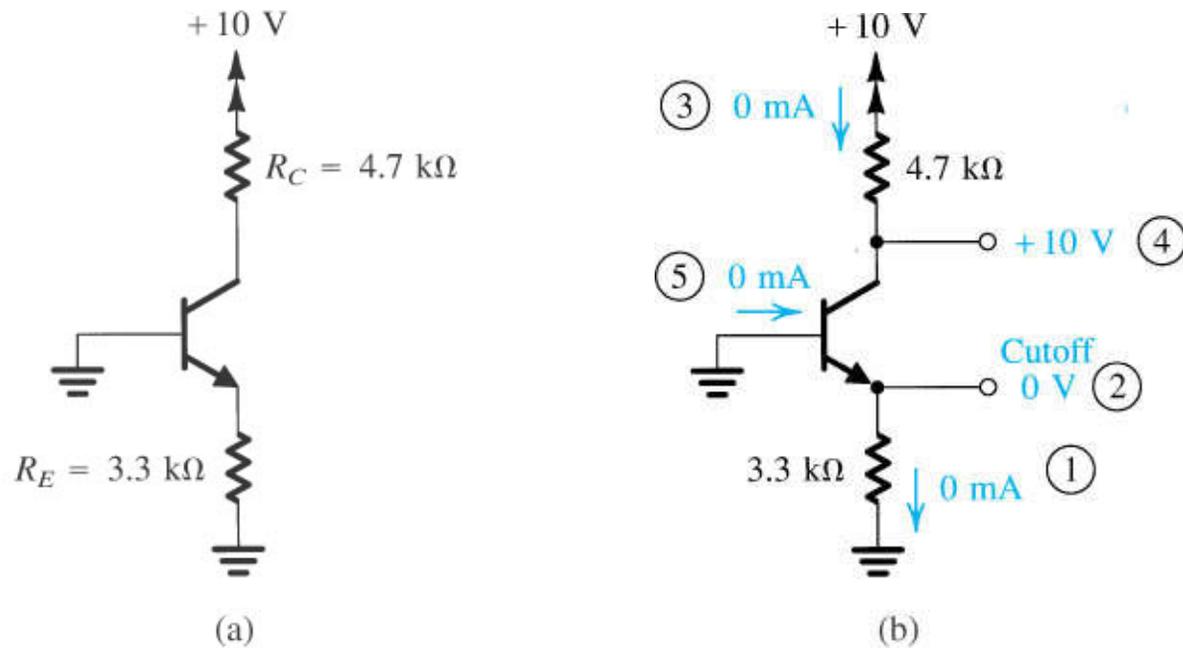
**Figure 5.33** Circuit for Example 5.3.



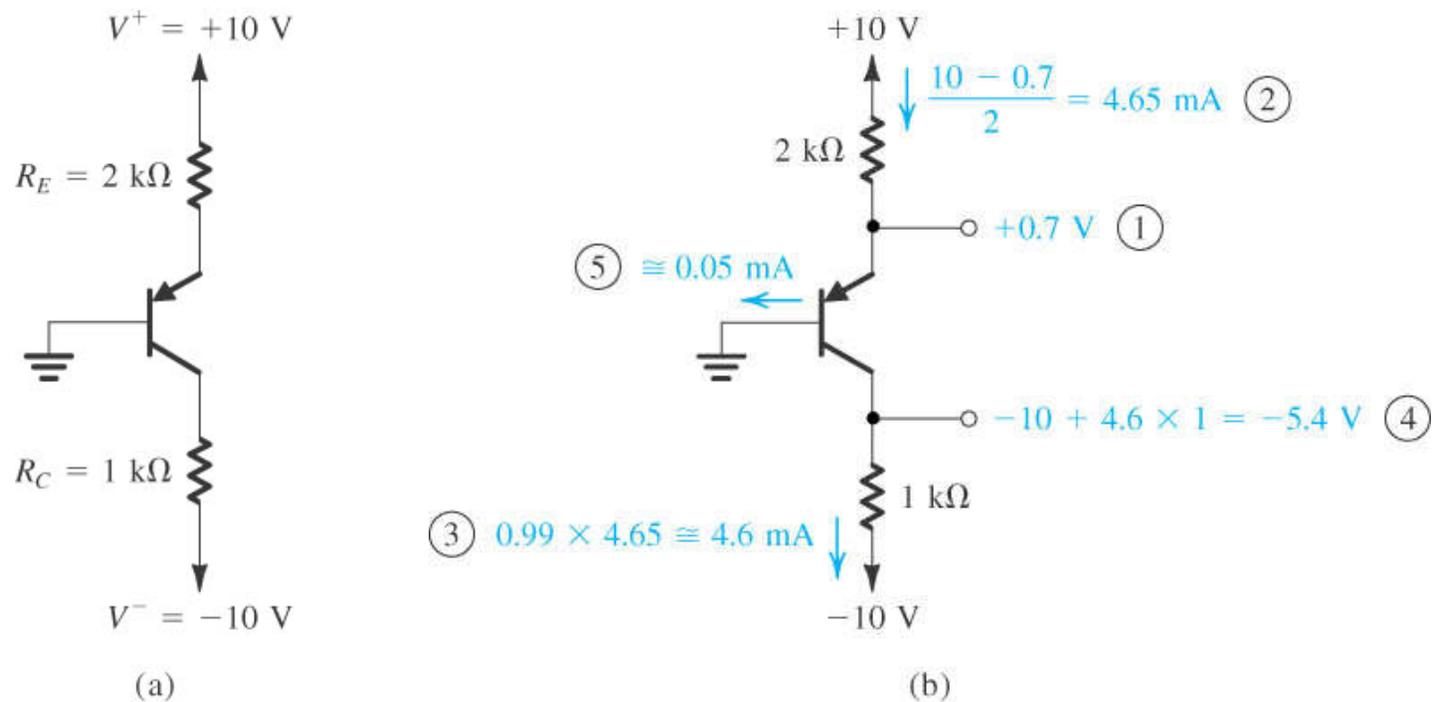
**Figure 5.34** Analysis of the circuit for Example 5.4: (a) circuit; (b) circuit redrawn to remind the reader of the convention used in this book to show connections to the power supply; (c) analysis with the steps numbered.



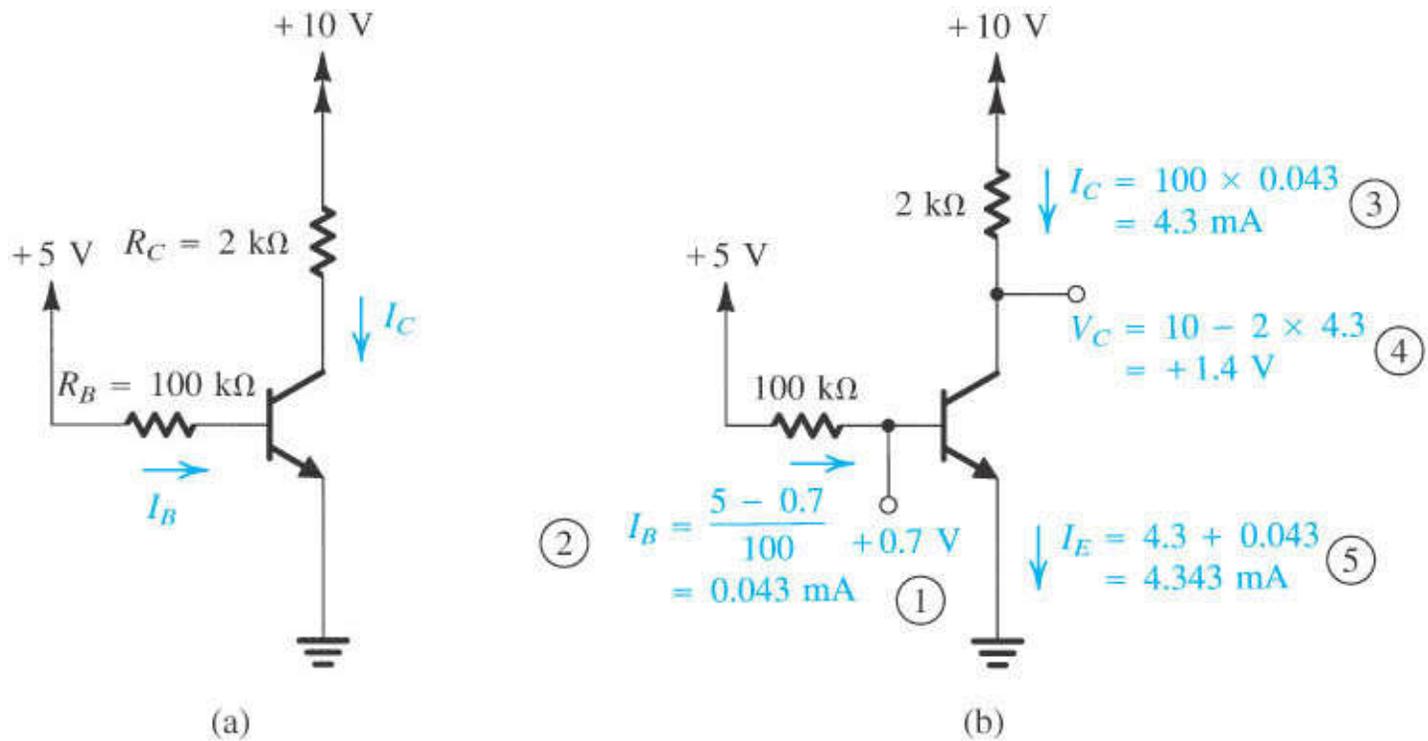
**Figure 5.35** Analysis of the circuit for Example 5.5. Note that the circled numbers indicate the order of the analysis steps.



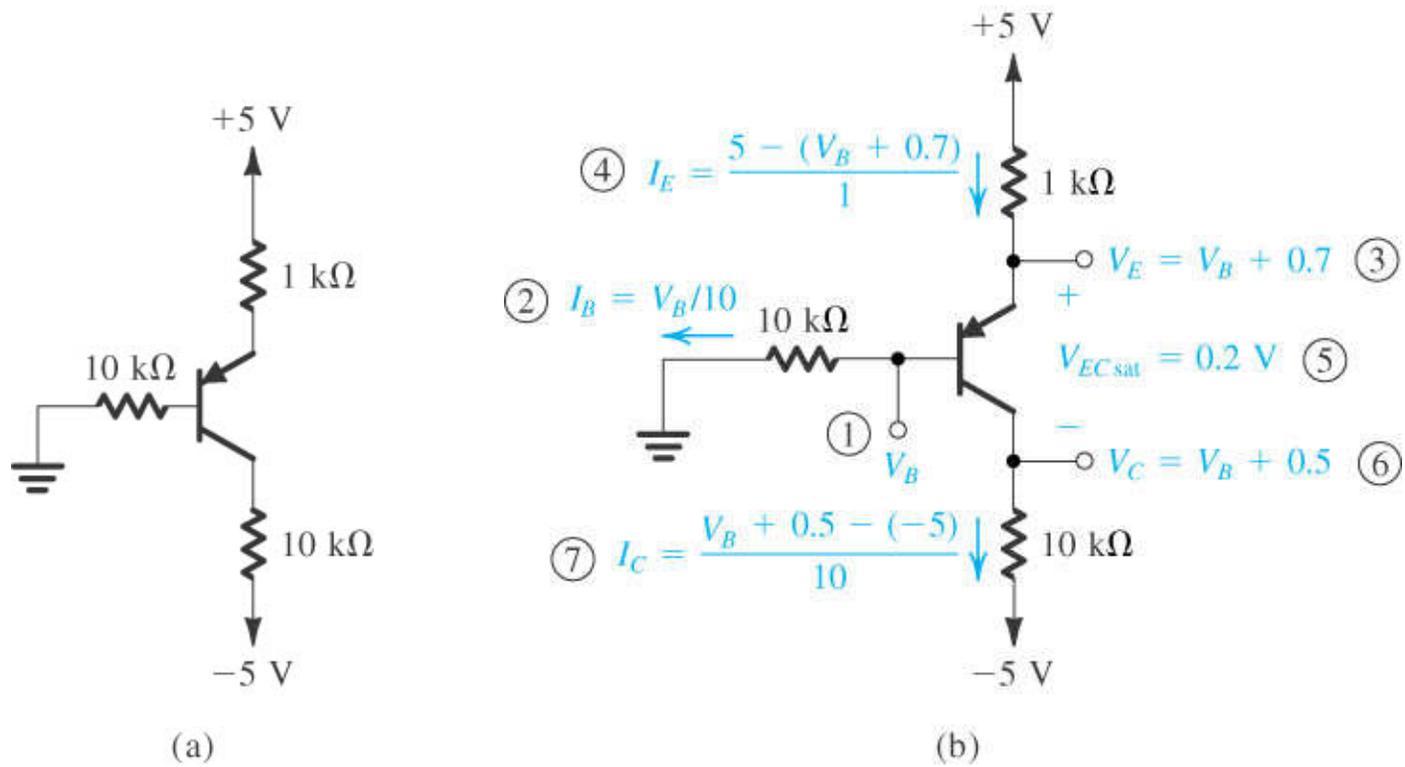
**Figure 5.36** Example 5.6: (a) circuit; (b) analysis with the order of the analysis steps indicated by circled numbers.



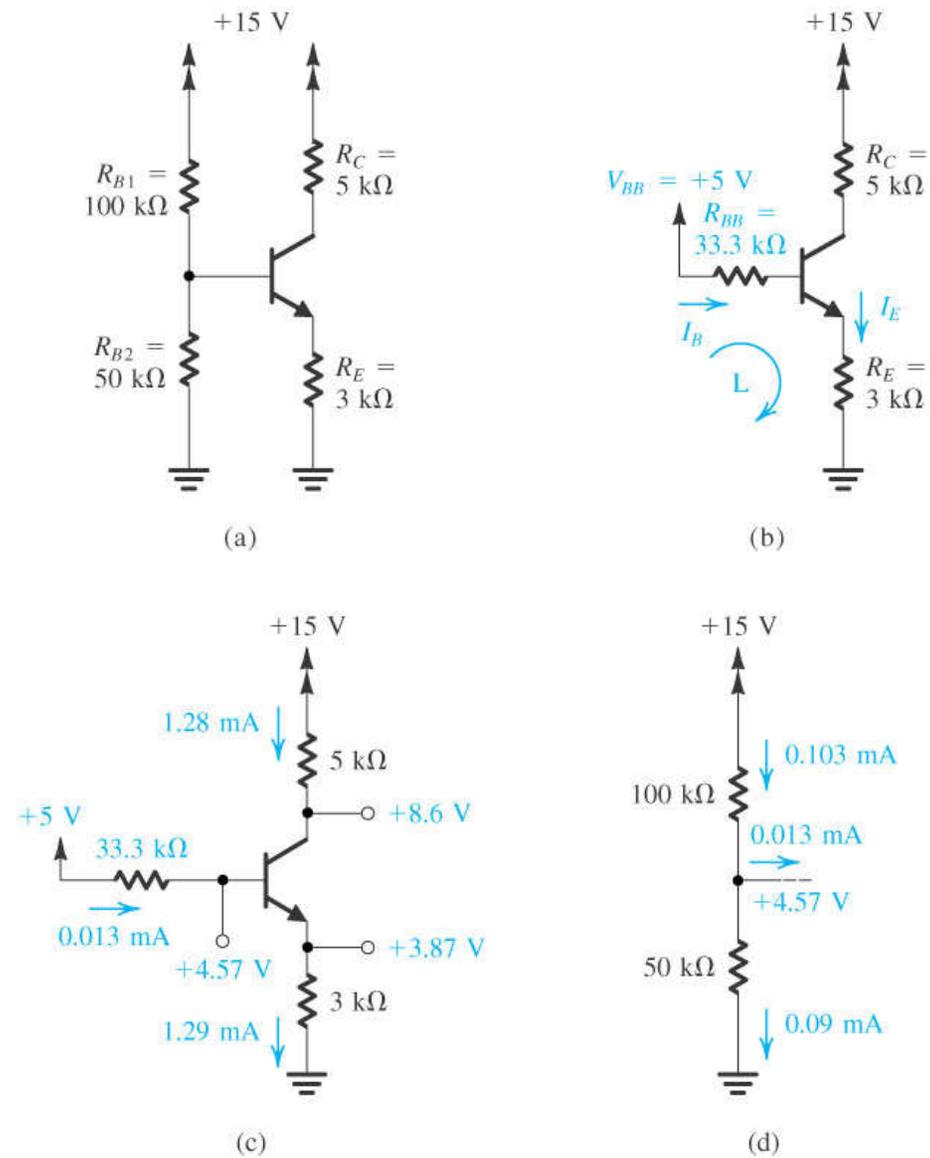
**Figure 5.37** Example 5.7: (a) circuit; (b) analysis with the steps indicated by circled numbers.



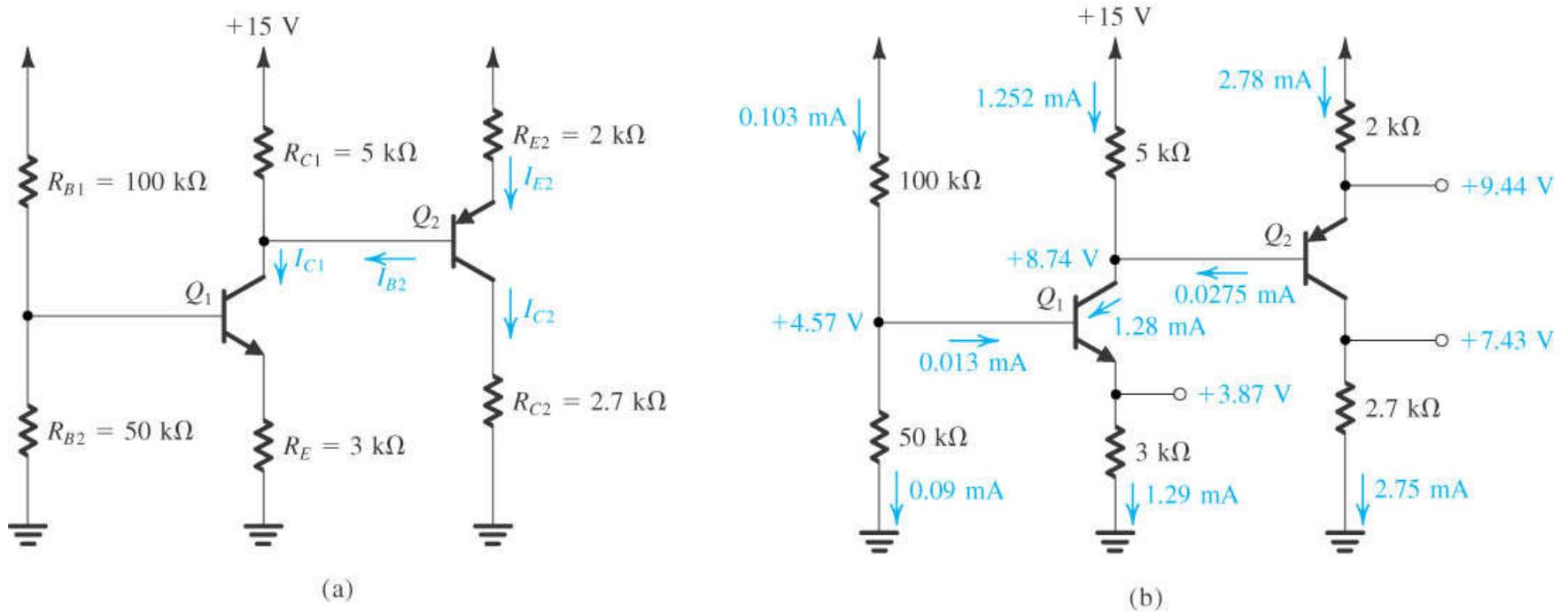
**Figure 5.38** Example 5.8: (a) circuit; (b) analysis with the steps indicated by the circled numbers.



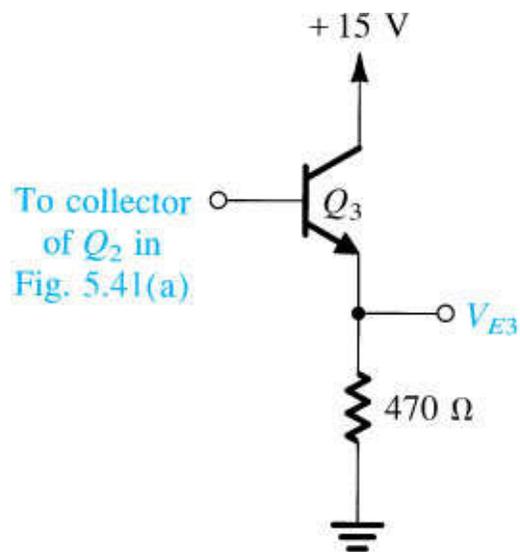
**Figure 5.39** Example 5.9: (a) circuit; (b) analysis with steps numbered.



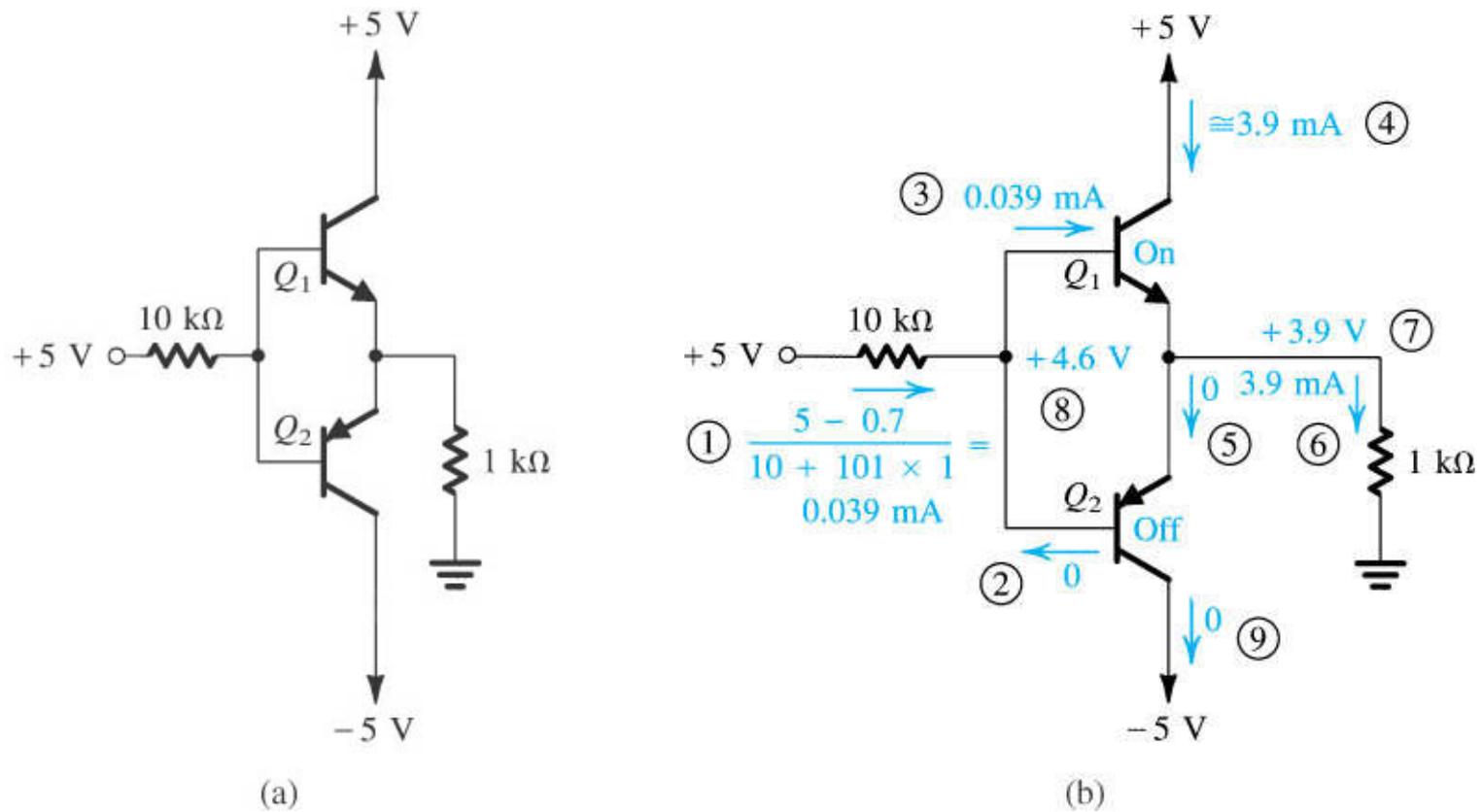
**Figure 5.40** Circuits for Example 5.10.



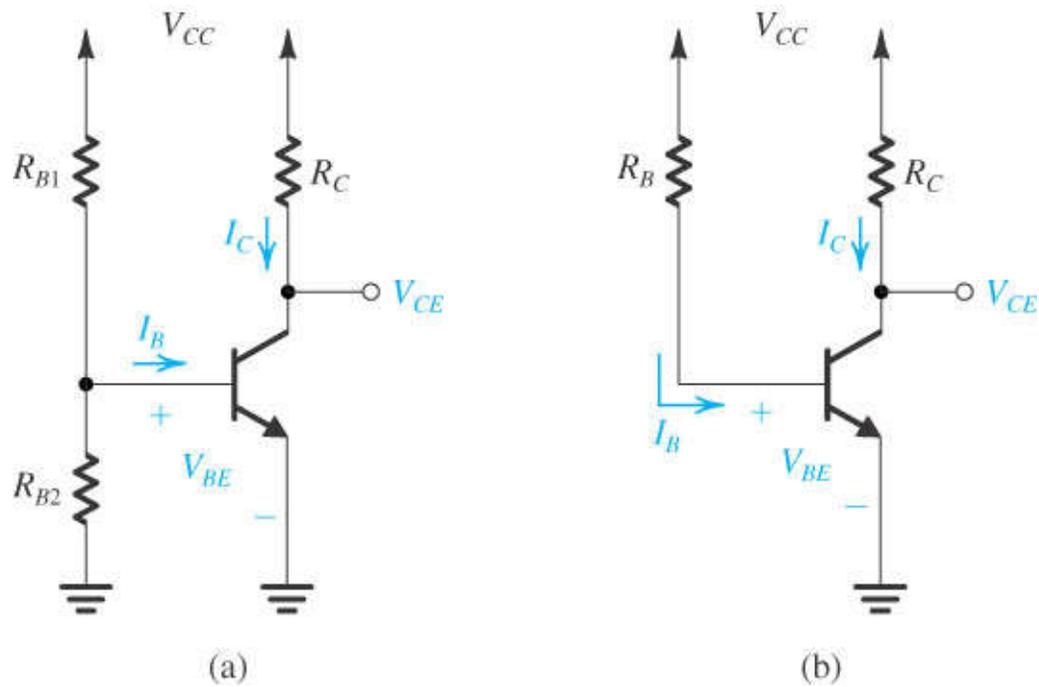
**Figure 5.41** Circuits for Example 5.11.



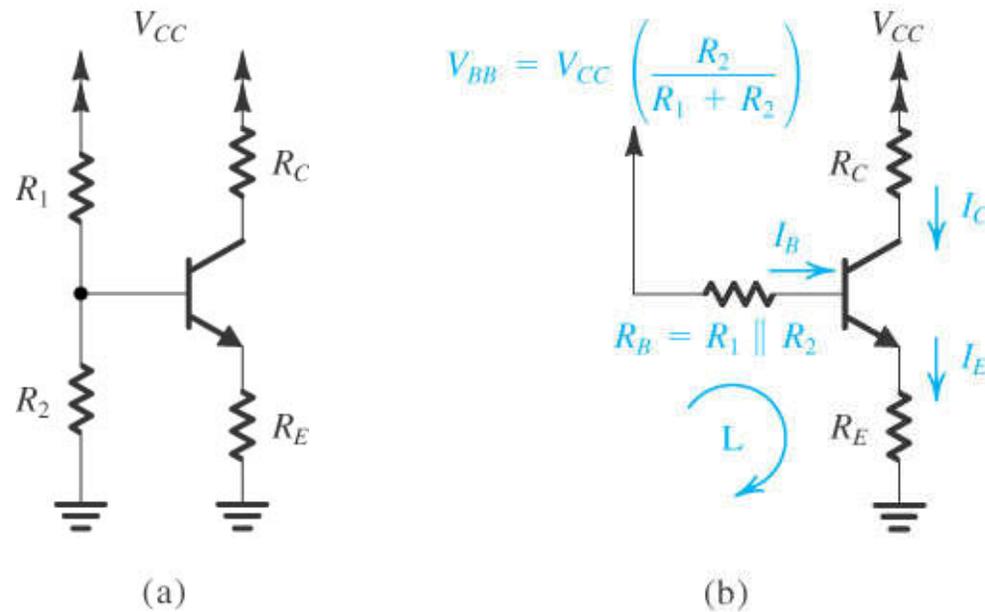
**Figure E5.30**



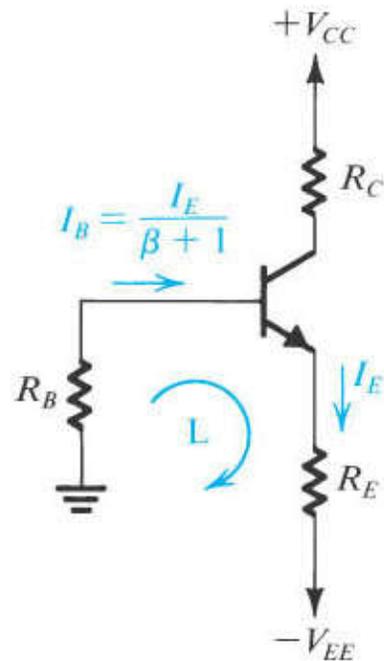
**Figure 5.42** Example 5.12: (a) circuit; (b) analysis with the steps numbered.



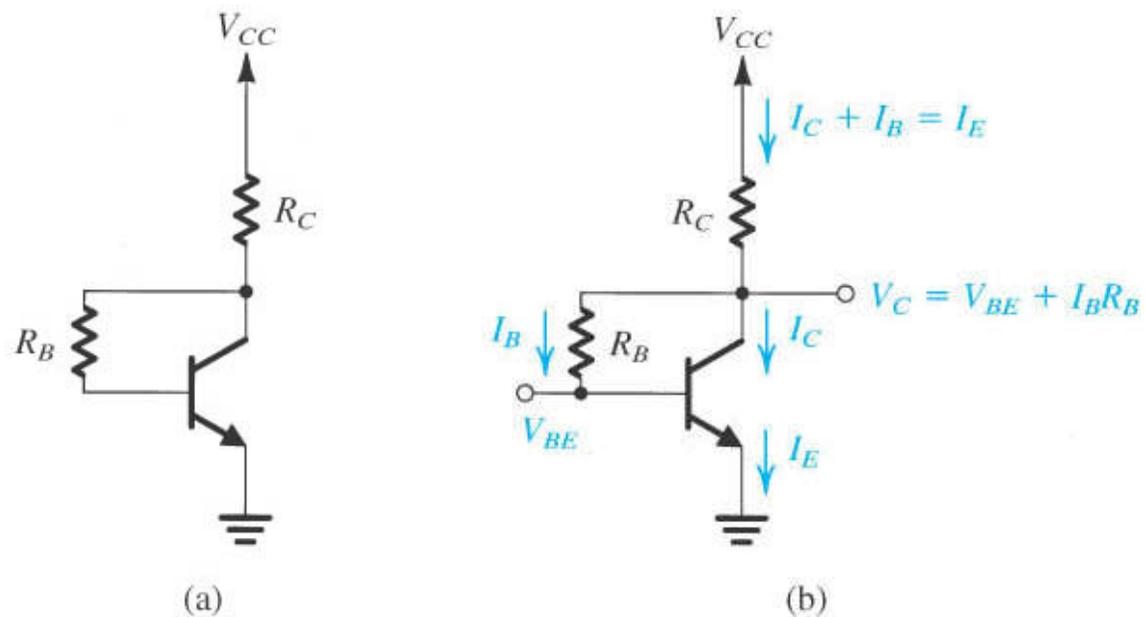
**Figure 5.43** Two obvious schemes for biasing the BJT: **(a)** by fixing  $V_{BE}$ ; **(b)** by fixing  $I_B$ . Both result in wide variations in  $I_C$  and hence in  $V_{CE}$  and therefore are considered to be “bad.” Neither scheme is recommended.



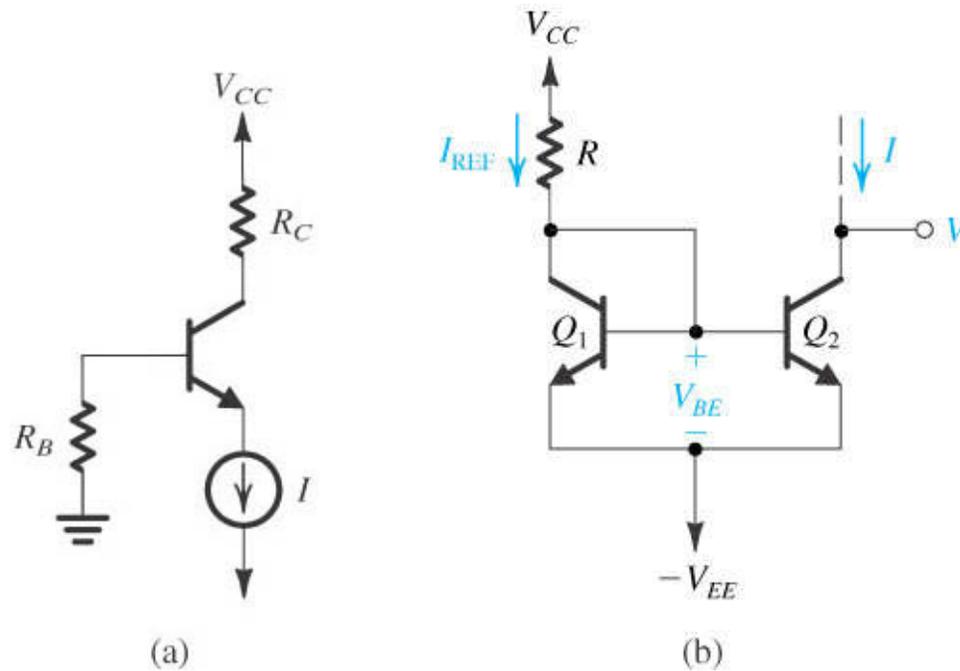
**Figure 5.44** Classical biasing for BJTs using a single power supply: **(a)** circuit; **(b)** circuit with the voltage divider supplying the base replaced with its Thévenin equivalent.



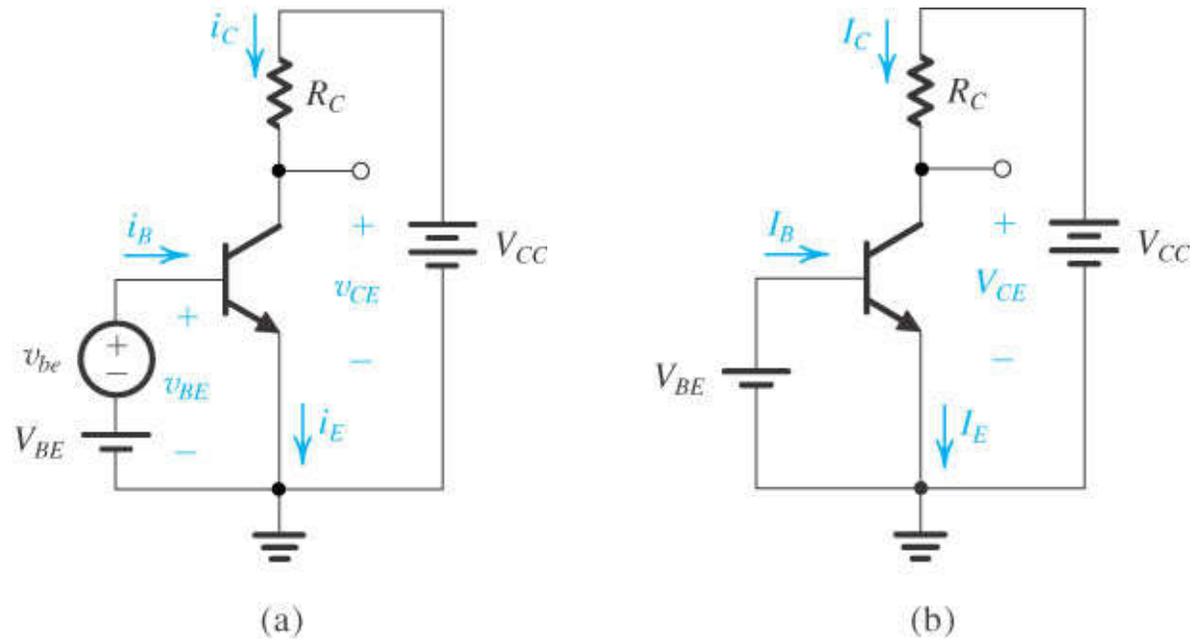
**Figure 5.45** Biasing the BJT using two power supplies. Resistor  $R_B$  is needed only if the signal is to be capacitively coupled to the base. Otherwise, the base can be connected directly to ground, or to a grounded signal source, resulting in almost total  $\beta$ -independence of the bias current.



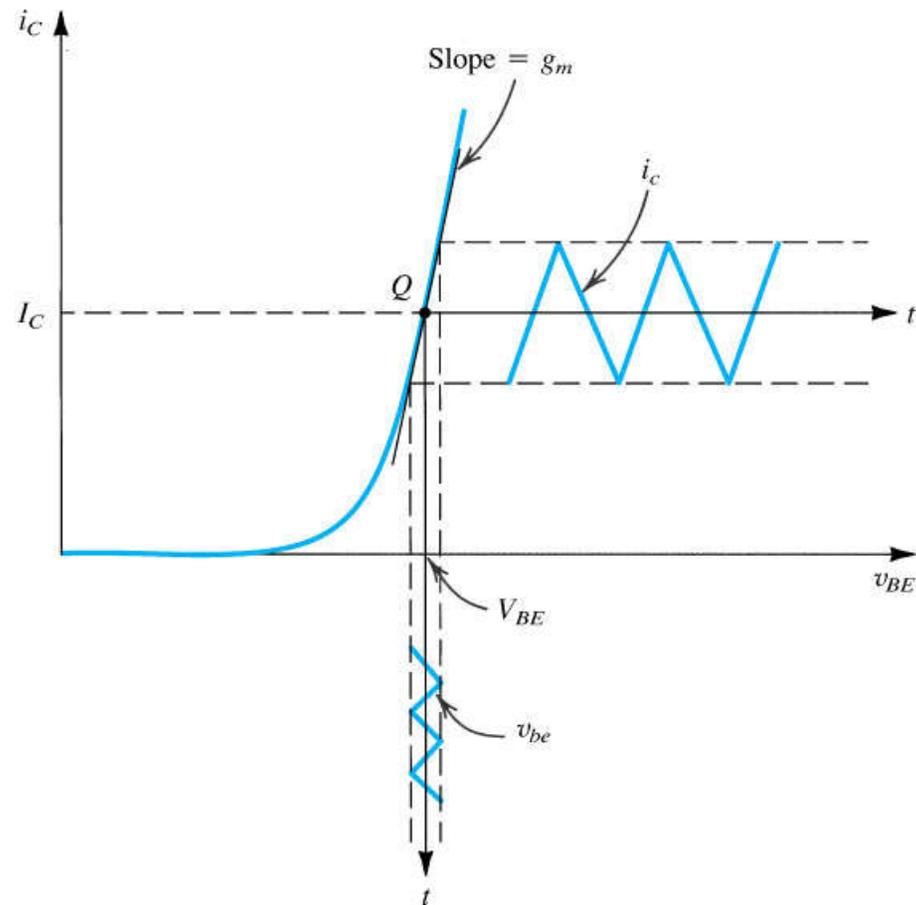
**Figure 5.46** (a) A common-emitter transistor amplifier biased by a feedback resistor  $R_B$ . (b) Analysis of the circuit in (a).



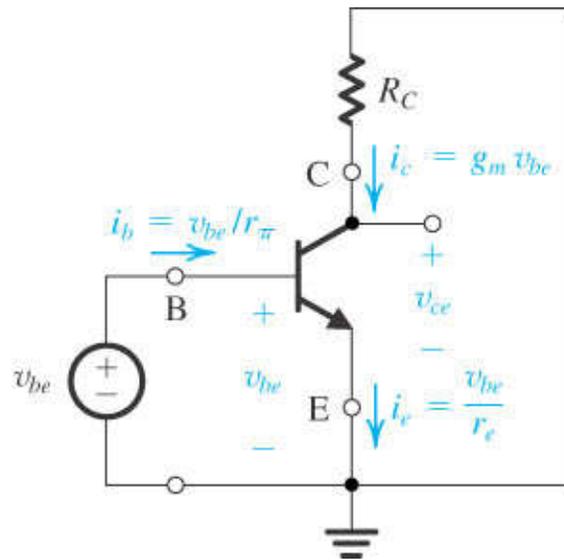
**Figure 5.47** (a) A BJT biased using a constant-current source  $I$ . (b) Circuit for implementing the current source  $I$ .



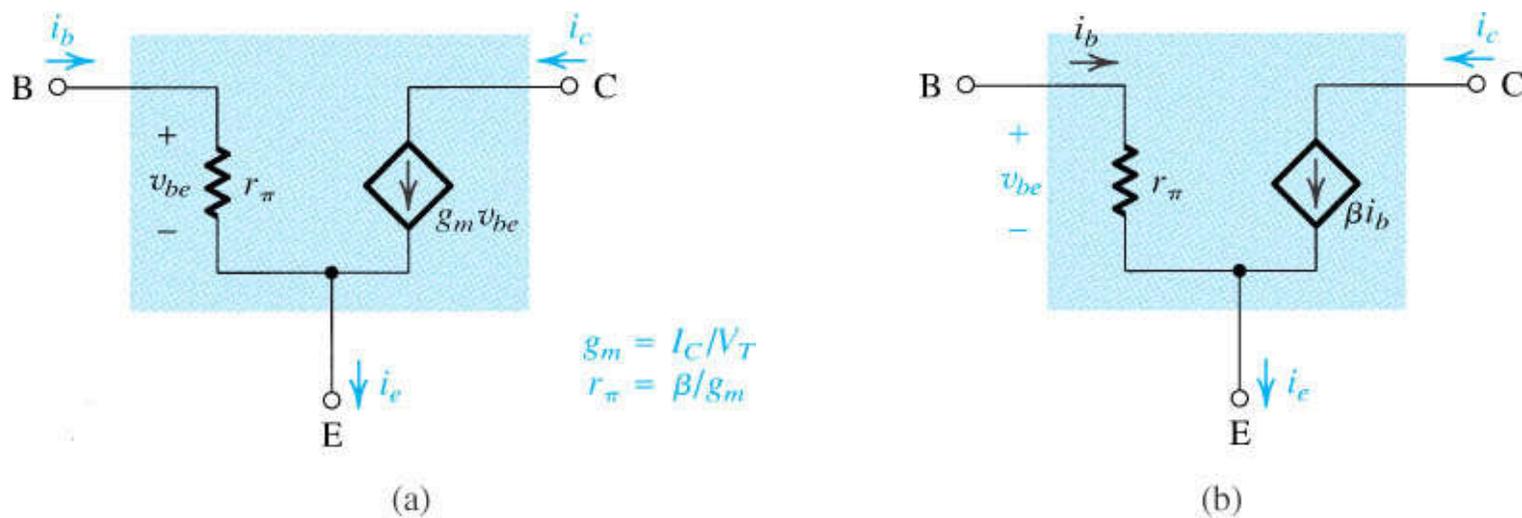
**Figure 5.48** (a) Conceptual circuit to illustrate the operation of the transistor as an amplifier. (b) The circuit of (a) with the signal source  $v_{be}$  eliminated for dc (bias) analysis.



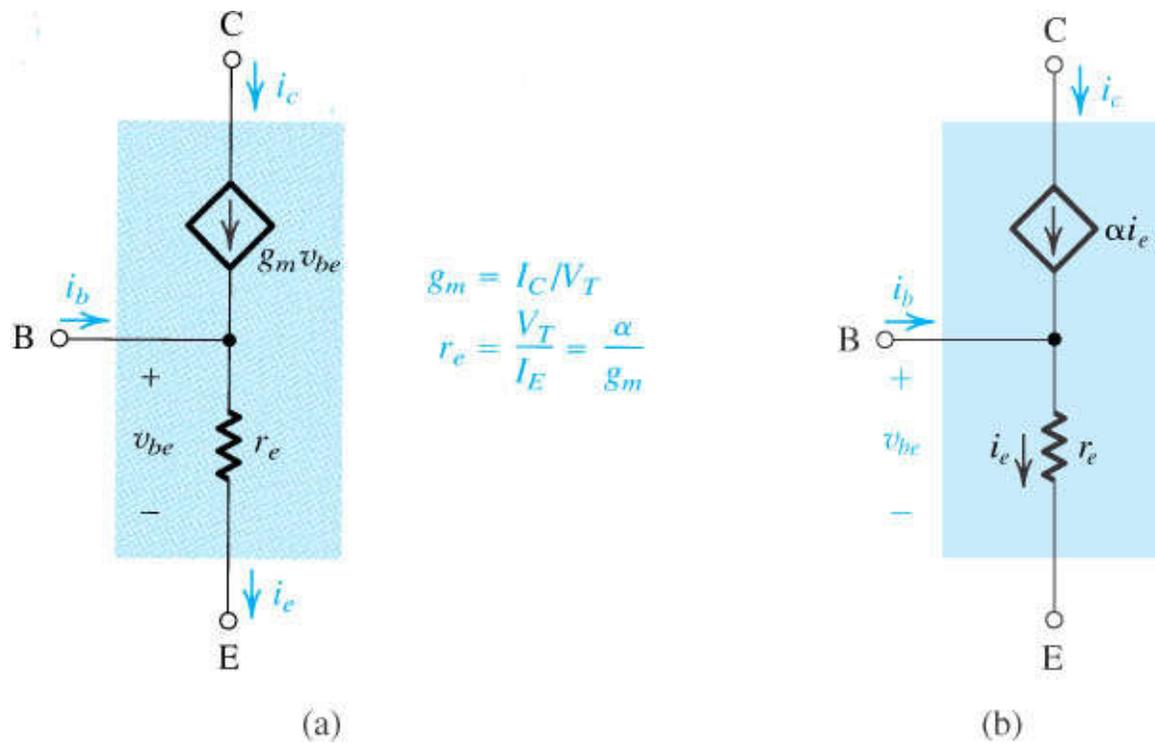
**Figure 5.49** Linear operation of the transistor under the small-signal condition: A small signal  $v_{be}$  with a triangular waveform is superimposed on the dc voltage  $V_{BE}$ . It gives rise to a collector signal current  $i_c$ , also of triangular waveform, superimposed on the dc current  $I_C$ . Here,  $i_c = g_m v_{be}$ , where  $g_m$  is the slope of the  $i_c$ - $v_{BE}$  curve at the bias point  $Q$ .



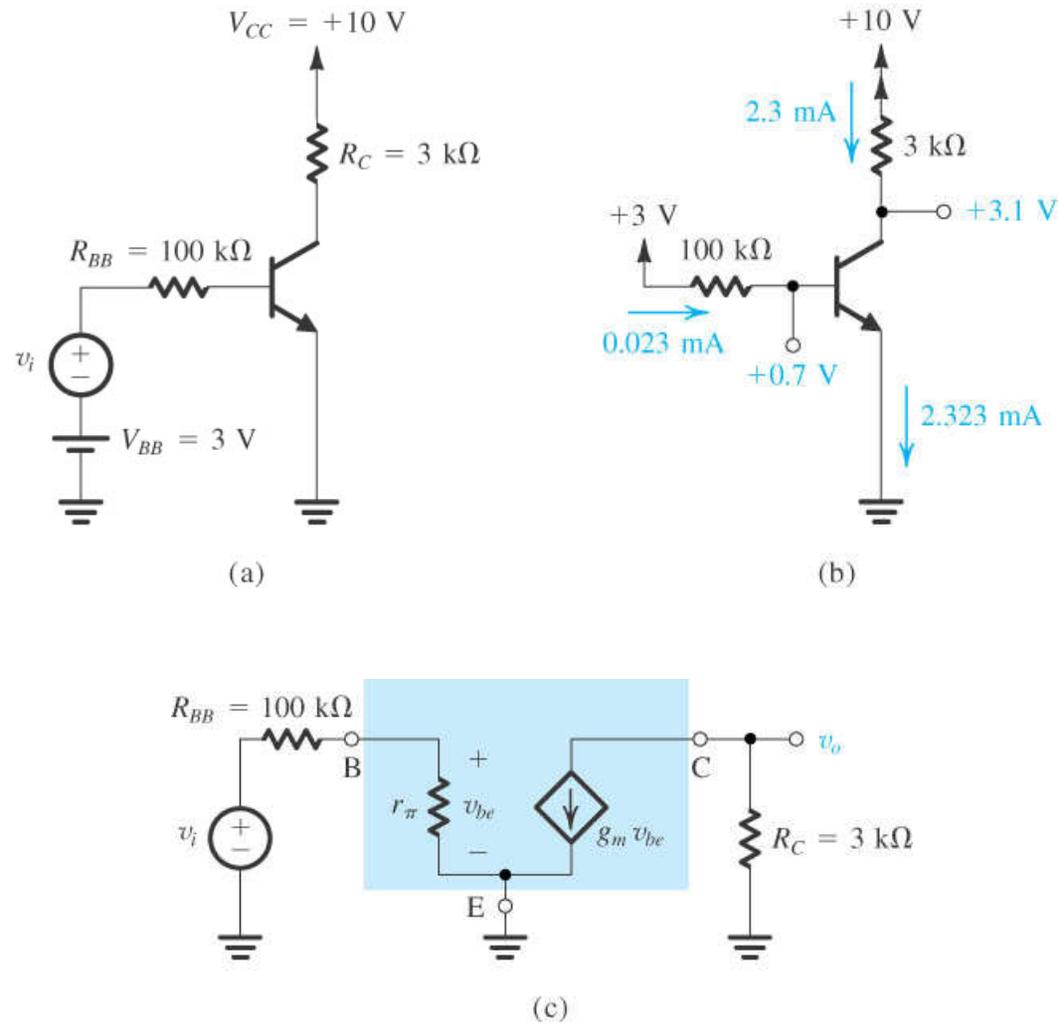
**Figure 5.50** The amplifier circuit of Fig. 5.48(a) with the dc sources ( $V_{BE}$  and  $V_{CC}$ ) eliminated (short circuited). Thus only the signal components are present. Note that this is a representation of the signal operation of the BJT and not an actual amplifier circuit.



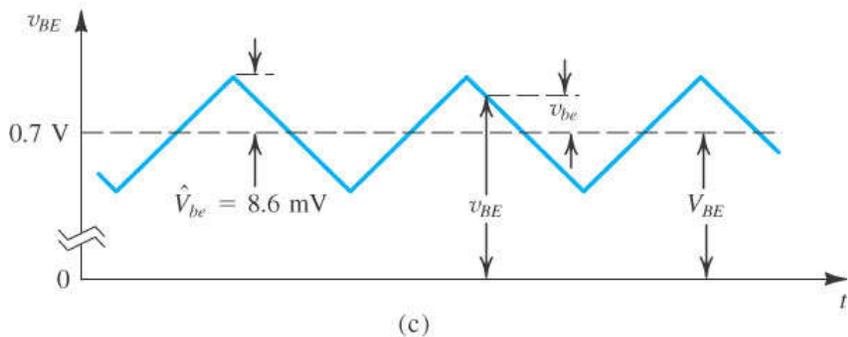
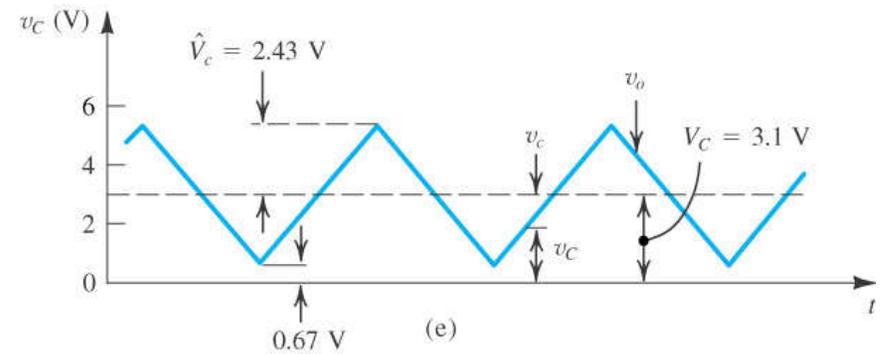
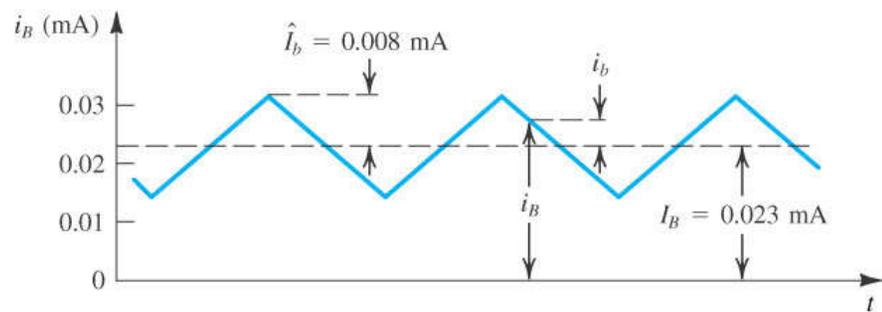
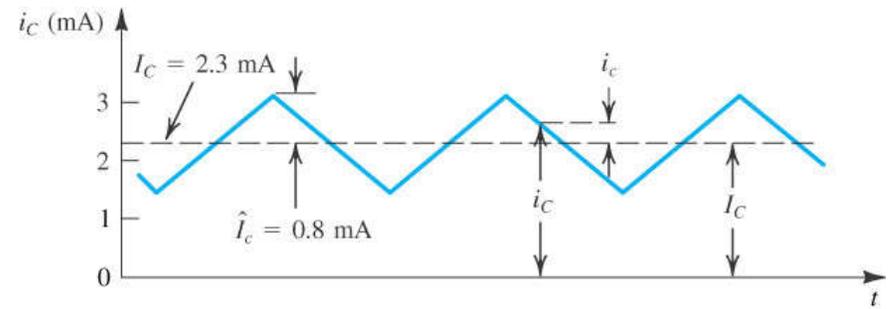
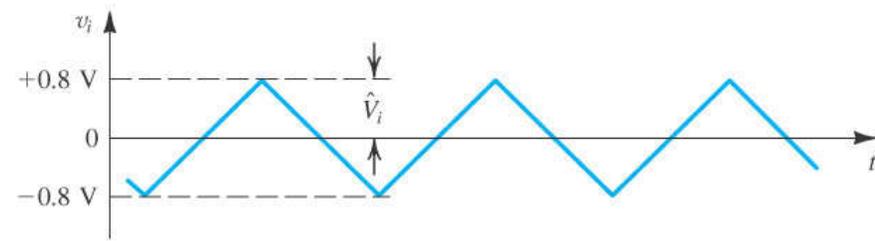
**Figure 5.51** Two slightly different versions of the simplified hybrid- $\pi$  model for the small-signal operation of the BJT. The equivalent circuit in **(a)** represents the BJT as a voltage-controlled current source (a transconductance amplifier), and that in **(b)** represents the BJT as a current-controlled current source (a current amplifier).



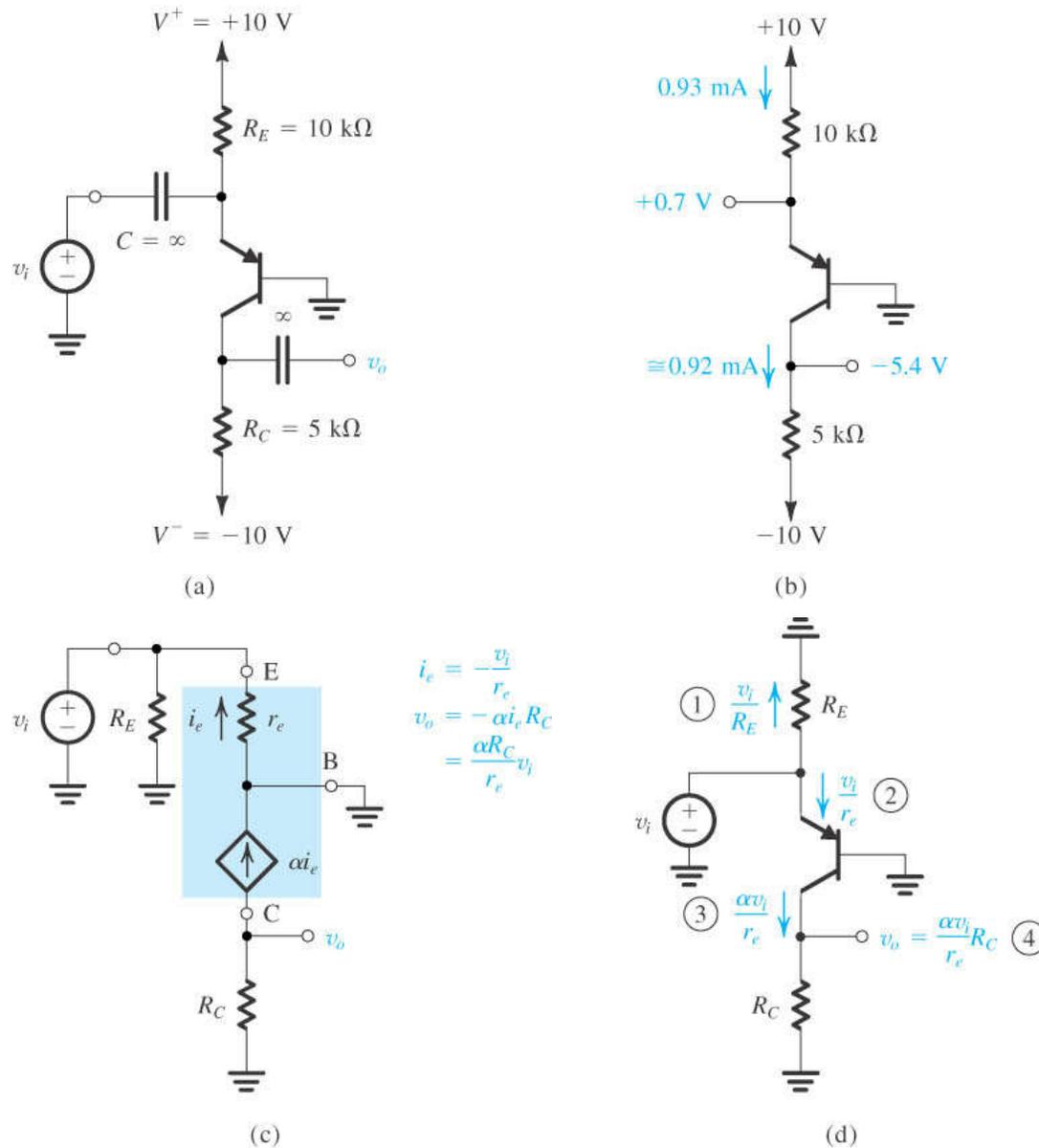
**Figure 5.52** Two slightly different versions of what is known as the *T model* of the BJT. The circuit in (a) is a voltage-controlled current source representation and that in (b) is a current-controlled current source representation. These models explicitly show the emitter resistance  $r_e$  rather than the base resistance  $r_\pi$  featured in the hybrid- $\pi$  model.



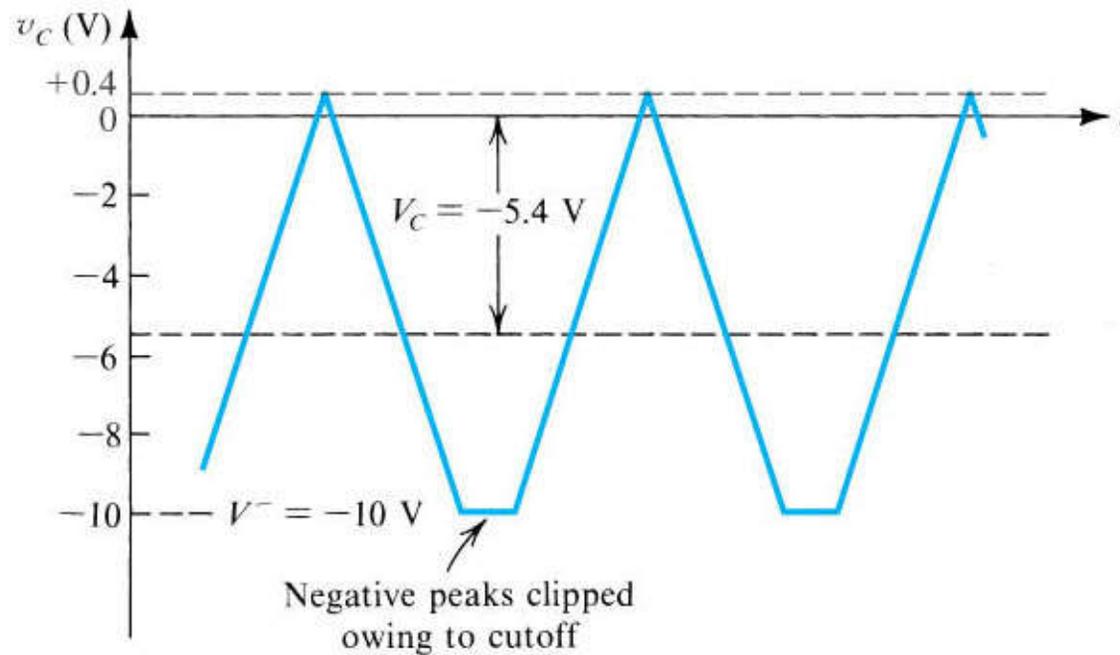
**Figure 5.53** Example 5.14: (a) circuit; (b) dc analysis; (c) small-signal model.



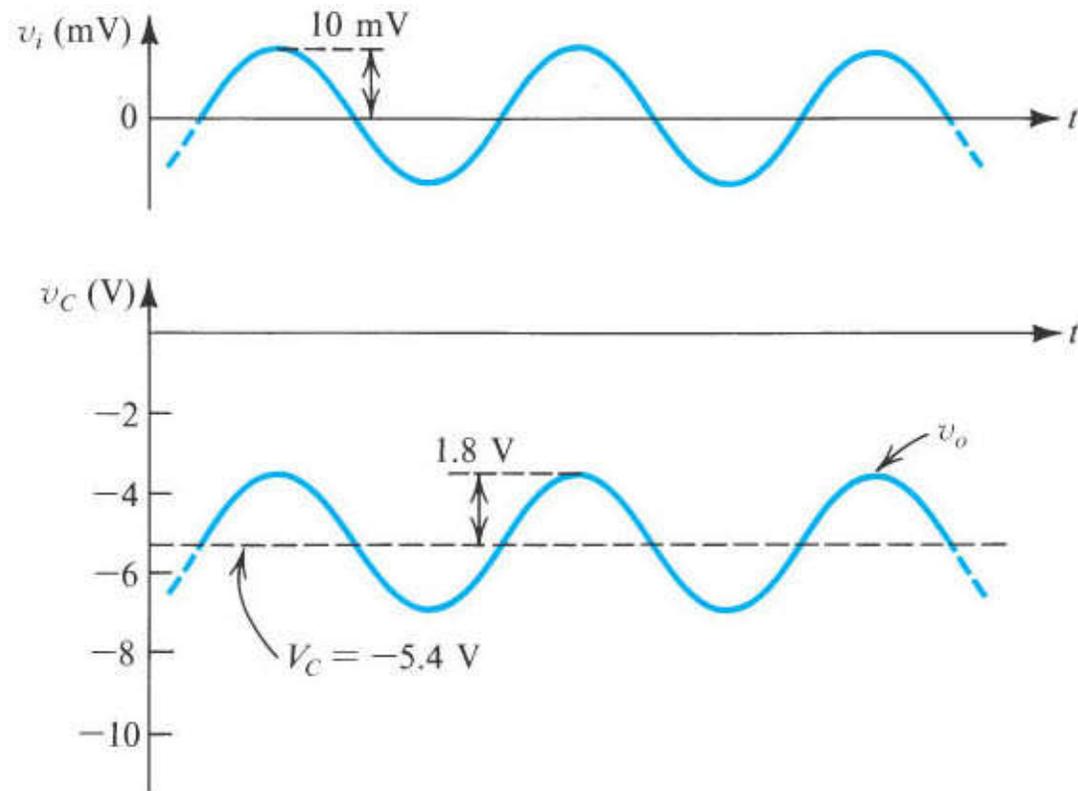
**Figure 5.54** Signal waveforms in the circuit of Fig. 5.53.



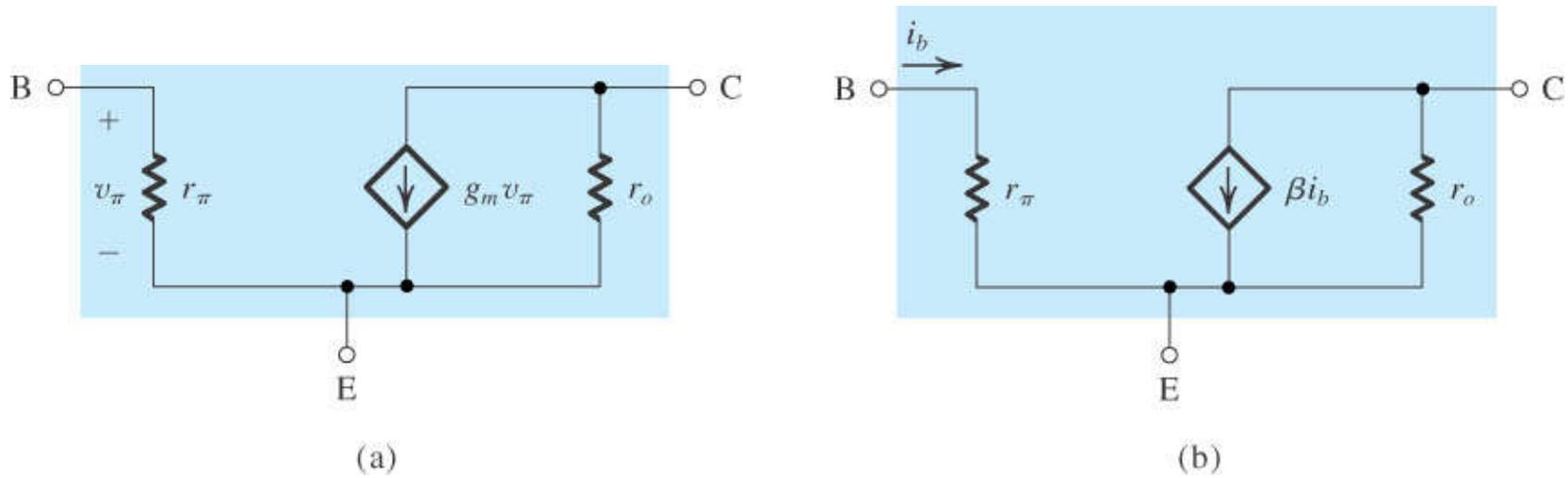
**Figure 5.55** Example 5.16: **(a)** circuit; **(b)** dc analysis; **(c)** small-signal model; **(d)** small-signal analysis performed directly on the circuit.



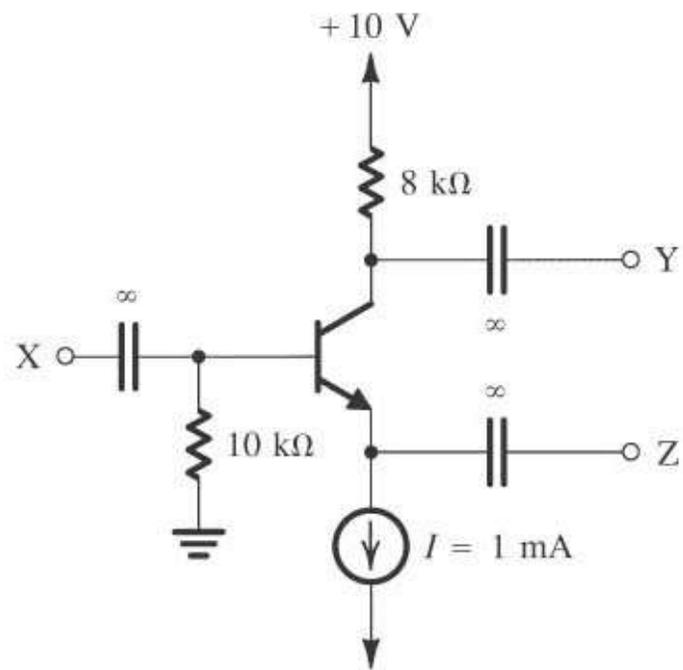
**Figure 5.56** Distortion in output signal due to transistor cutoff. Note that it is assumed that no distortion due to the transistor nonlinear characteristics is occurring.



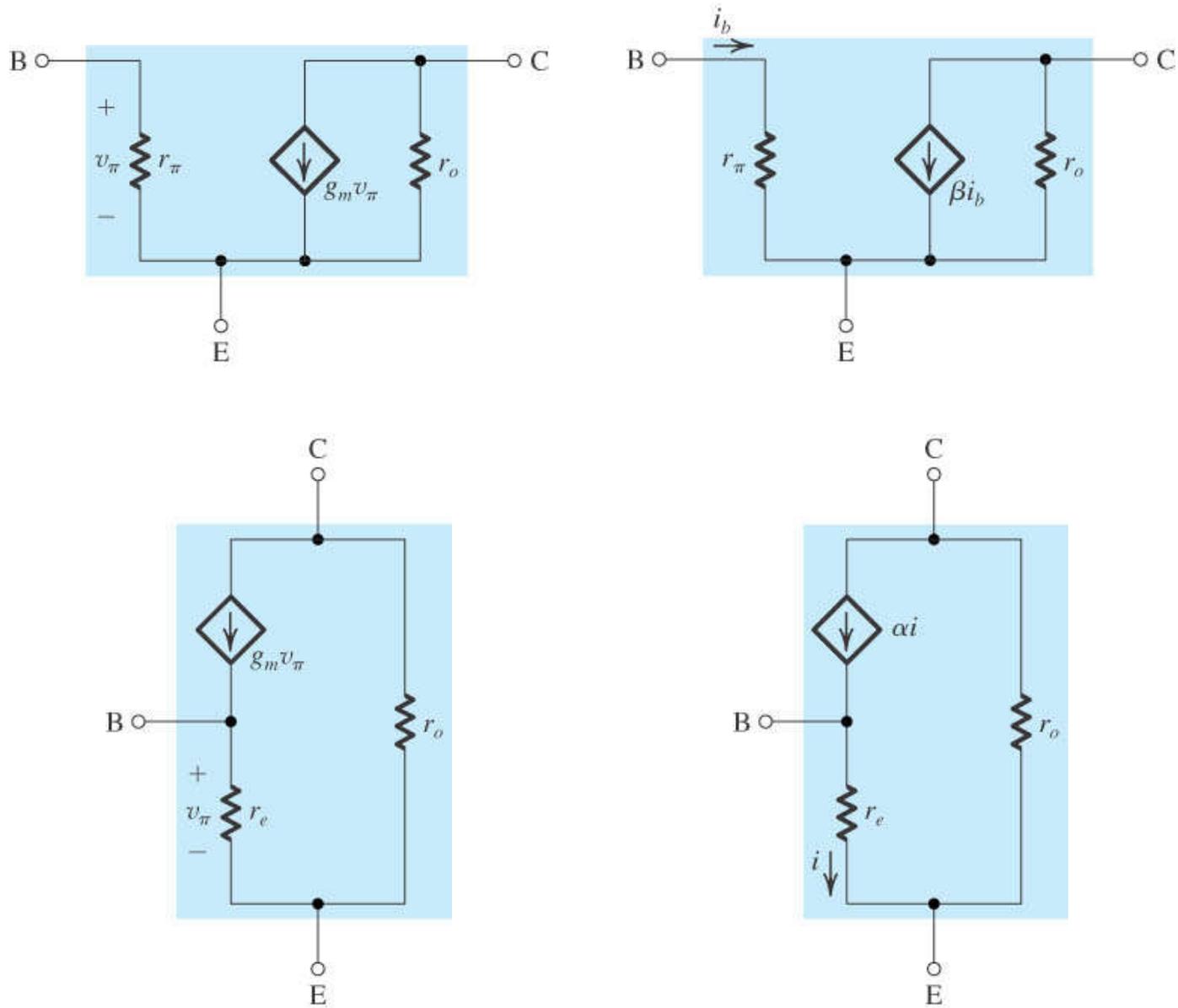
**Figure 5.57** Input and output waveforms for the circuit of Fig. 5.55. Observe that this amplifier is noninverting, a property of the common-base configuration.



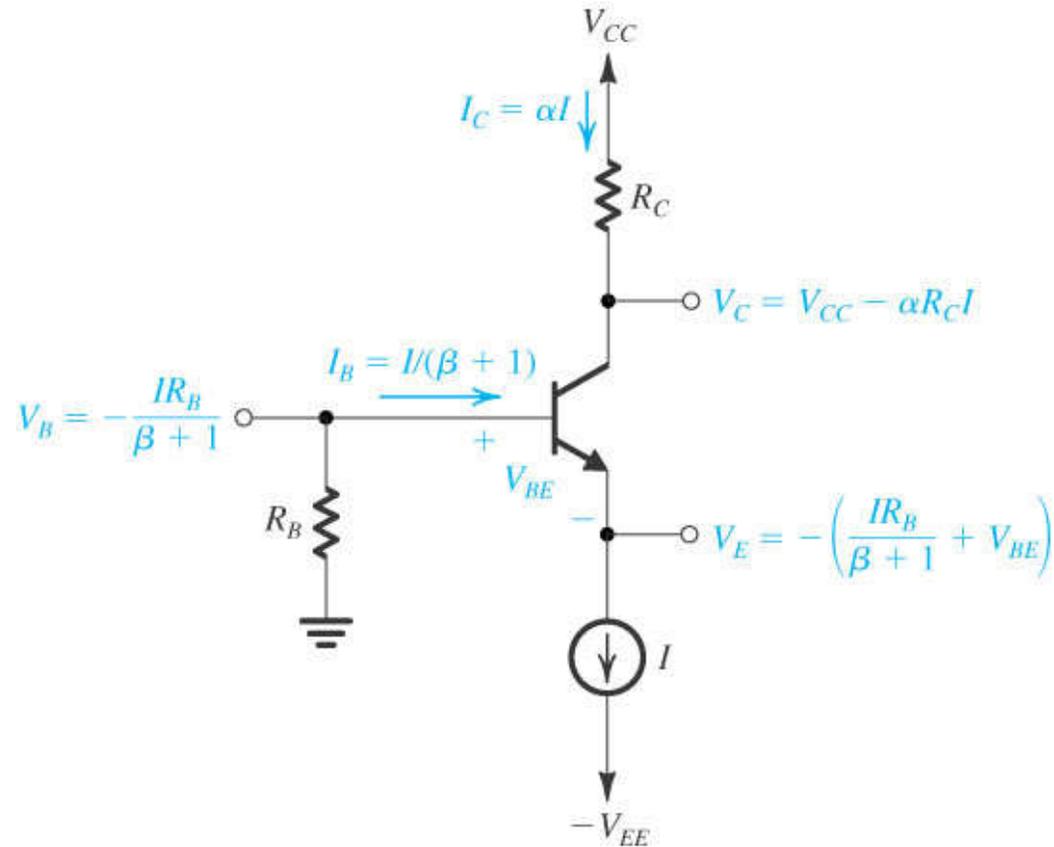
**Figure 5.58** The hybrid- $\pi$  small-signal model, in its two versions, with the resistance  $r_o$  included.



**Figure E5.40**



**Table 5.4**



**Figure 5.59** Basic structure of the circuit used to realize single-stage, discrete-circuit BJT amplifier configurations.

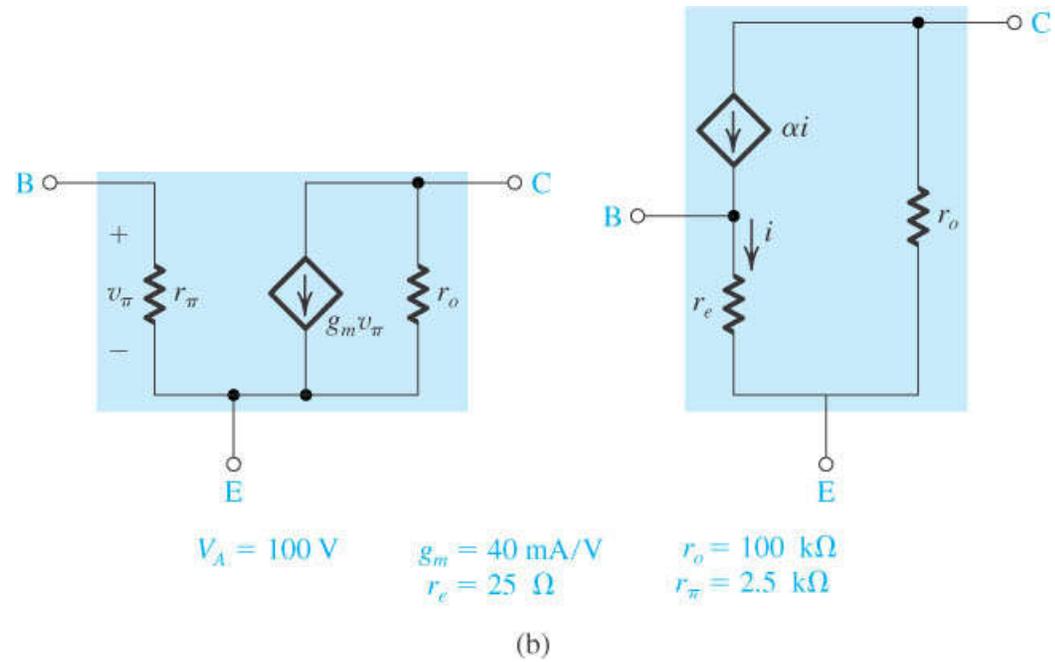
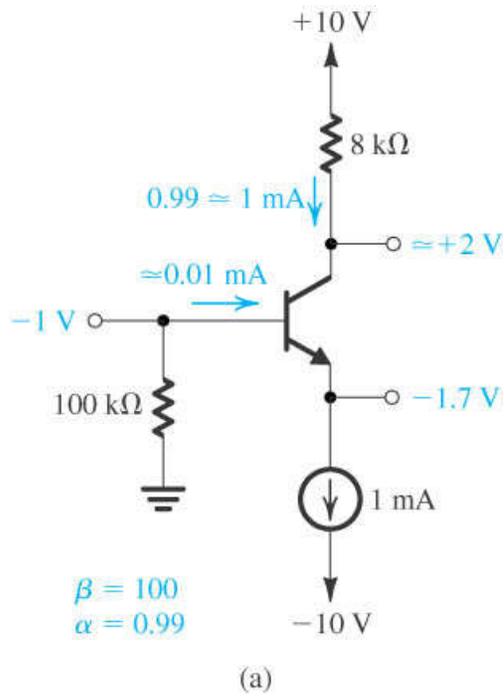
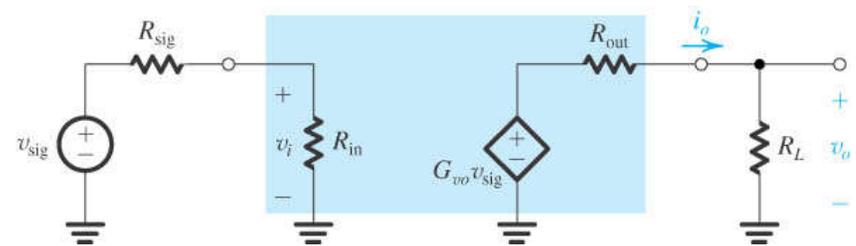
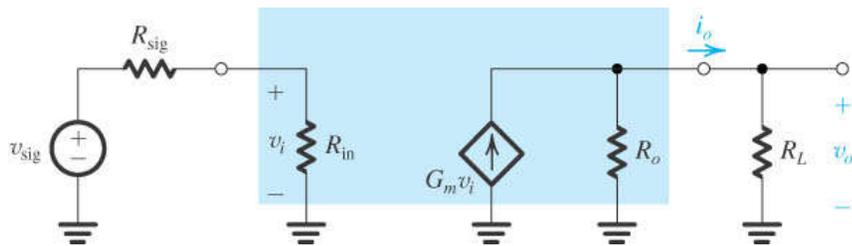
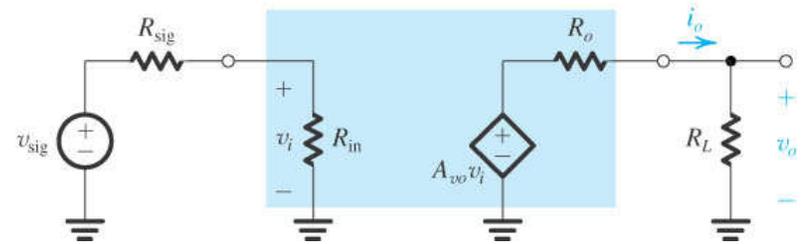
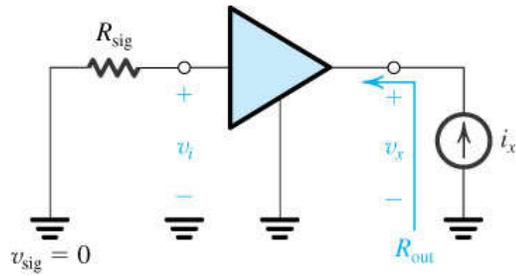
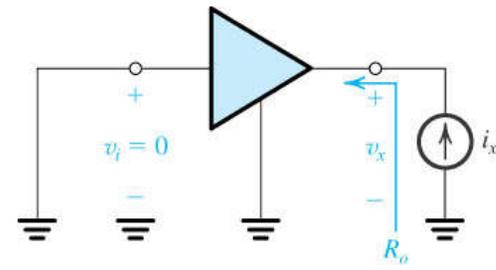
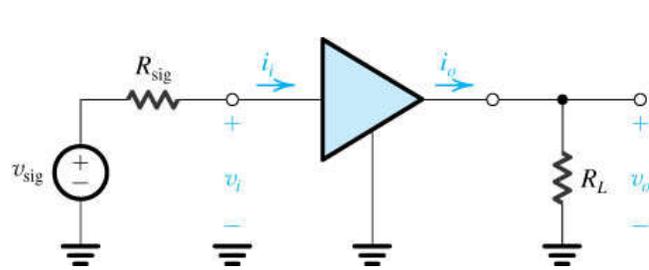
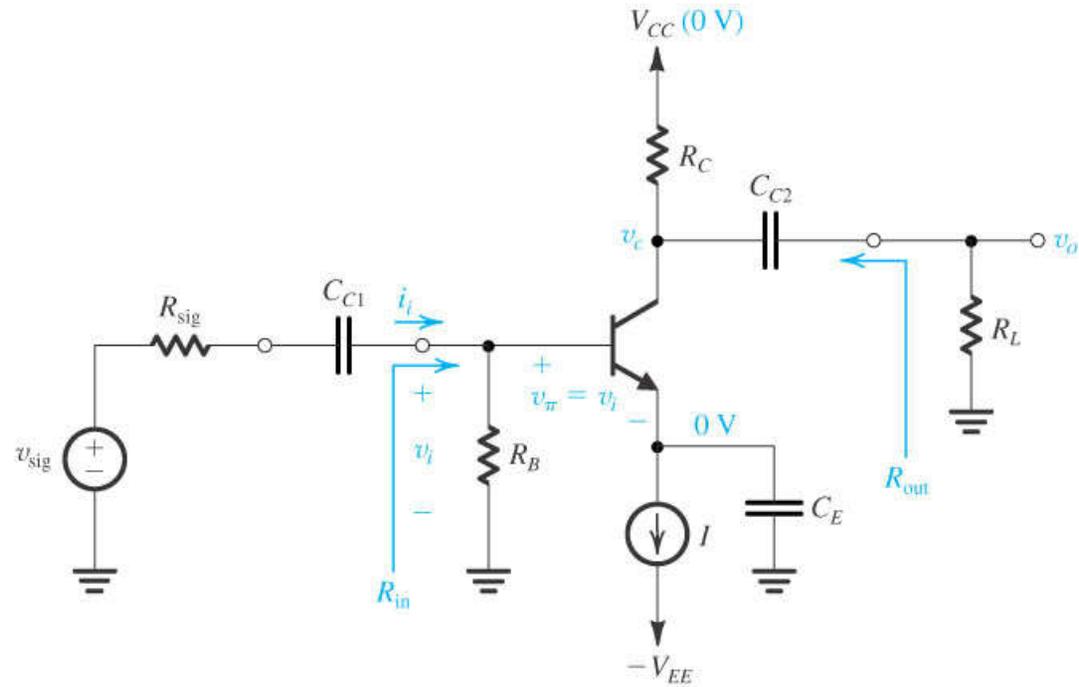


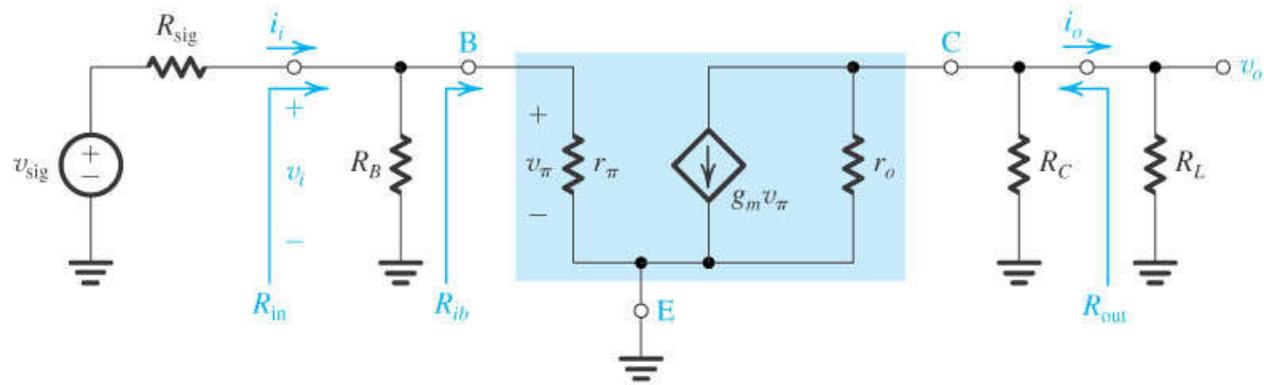
Figure E5.41



**Table 5.5**

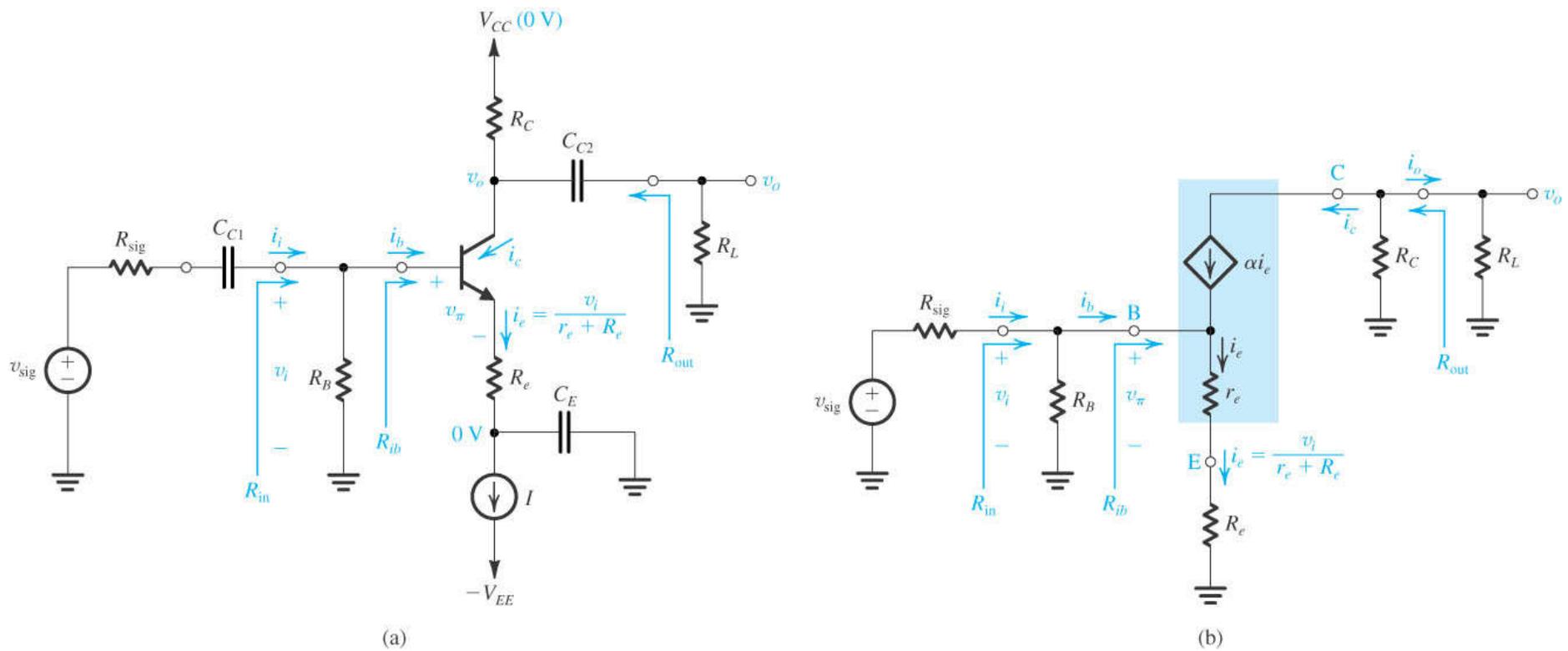


(a)

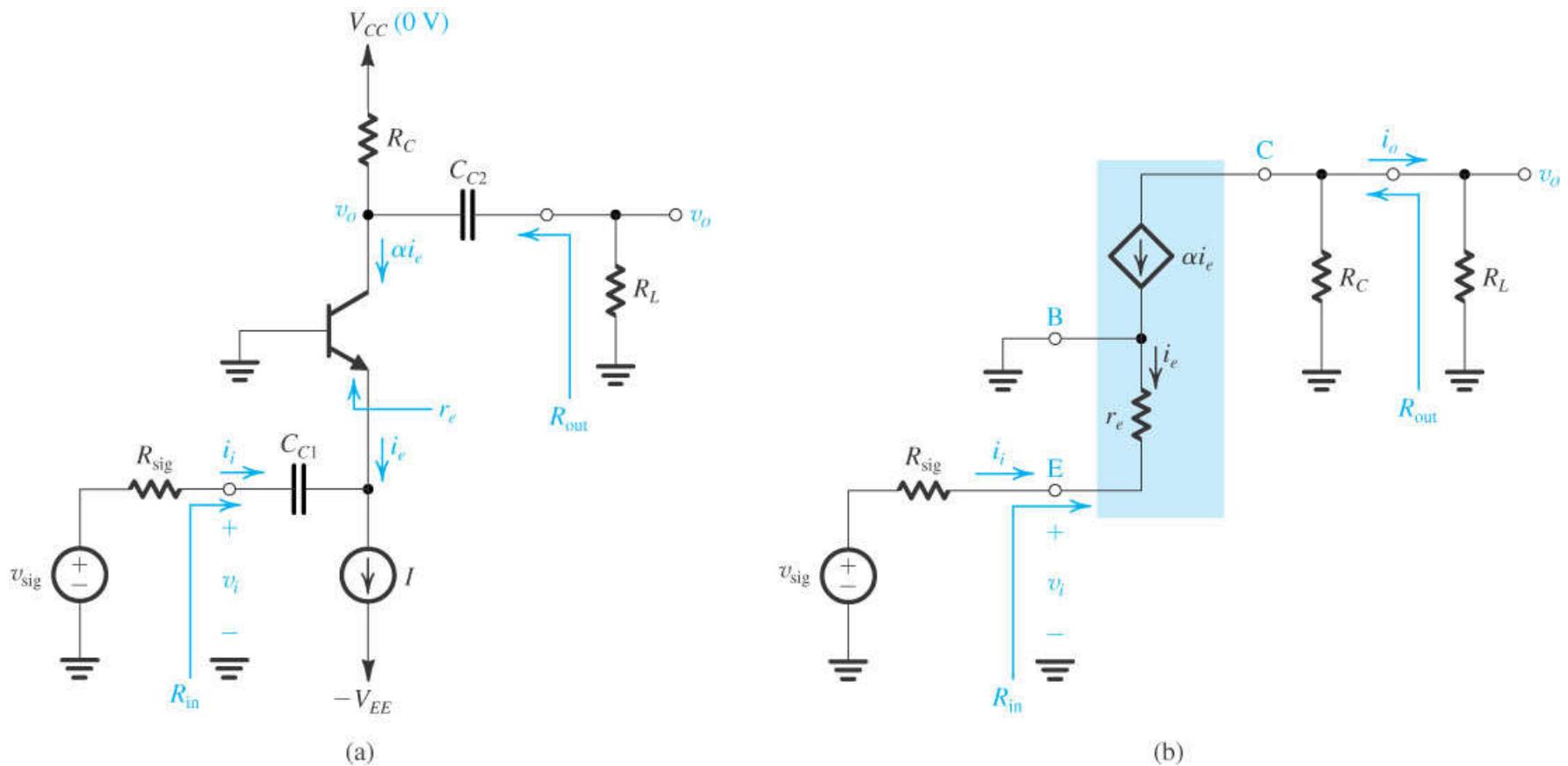


(b)

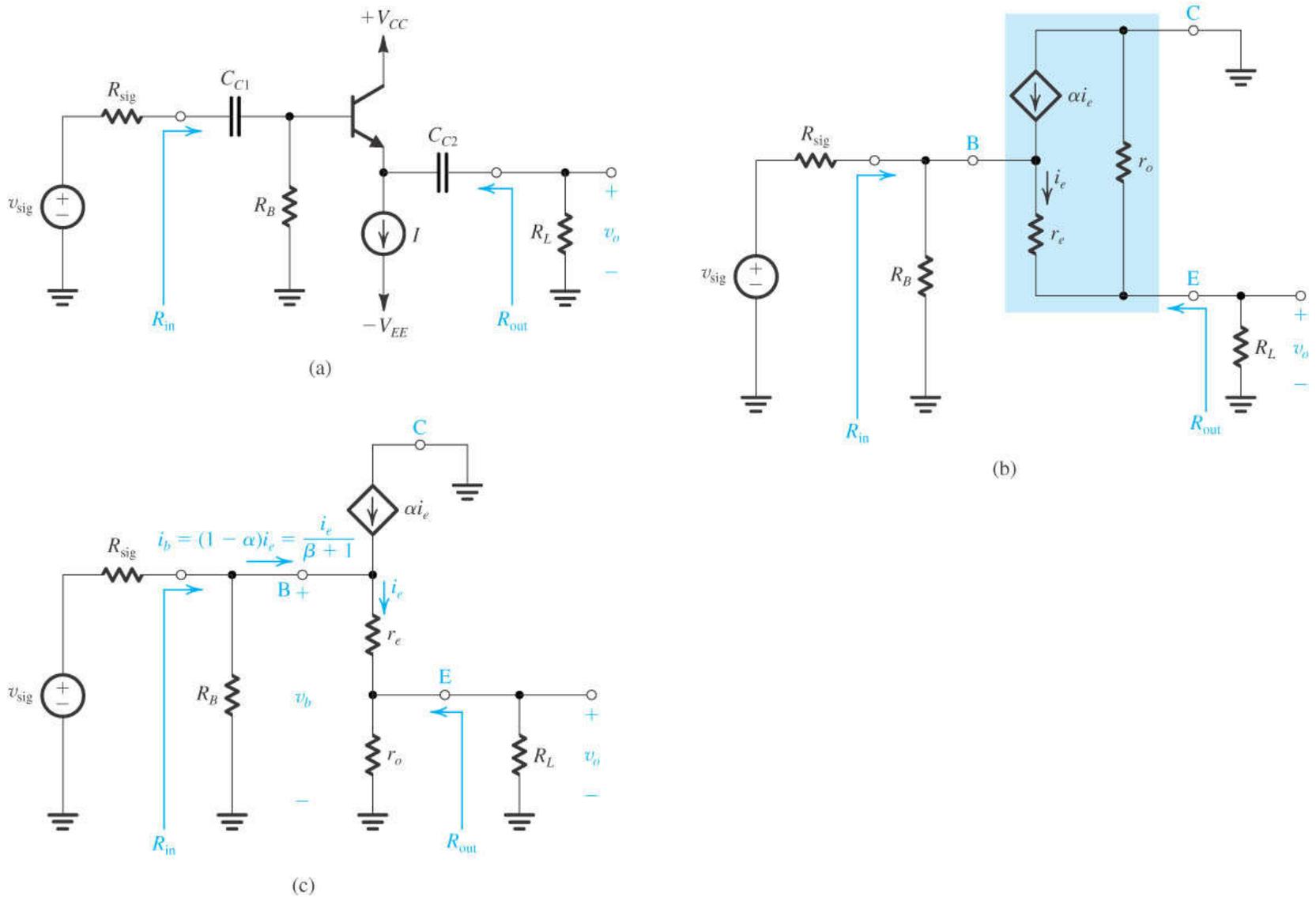
**Figure 5.60** (a) A common-emitter amplifier using the structure of Fig. 5.59. (b) Equivalent circuit obtained by replacing the transistor with its hybrid- $\pi$  model.



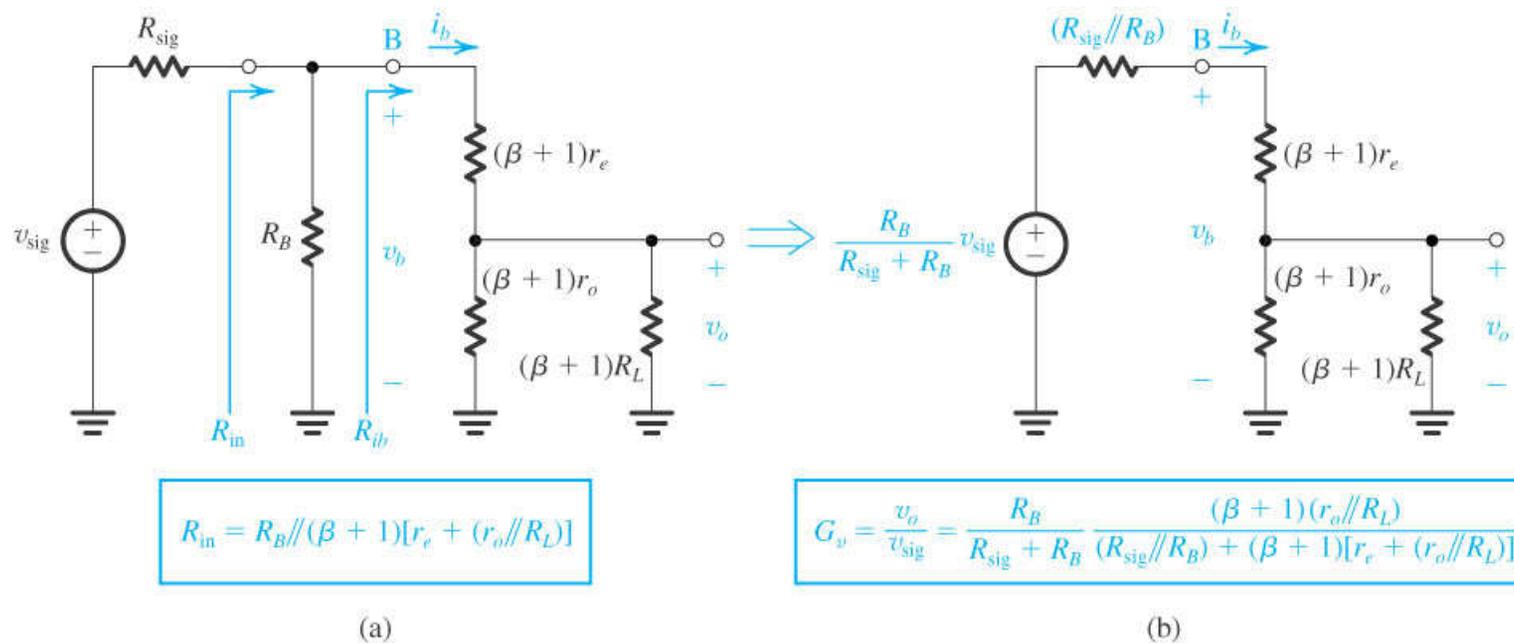
**Figure 5.61** (a) A common-emitter amplifier with an emitter resistance  $R_e$ . (b) Equivalent circuit obtained by replacing the transistor with its T model.



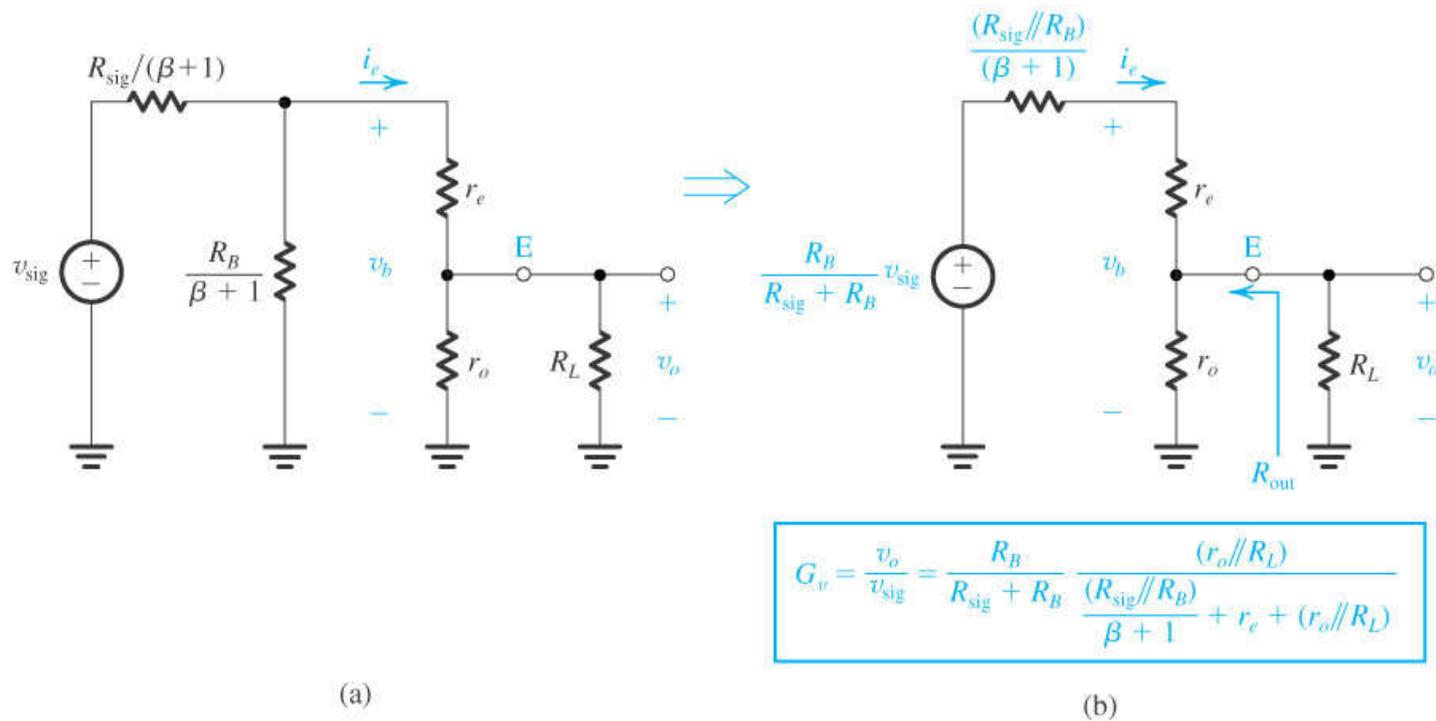
**Figure 5.62** (a) A common-base amplifier using the structure of Fig. 5.59. (b) Equivalent circuit obtained by replacing the transistor with its T model.



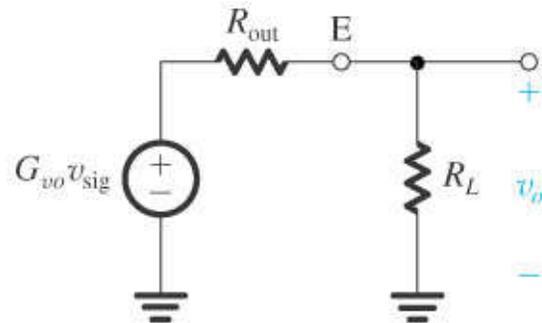
**Figure 5.63** (a) An emitter-follower circuit based on the structure of Fig. 5.59. (b) Small-signal equivalent circuit of the emitter follower with the transistor replaced by its T model augmented with  $r_o$ . (c) The circuit in (b) redrawn to emphasize that  $r_o$  is in parallel with  $R_L$ . This simplifies the analysis considerably.



**Figure 5.64** (a) An equivalent circuit of the emitter follower obtained from the circuit in Fig. 5.63(c) by reflecting all resistances in the emitter to the base side. (b) The circuit in (a) after application of Thévenin theorem to the input circuit composed of  $v_{sig}$ ,  $R_{sig}$ , and  $R_B$ .



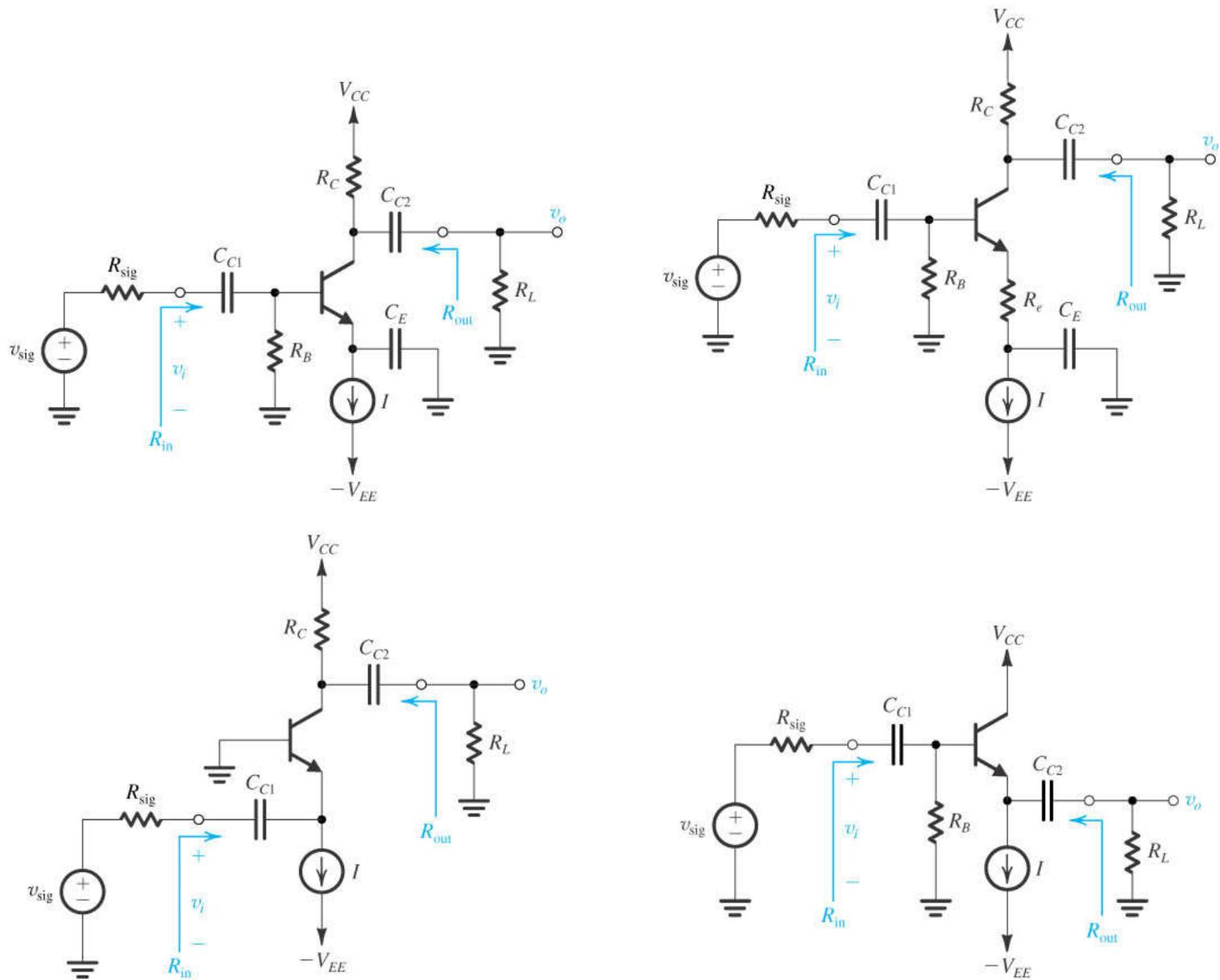
**Figure 5.65** (a) An alternate equivalent circuit of the emitter follower obtained by reflecting all base-circuit resistances to the emitter side. (b) The circuit in (a) after application of Thévenin theorem to the input circuit composed of  $v_{sig}$ ,  $R_{sig}/(\beta + 1)$ , and  $R_B/(\beta + 1)$ .



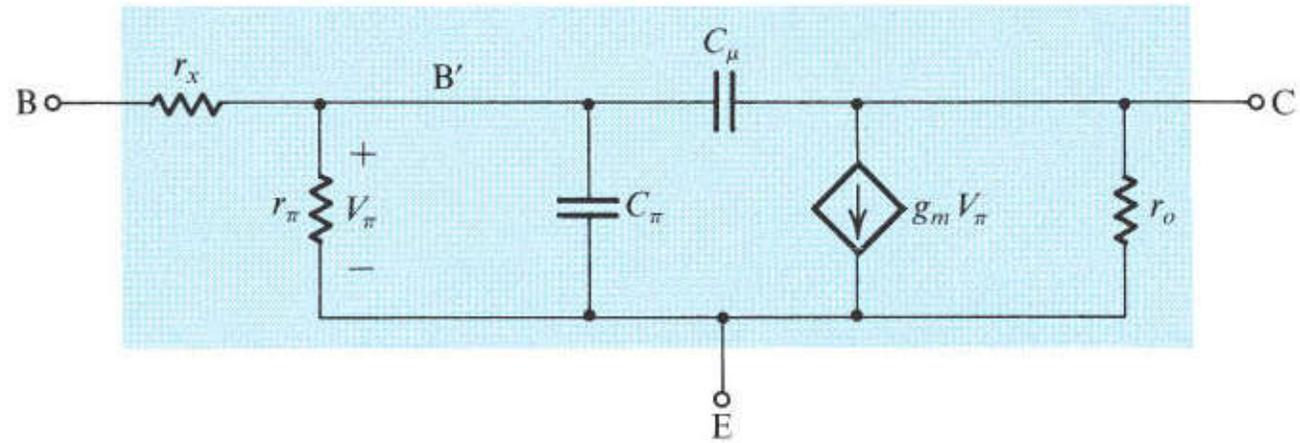
$$G_{vo} = \frac{R_B}{R_{sig} + R_B} \frac{r_o}{\frac{R_{sig} // R_B}{\beta + 1} + r_e + r_o}$$

$$R_{out} = r_o // \left( r_e + \frac{R_{sig} // R_B}{\beta + 1} \right)$$

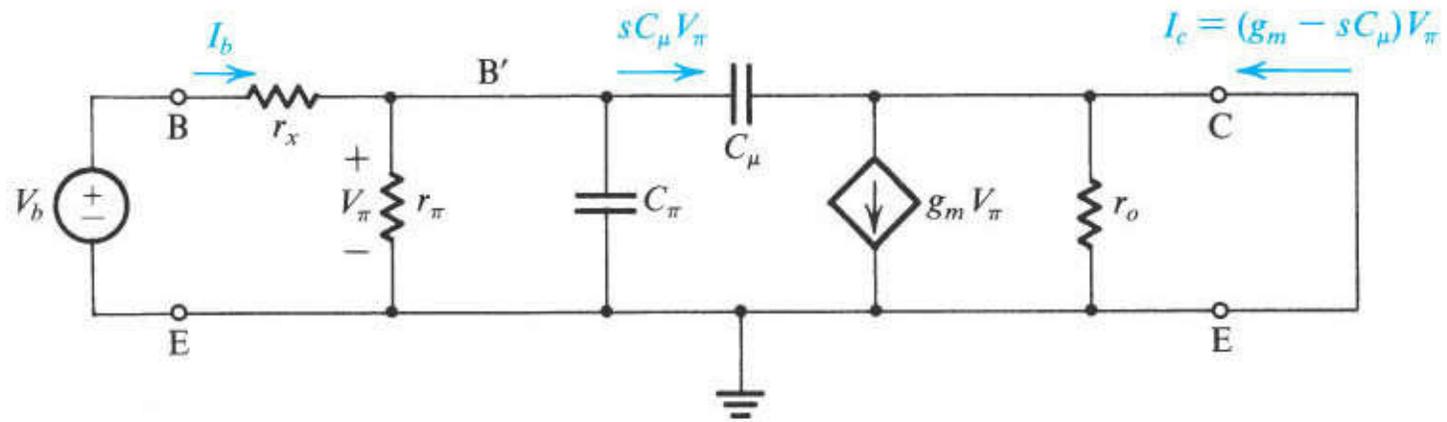
**Figure 5.66** Thévenin equivalent circuit of the output of the emitter follower of Fig. 5.63(a). This circuit can be used to find  $v_o$  and hence the overall voltage gain  $v_o/v_{sig}$  for any desired  $R_L$ .



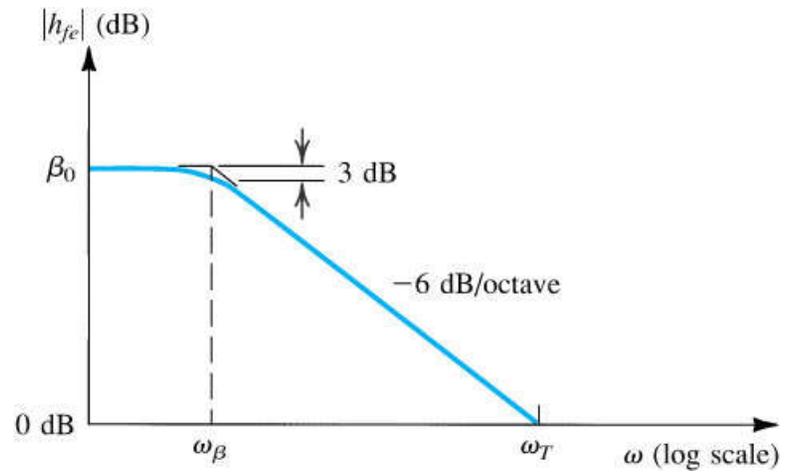
**Table 5.6**



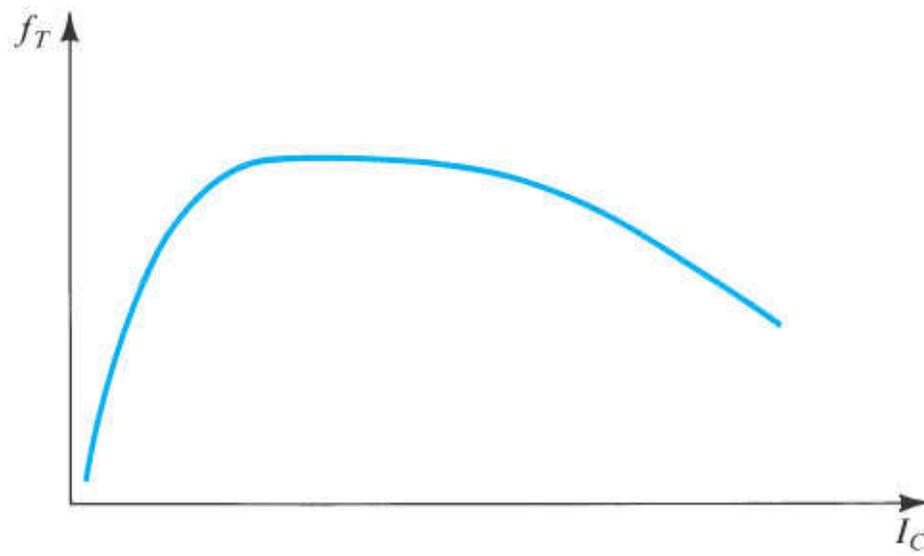
**Figure 5.67** The high-frequency hybrid- $\pi$  model.



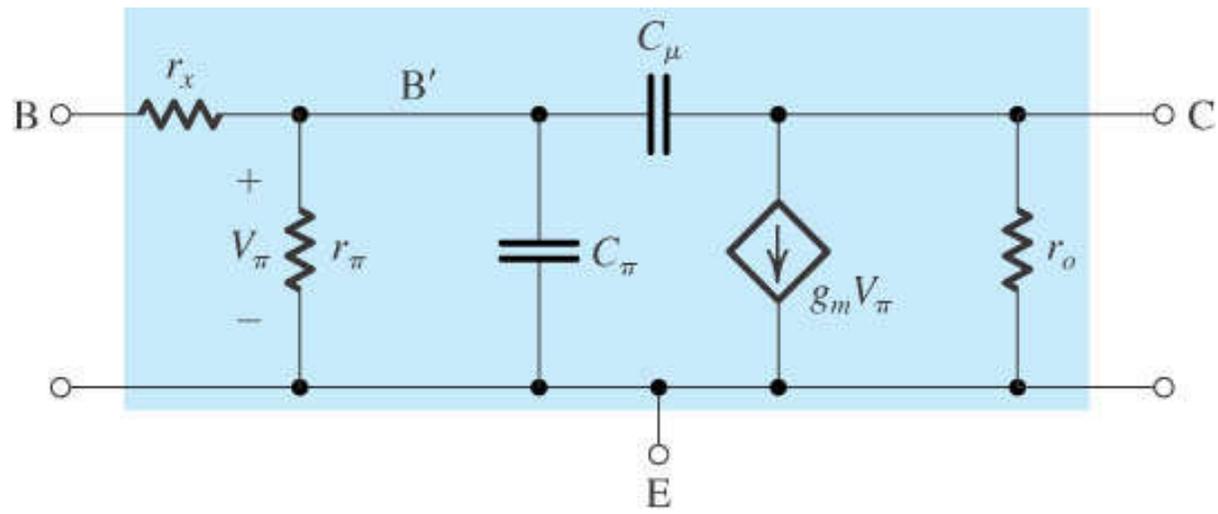
**Figure 5.68** Circuit for deriving an expression for  $h_{fe}(s) ; I_c/I_b$ .



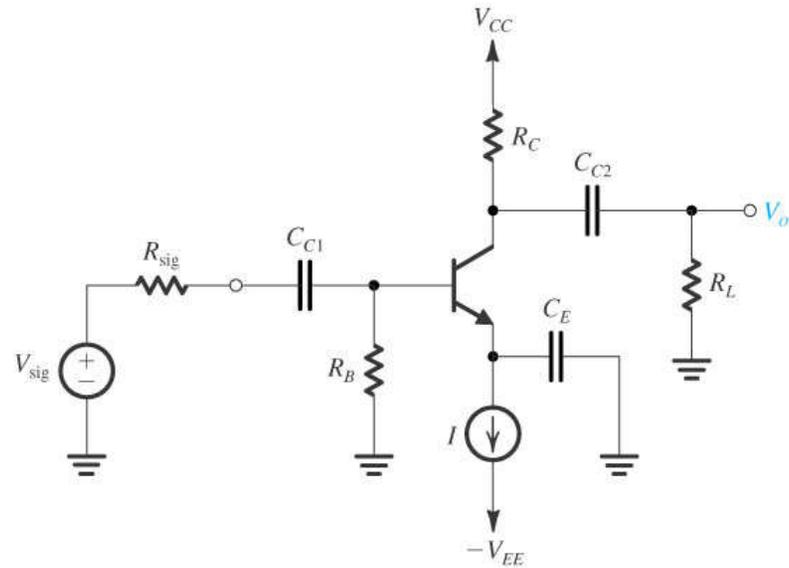
**Figure 5.69** Bode plot for  $|h_{fe}|$ .



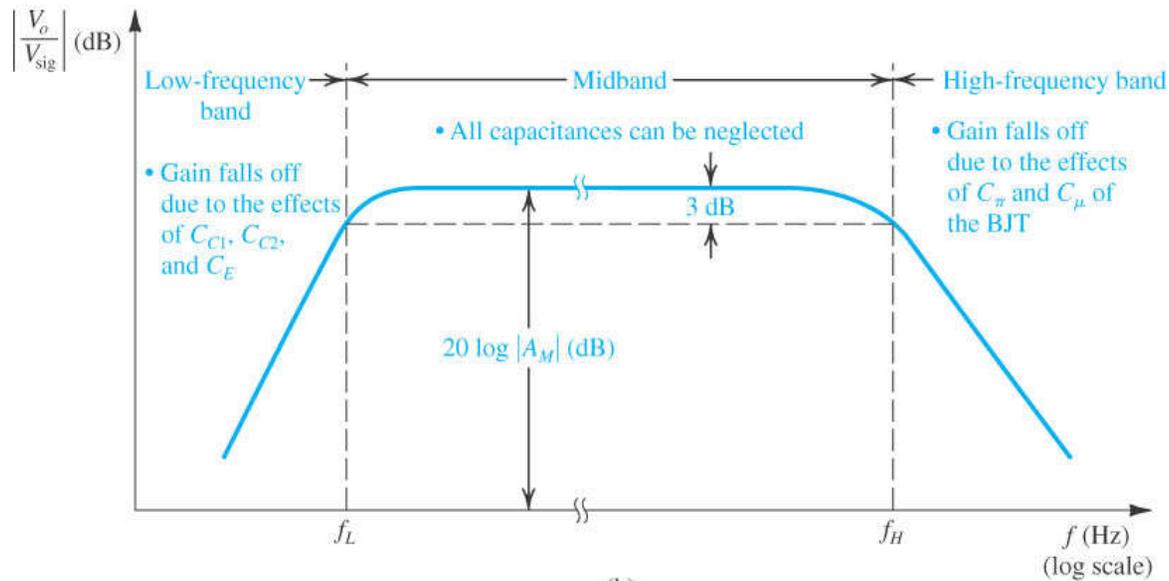
**Figure 5.70** Variation of  $f_T$  with  $I_C$ .



**Table 5.7**

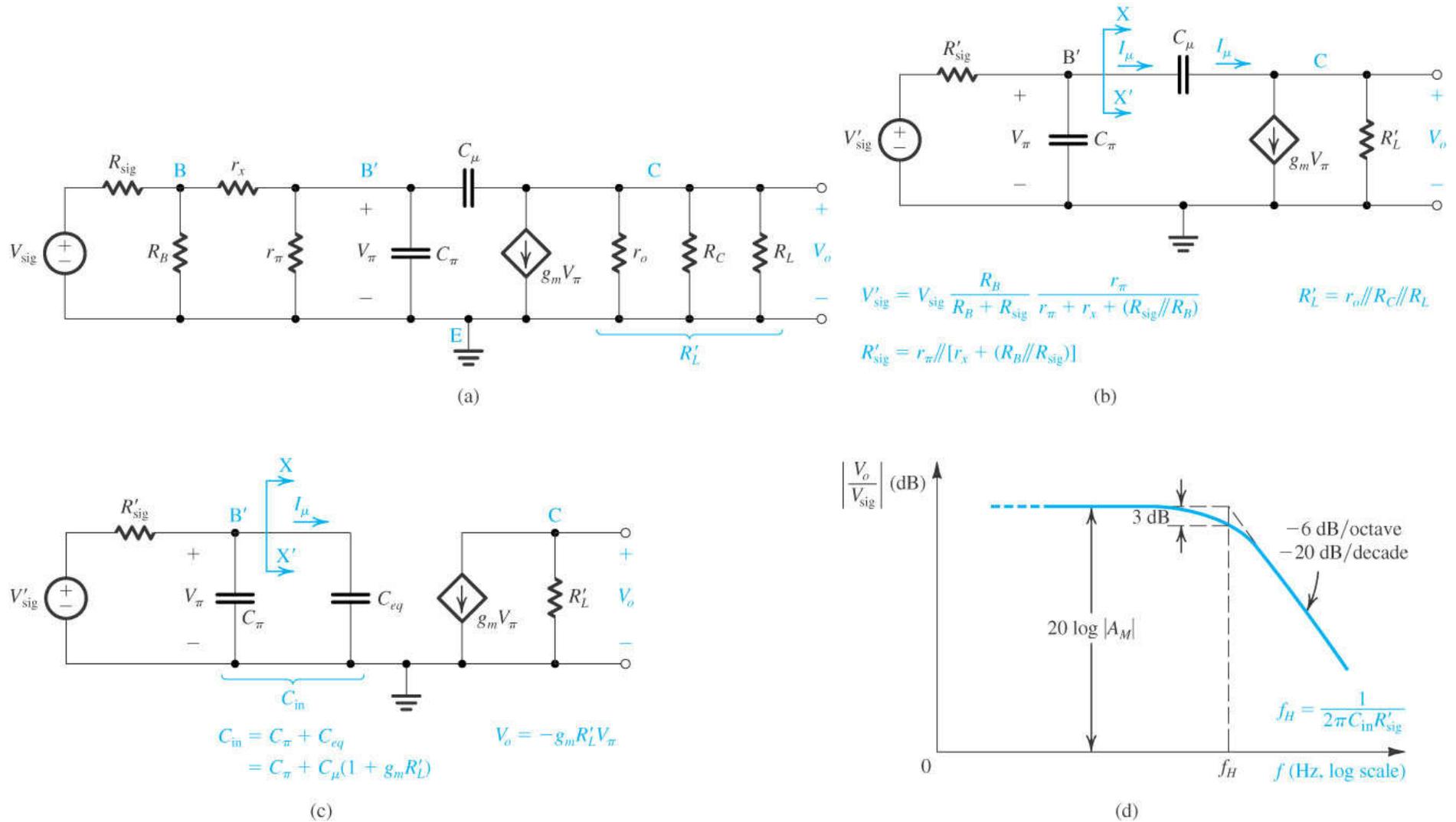


(a)

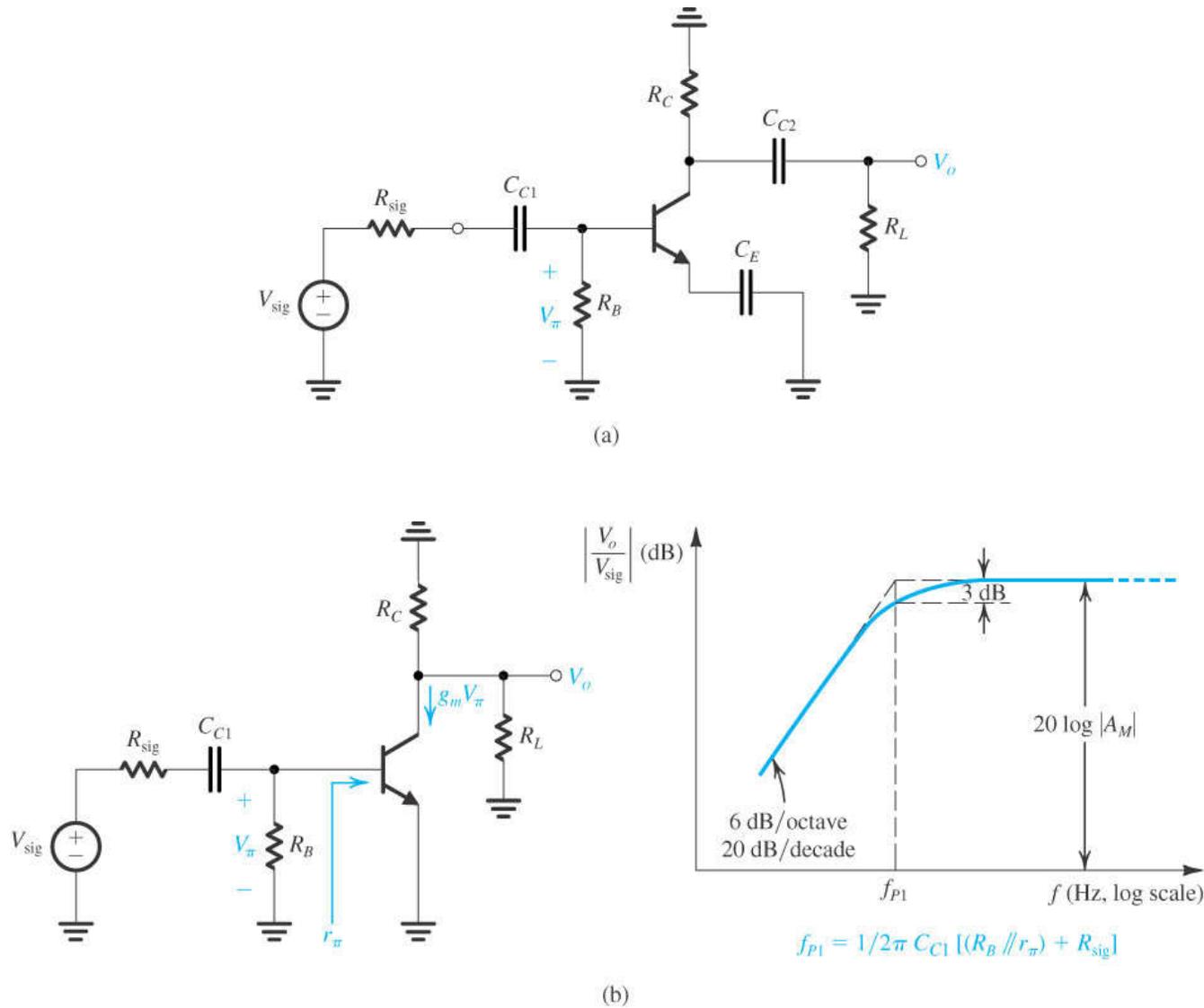


(b)

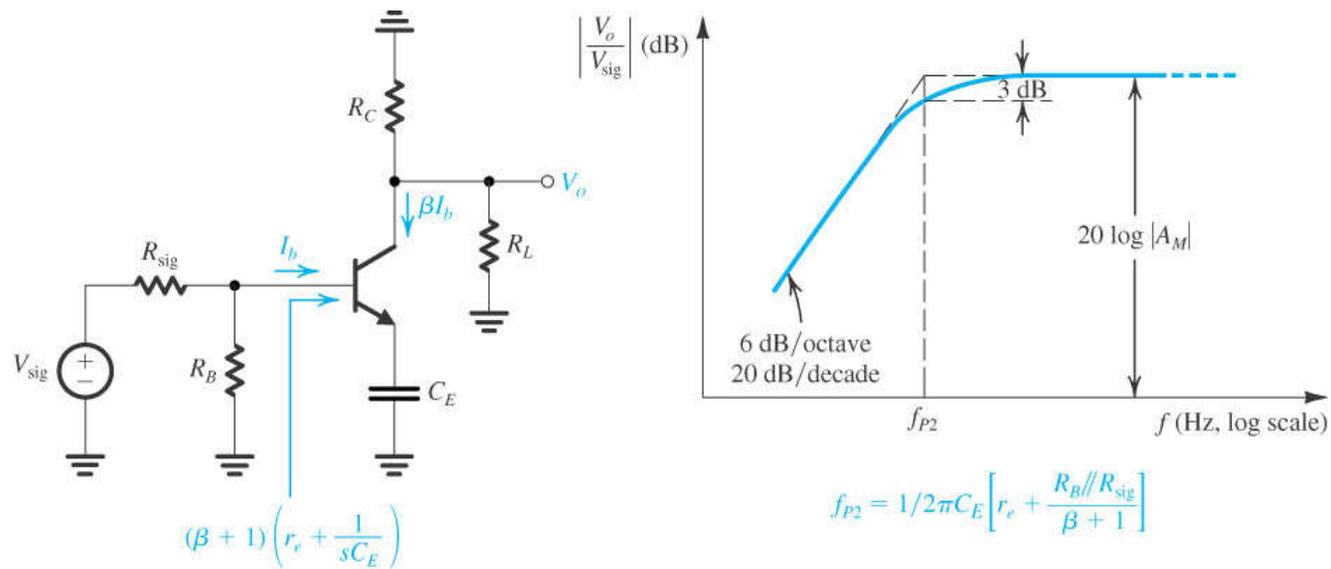
**Figure 5.71** (a) Capacitively coupled common-emitter amplifier. (b) Sketch of the magnitude of the gain of the CE amplifier versus frequency. The graph delineates the three frequency bands relevant to frequency-response determination.



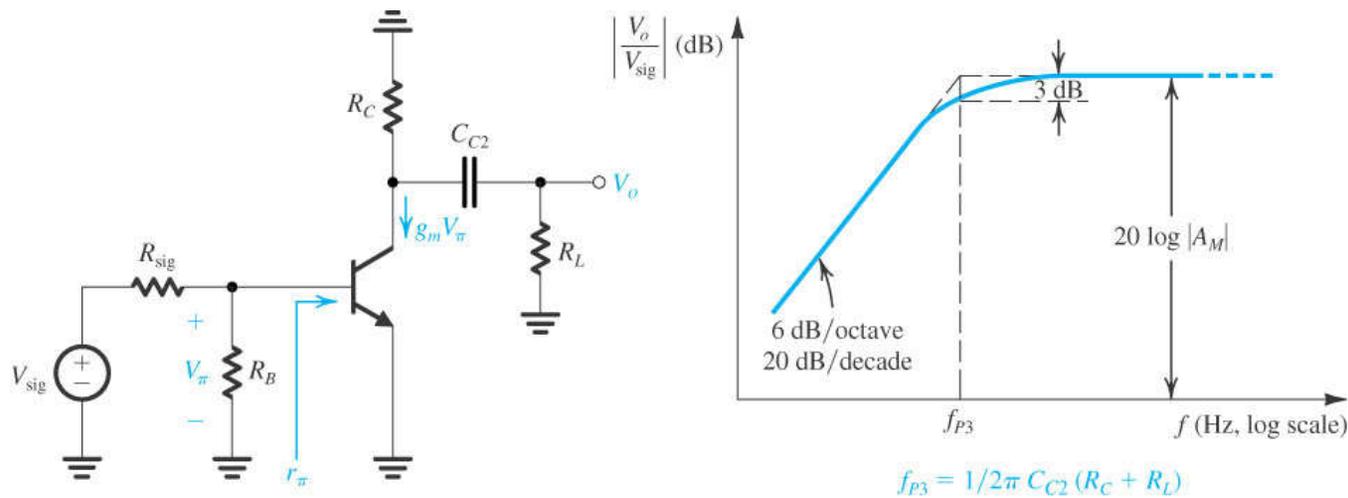
**Figure 5.72** Determining the high-frequency response of the CE amplifier: **(a)** equivalent circuit; **(b)** the circuit of (a) simplified at both the input side and the output side; **(c)** equivalent circuit with  $C_\mu$  replaced at the input side with the equivalent capacitance  $C_{eq}$ ; **(d)** sketch of the frequency-response plot, which is that of a low-pass STC circuit.



**Figure 5.73** Analysis of the low-frequency response of the CE amplifier: **(a)** amplifier circuit with dc sources removed; **(b)** the effect of  $C_{C1}$  is determined with  $C_E$  and  $C_{C2}$  assumed to be acting as perfect short circuits;

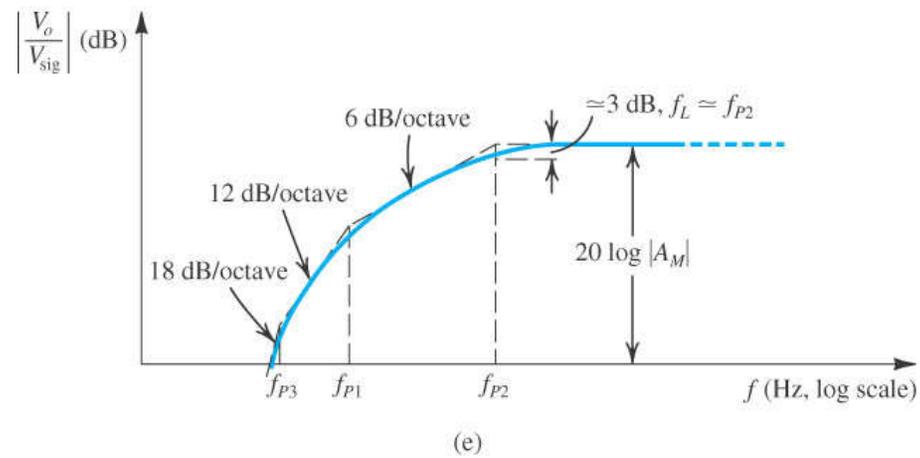


(c)

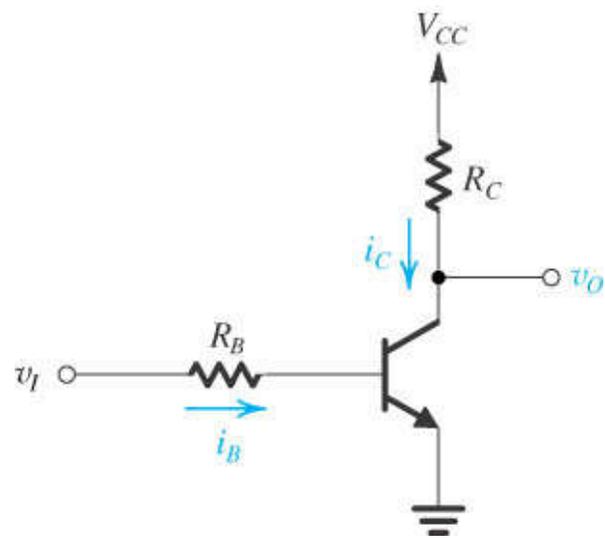


(d)

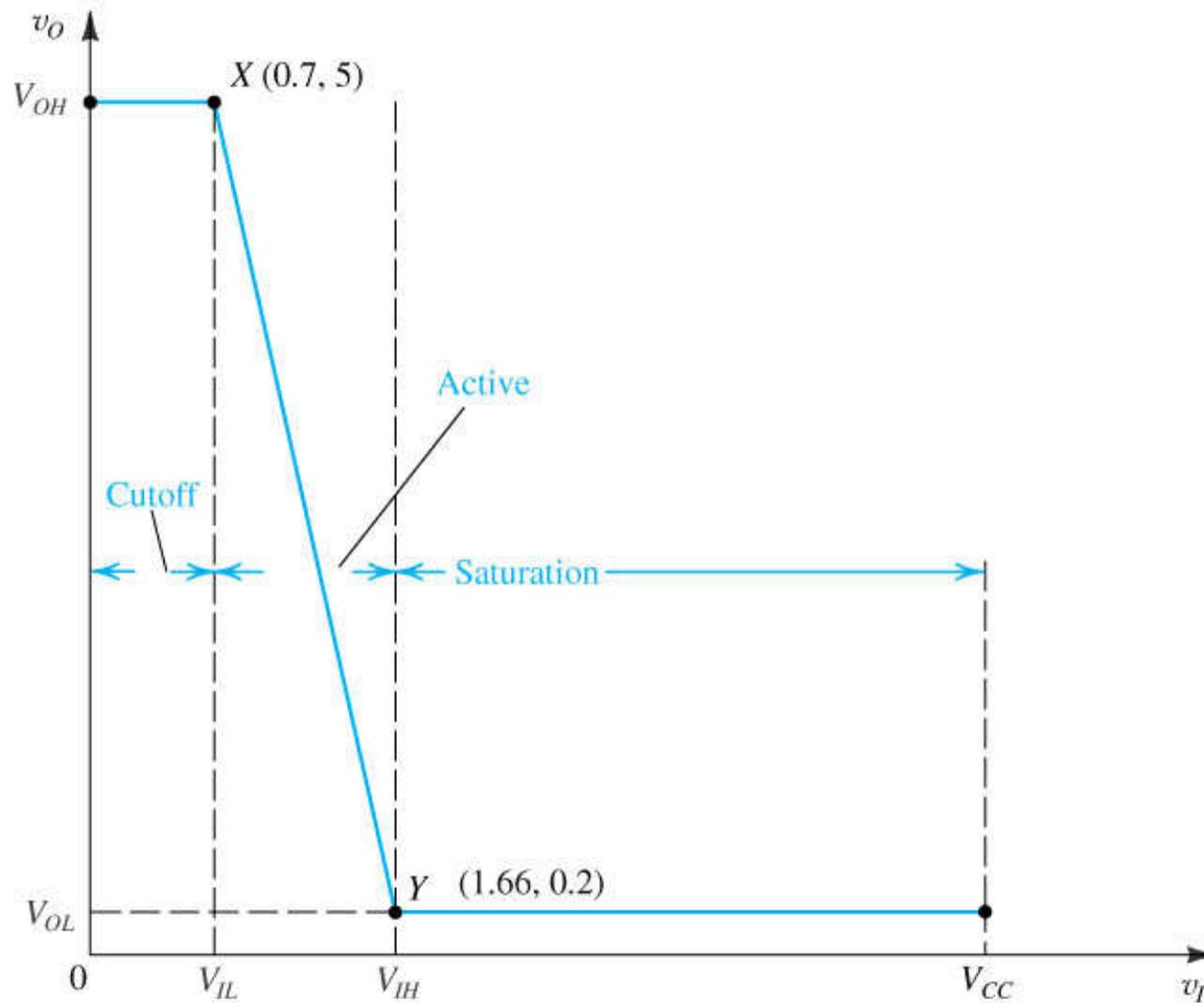
**Figure 5.73** (Continued) **(c)** the effect of  $C_E$  is determined with  $C_{C1}$  and  $C_{C2}$  assumed to be acting as perfect short circuits; **(d)** the effect of  $C_{C2}$  is determined with  $C_{C1}$  and  $C_E$  assumed to be acting as perfect short circuits;



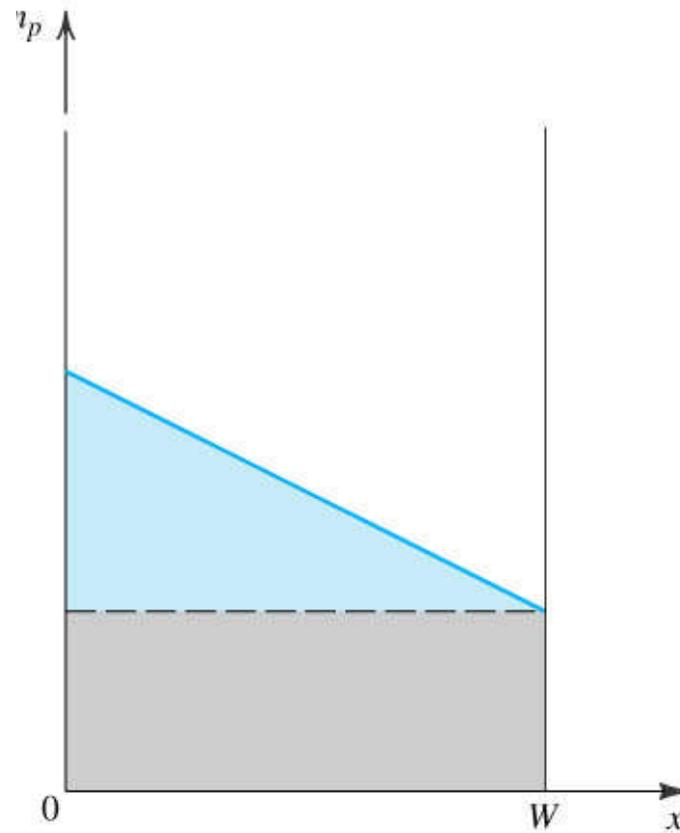
**Figure 5.73** (Continued) (e) sketch of the low-frequency gain under the assumptions that  $C_{C1}$ ,  $C_E$ , and  $C_{C2}$  do not interact and that their break (or pole) frequencies are widely separated.



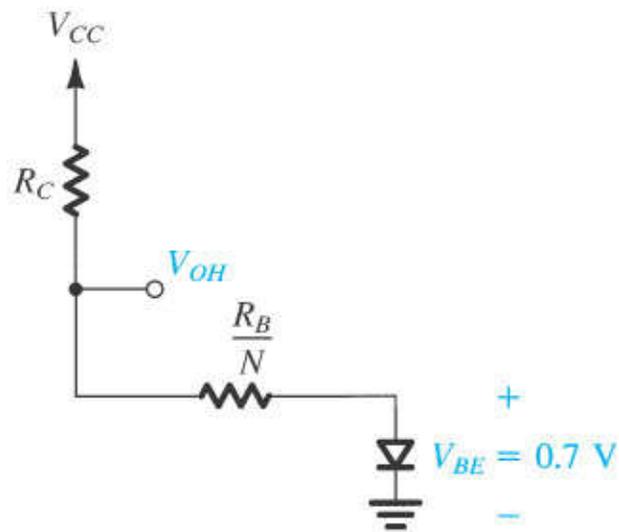
**Figure 5.74** Basic BJT digital logic inverter.



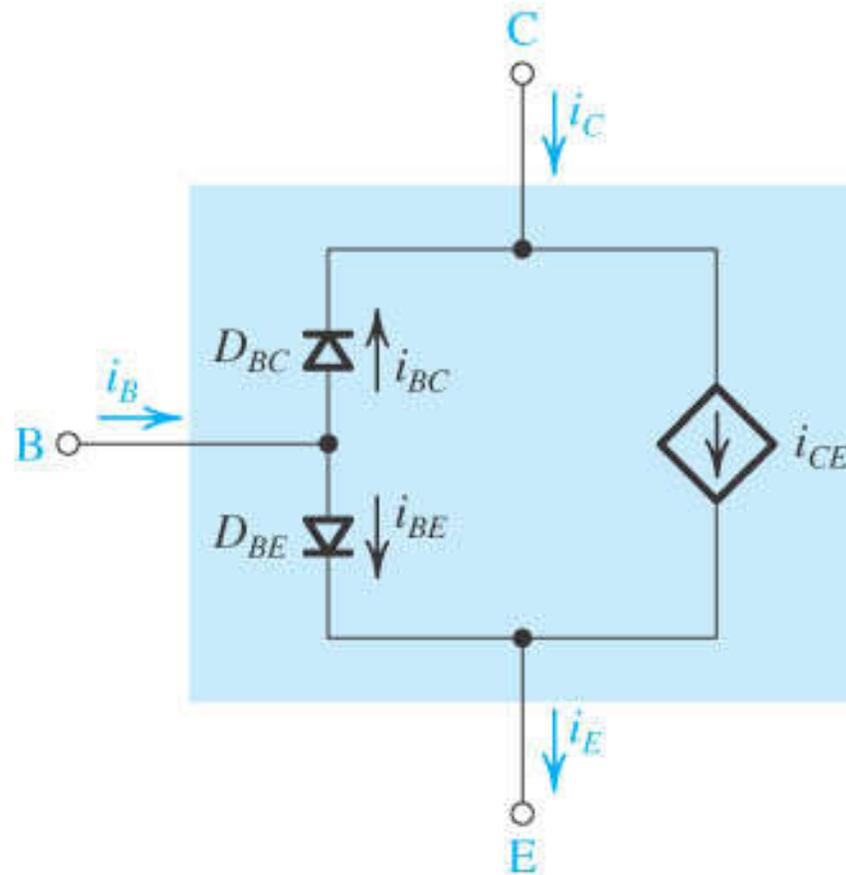
**Figure 5.75** Sketch of the voltage transfer characteristic of the inverter circuit of Fig. 5.74 for the case  $R_B = 10 \text{ k}\Omega$ ,  $R_C = 1 \text{ k}\Omega$ ,  $\beta = 50$ , and  $V_{CC} = 5 \text{ V}$ . For the calculation of the coordinates of  $X$  and  $Y$ , refer to the text.



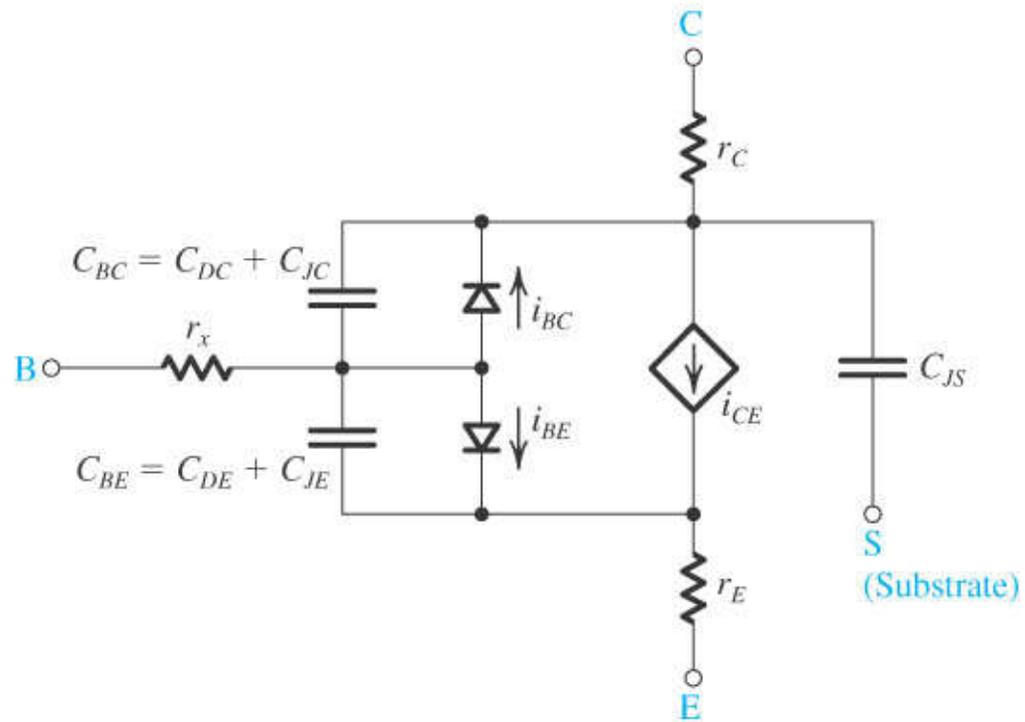
**Figure 5.76** The minority-carrier charge stored in the base of a saturated transistor can be divided into two components: That in blue produces the gradient that gives rise to the diffusion current across the base, and that in gray results from driving the transistor deeper into saturation.



**Figure E5.53**



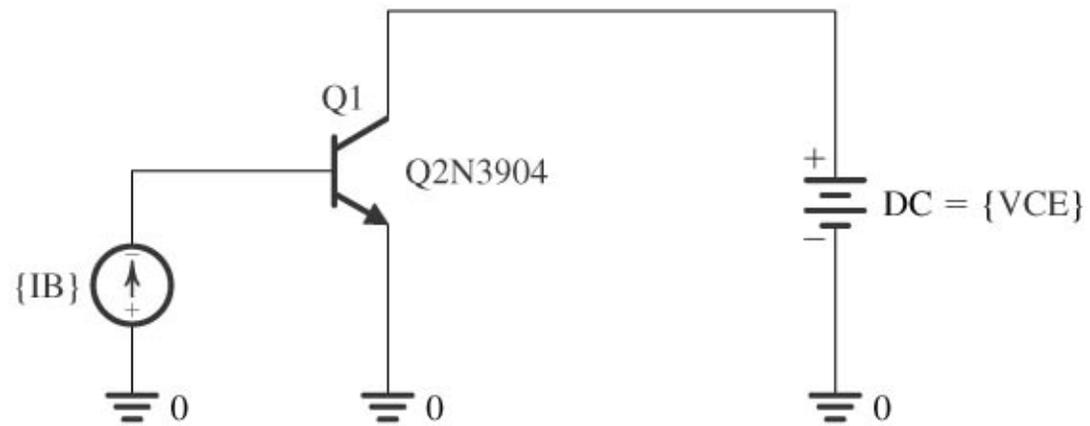
**Figure 5.77** The transport form of the Ebers-Moll model for an *npn* BJT.



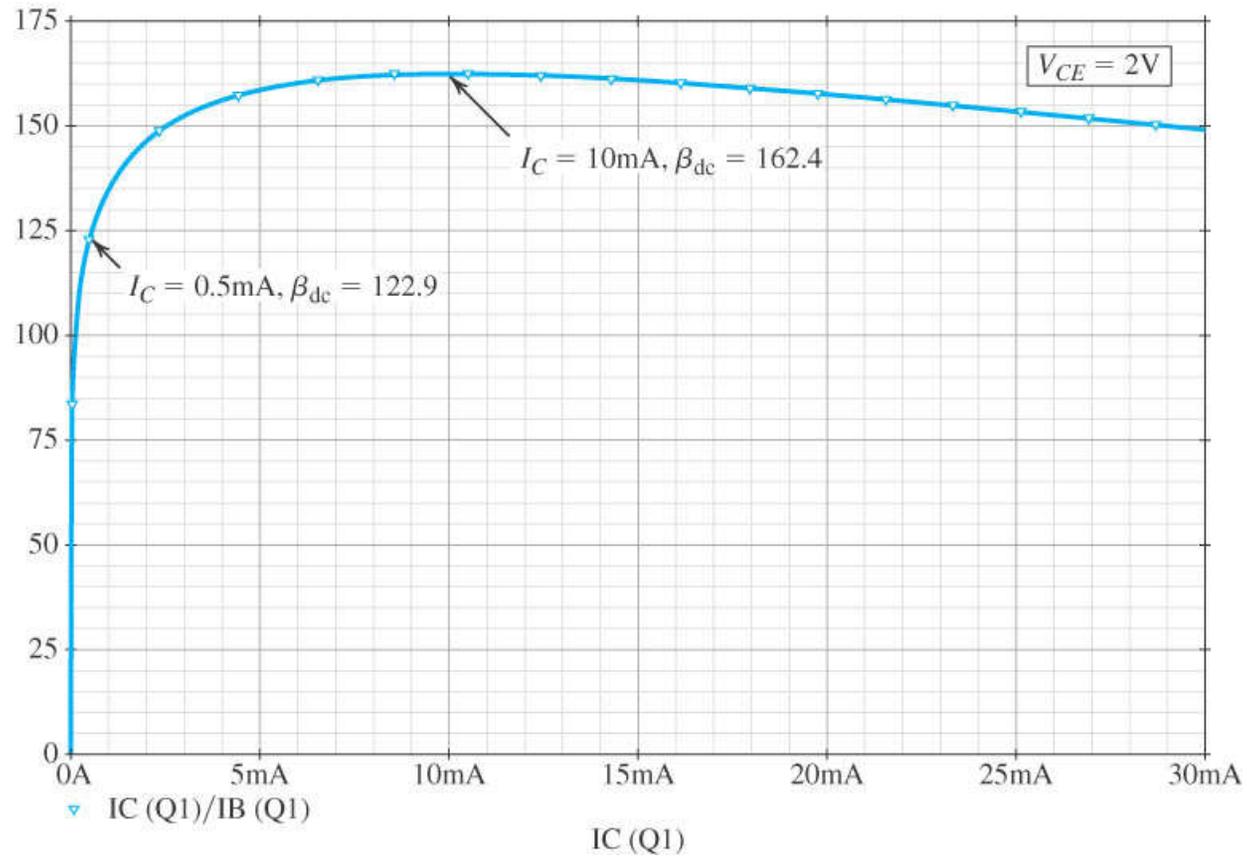
**Figure 5.78** The SPICE large-signal Ebers-Moll model for an *npn* BJT.

PARAMETERS:

$$I_B = 10\mu$$
$$V_{CE} = 2V$$



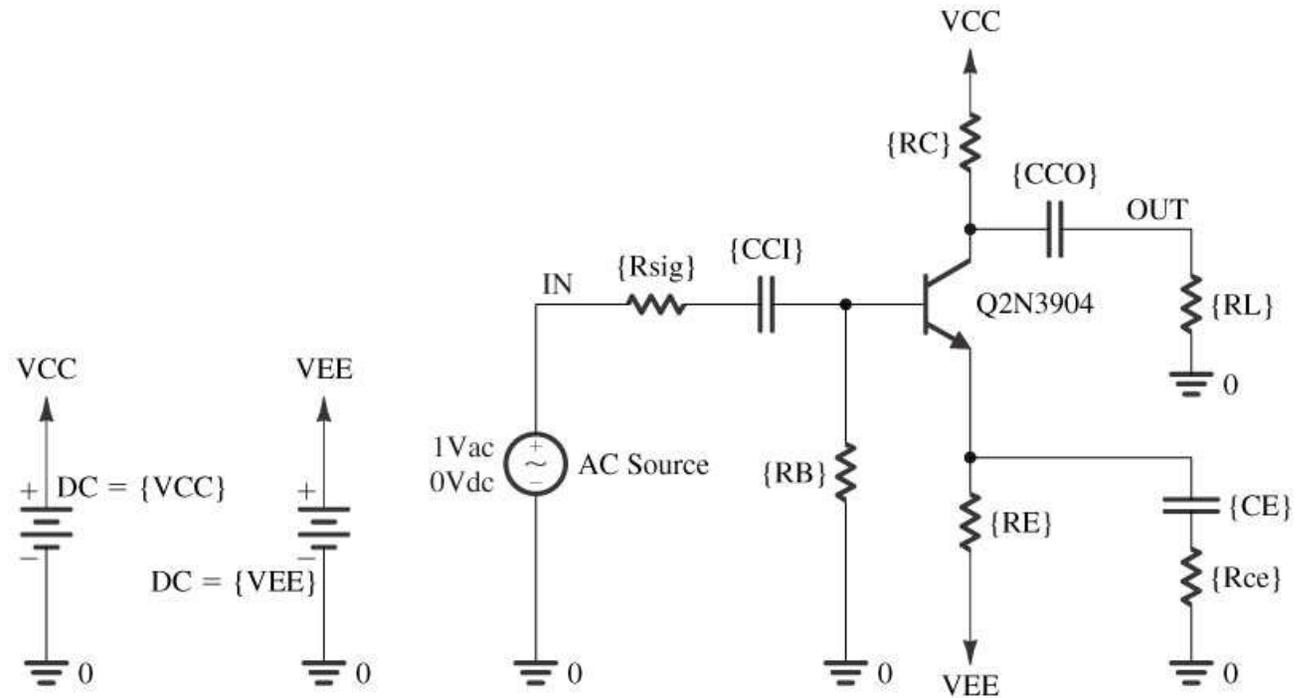
**Figure 5.79** The PSpice testbench used to demonstrate the dependence of  $\beta_{dc}$  on the collector bias current  $I_C$  for the Q2N3904 discrete BJT (Example 5.20).



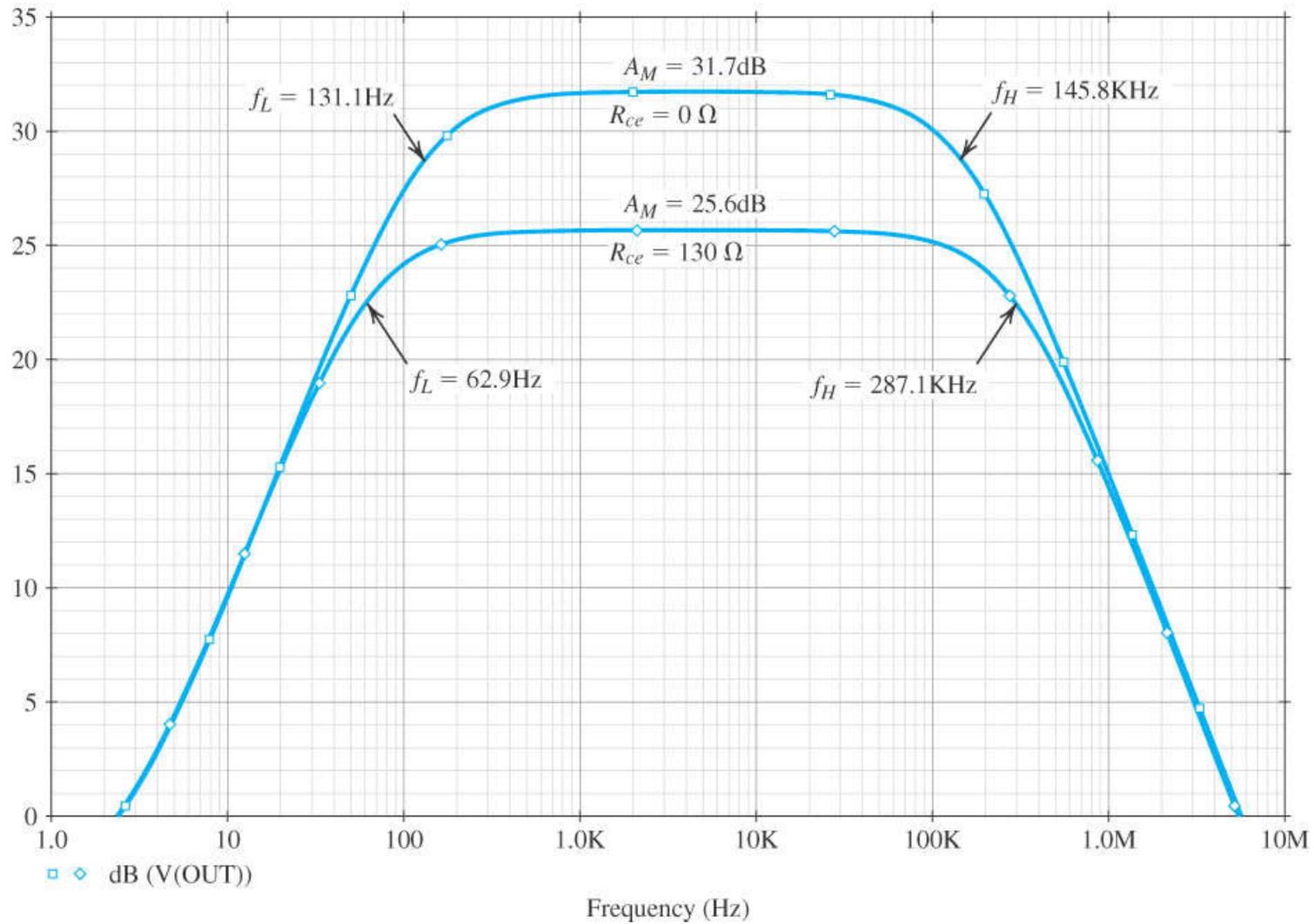
**Figure 5.80** Dependence of  $\beta_{dc}$  on  $I_C$  (at  $V_{CE} = 2V$ ) in the Q2N3904 discrete BJT (Example 5.20).

PARAMETERS:

- CE = 10u
- CCI = 10u
- CCO = 10u
- RC = 10K
- RB = 340K
- RE = 6K
- Rce = 130
- RL = 10K
- Rsig = 10K
- VCC = 5
- VEE = -5



**Figure 5.81** Capture schematic of the CE amplifier in Example 5.21.



**Figure 5.82** Frequency response of the CE amplifier in Example 5.21 with  $R_{ce} = 0$  and  $R_{ce} = 130 \Omega$ .

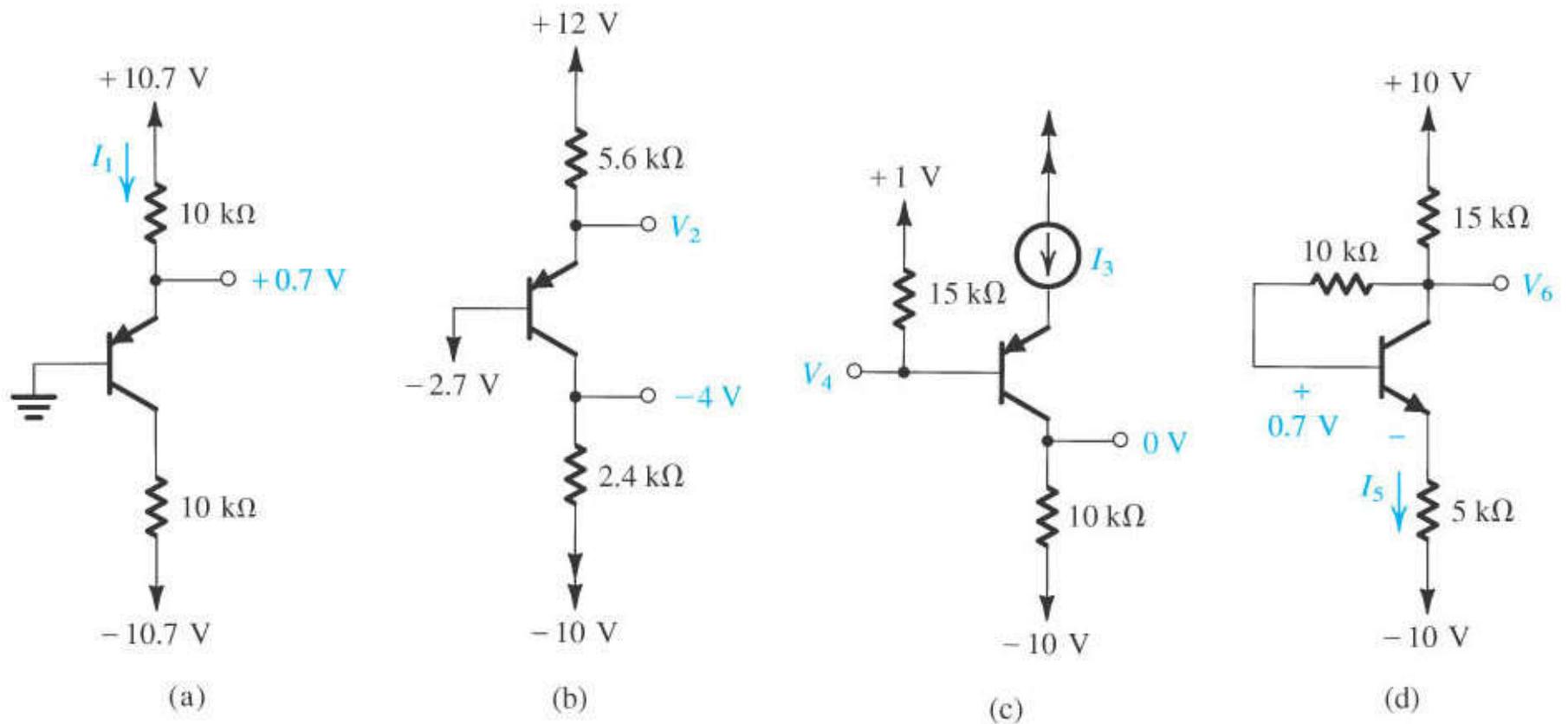
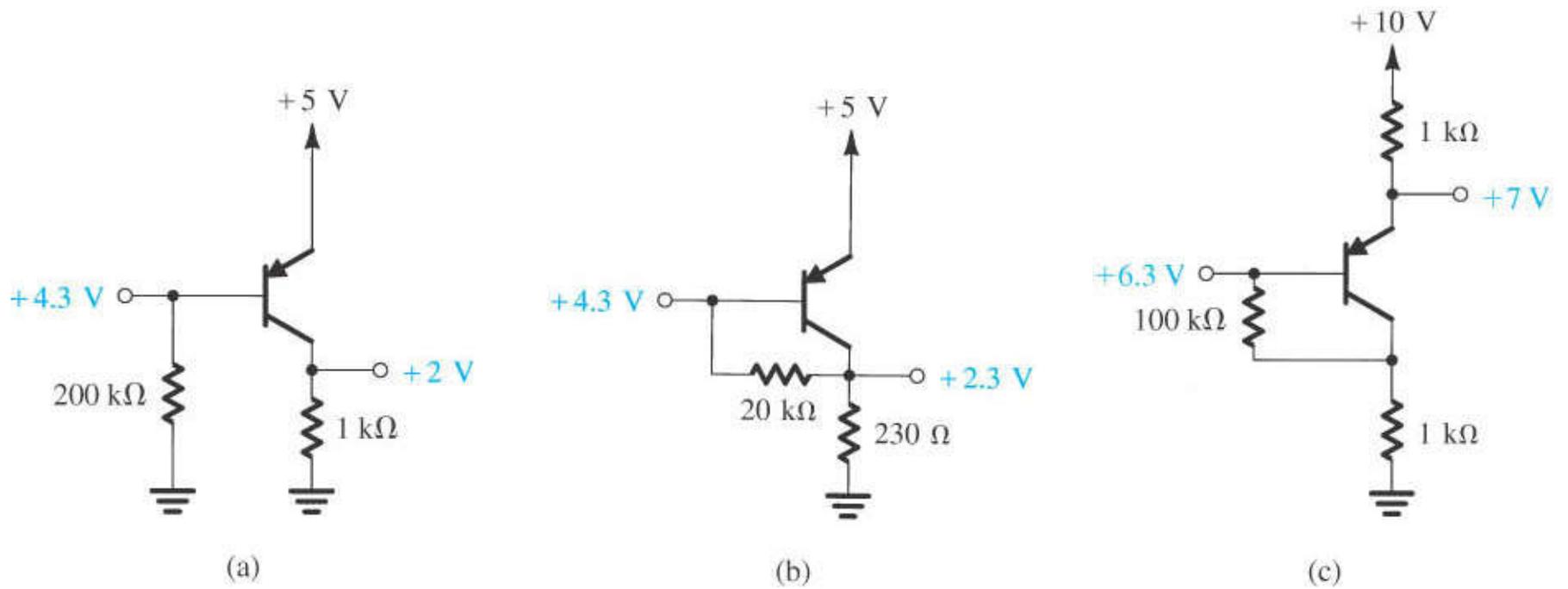
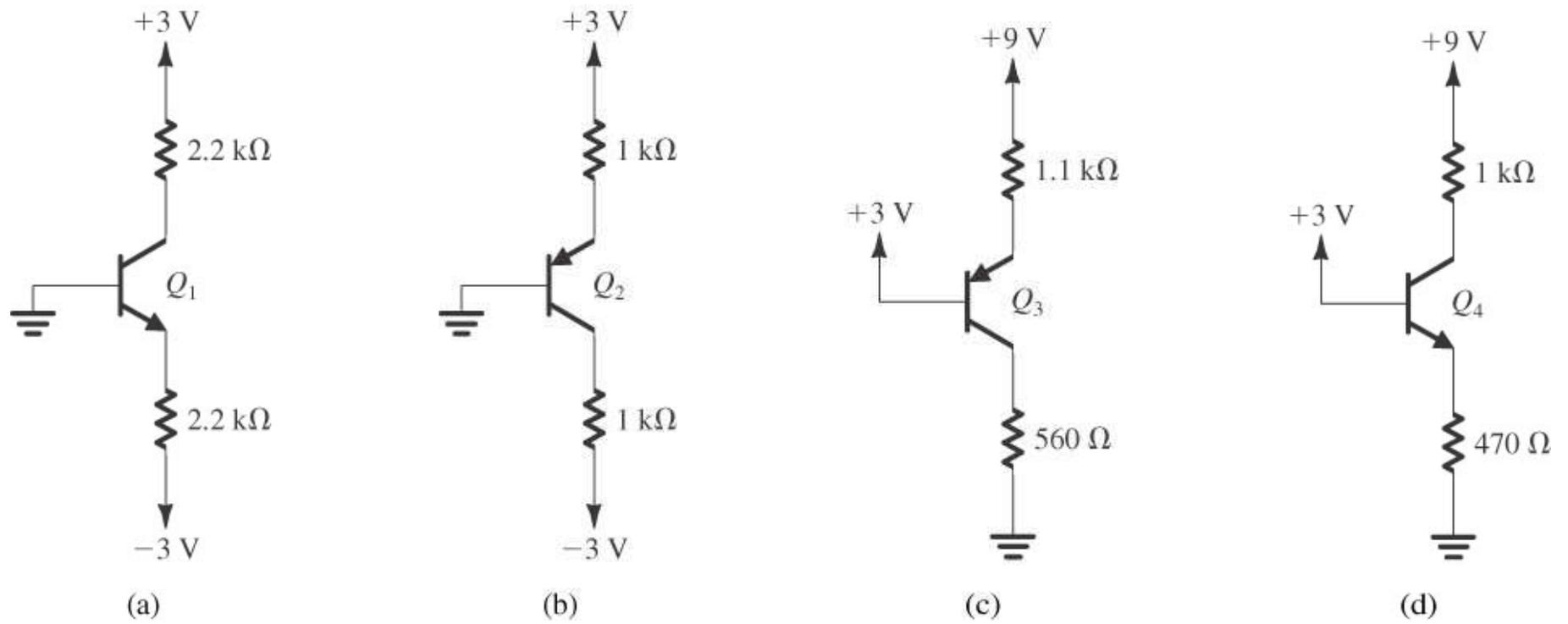


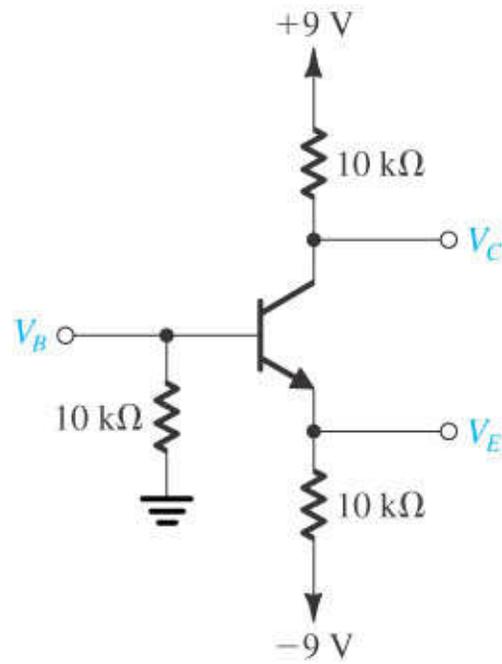
Figure P5.20



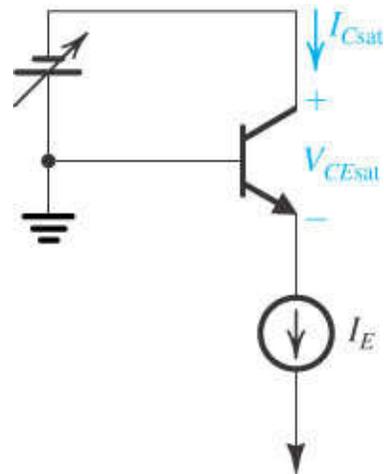
**Figure P5.21**



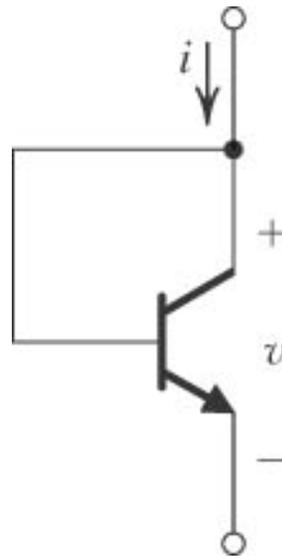
**Figure P5.24**



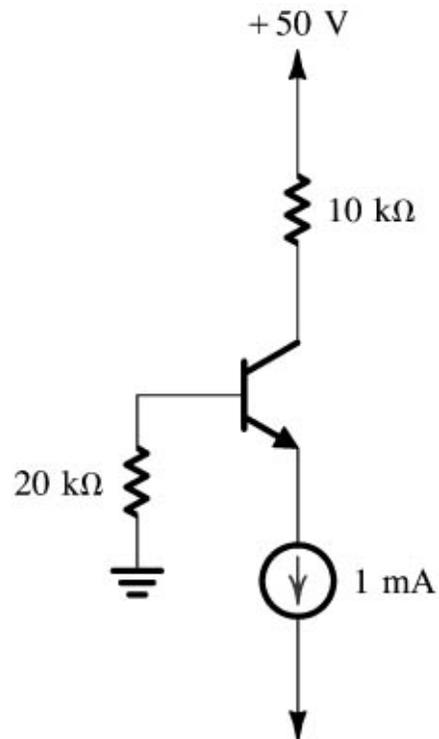
**Figure P5.26**



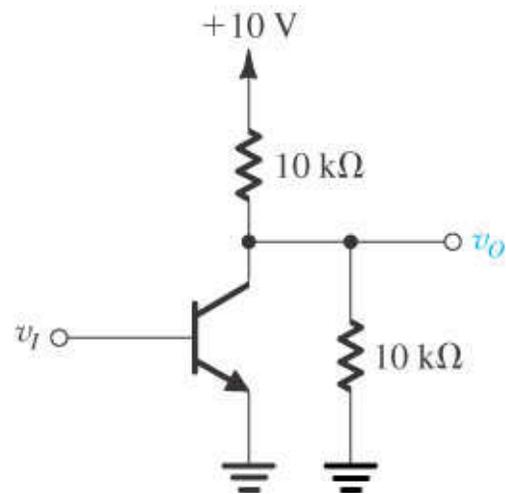
**Figure P5.36**



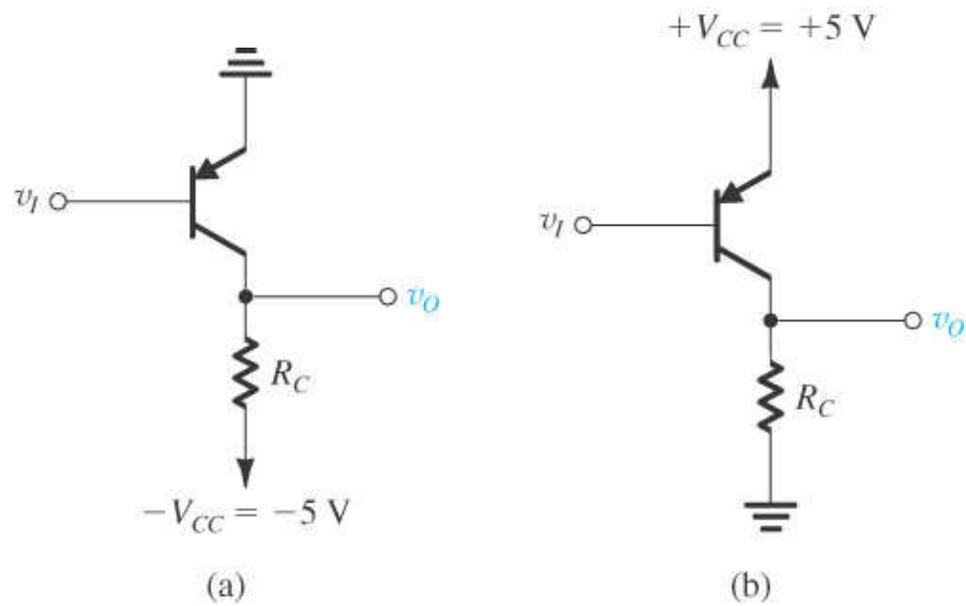
**Figure P5.44**



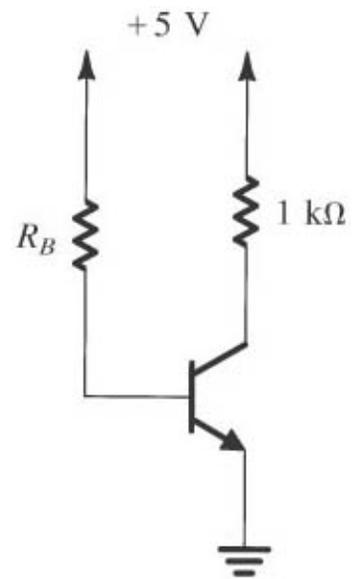
**Figure P5.53**



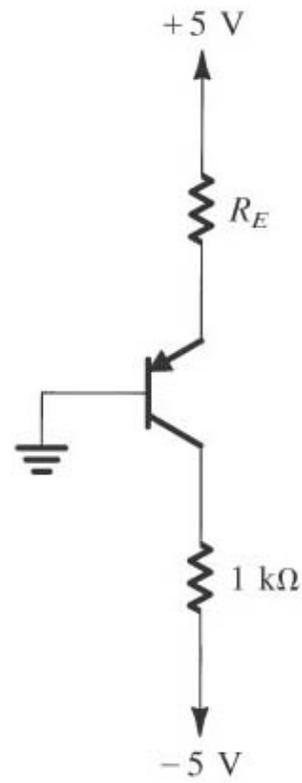
**Figure P5.57**



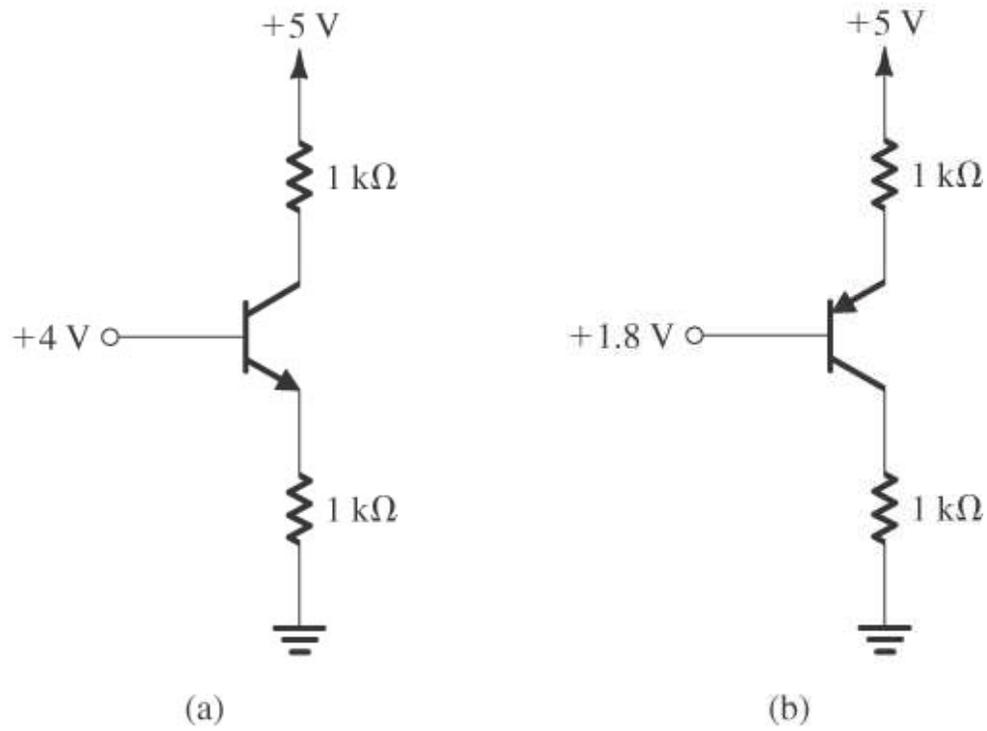
**Figure P5.58**



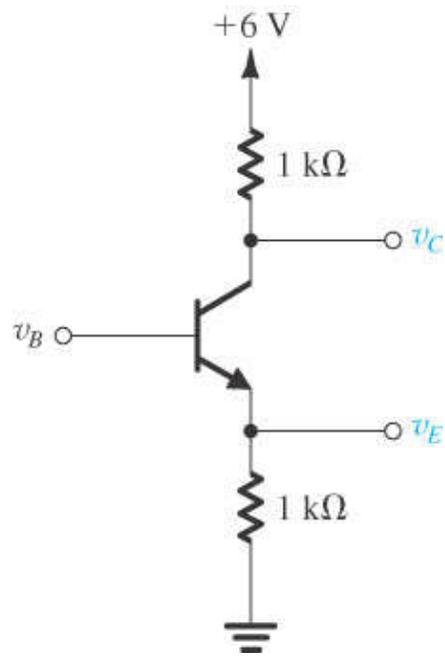
**Figure P5.65**



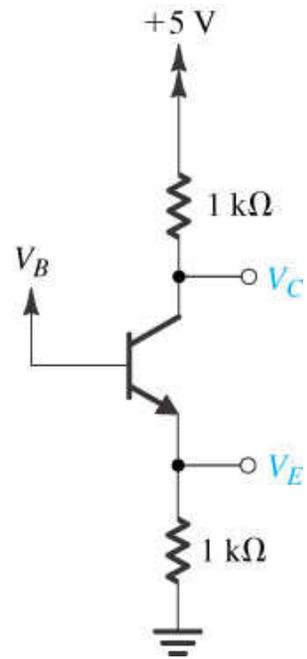
**Figure P5.66**



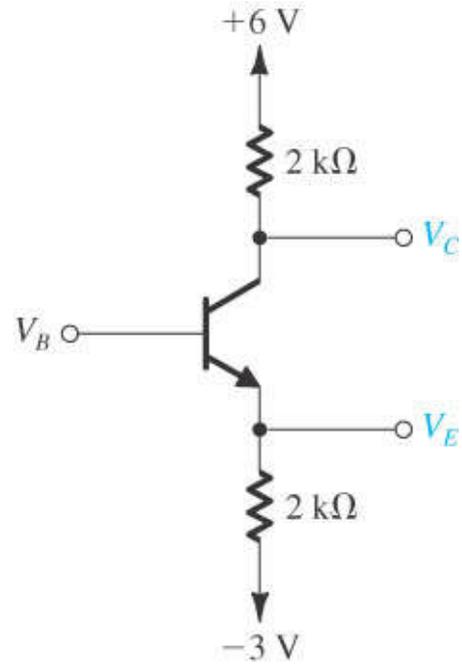
**Figure P5.67**



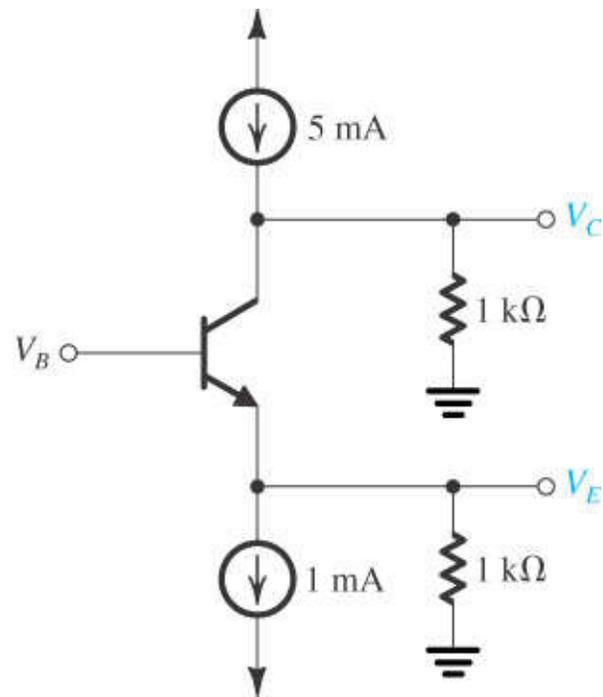
**Figure P5.68**



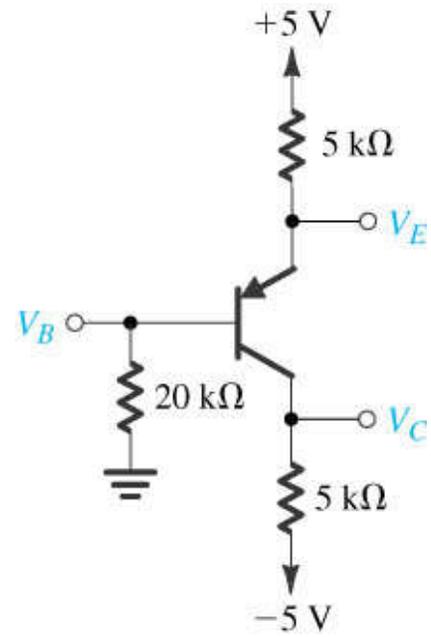
**Figure P5.69**



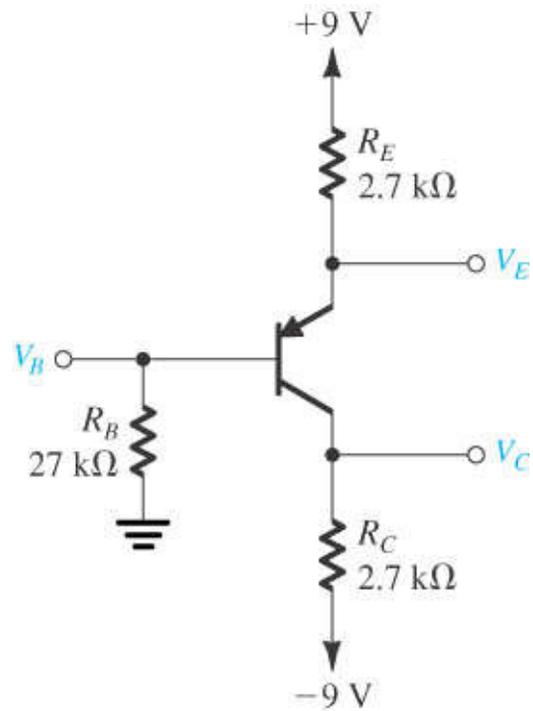
**Figure P5.71**



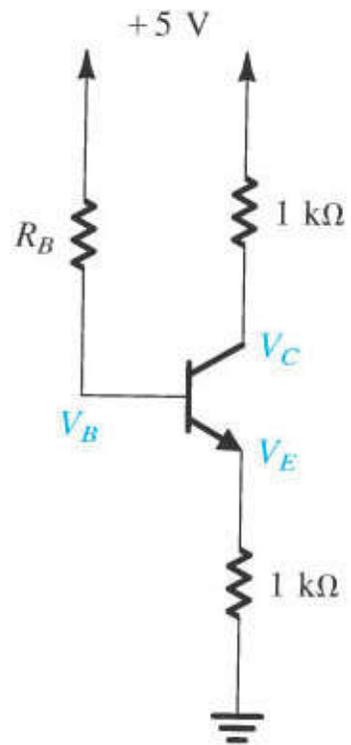
**Figure P5.72**



**Figure P5.74**



**Figure P5.76**



**Figure P5.78**

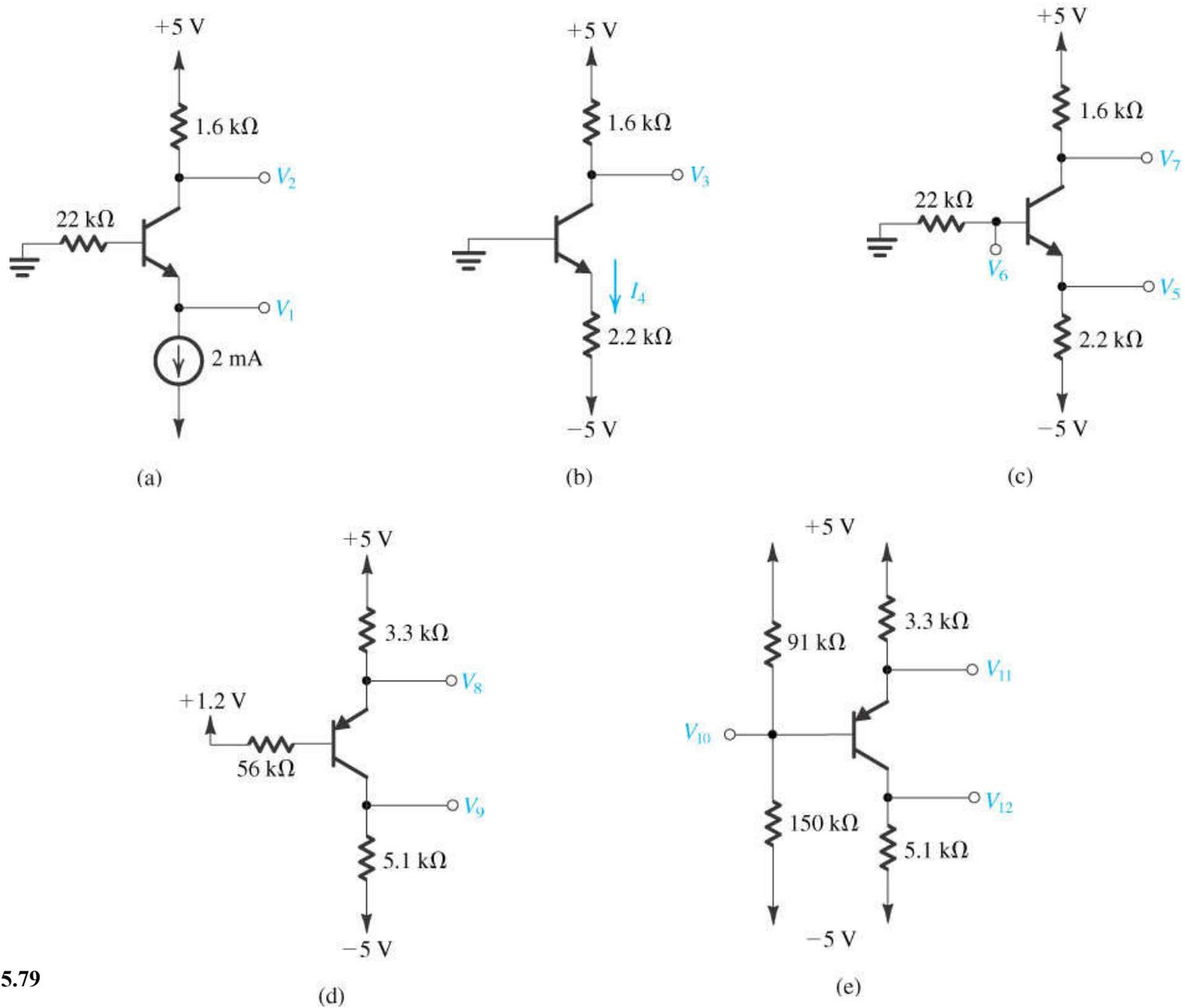
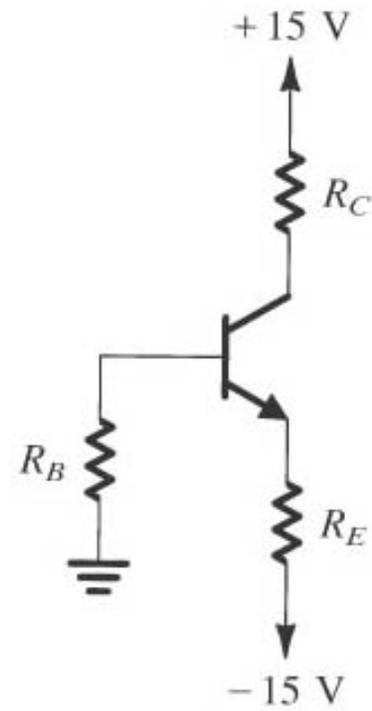
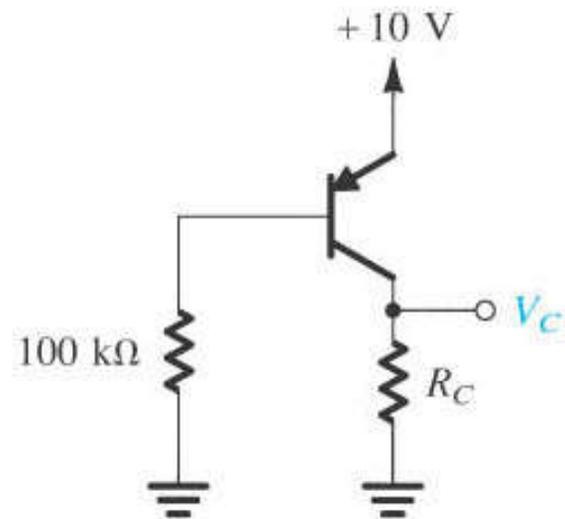


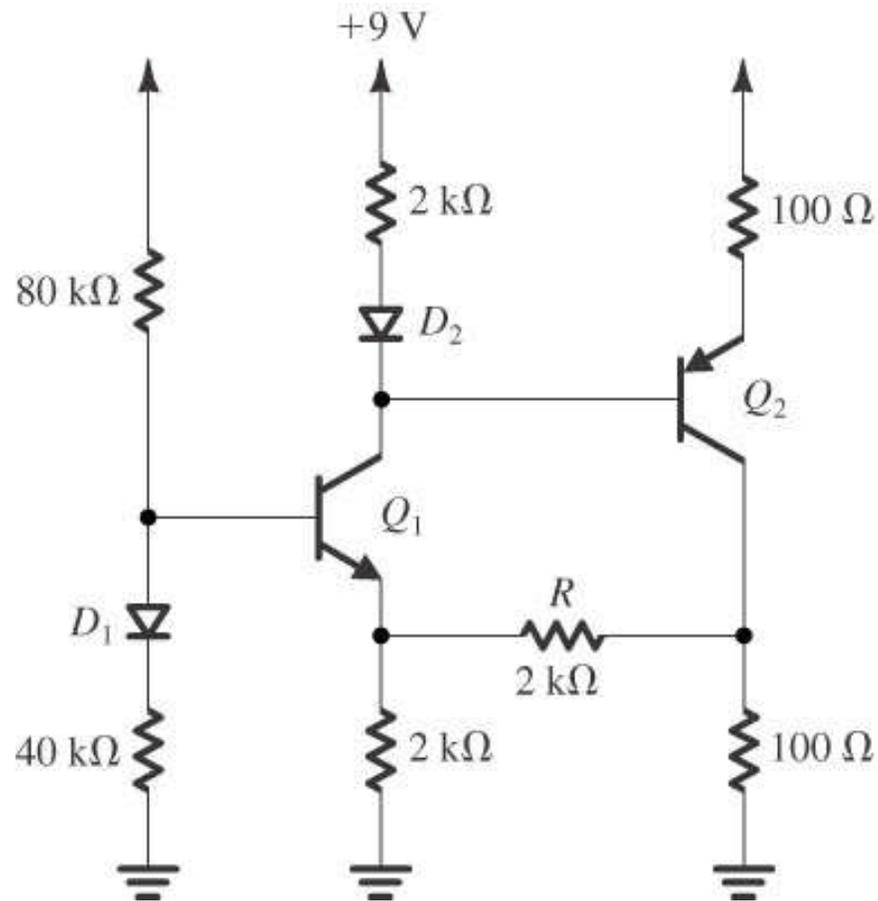
Figure P5.79



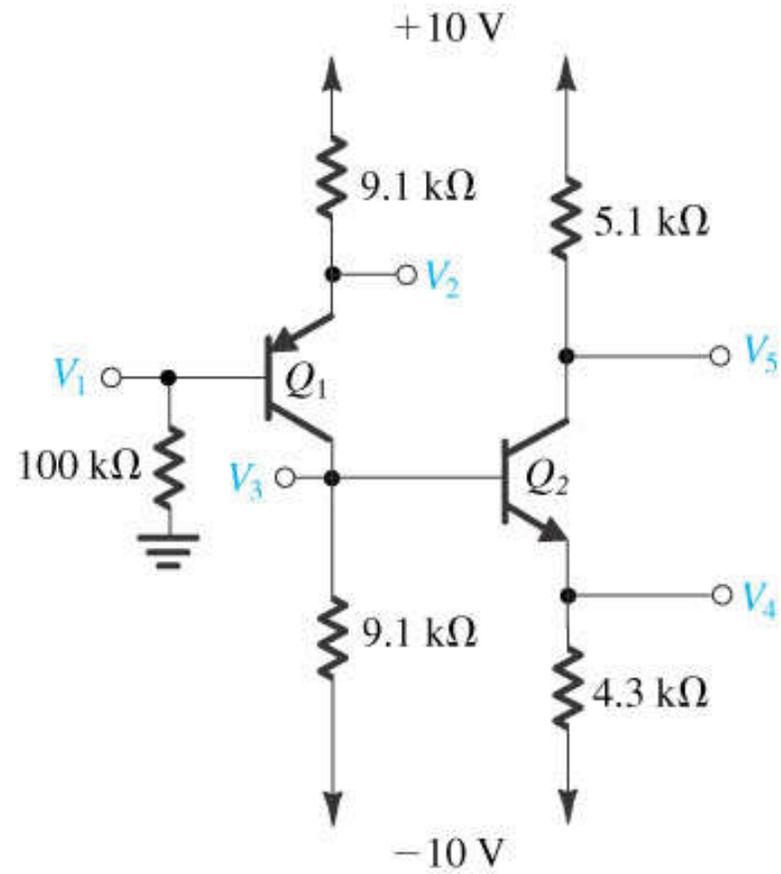
**Figure P5.81**



**Figure P5.82**



**Figure P5.83**



**Figure P5.84**

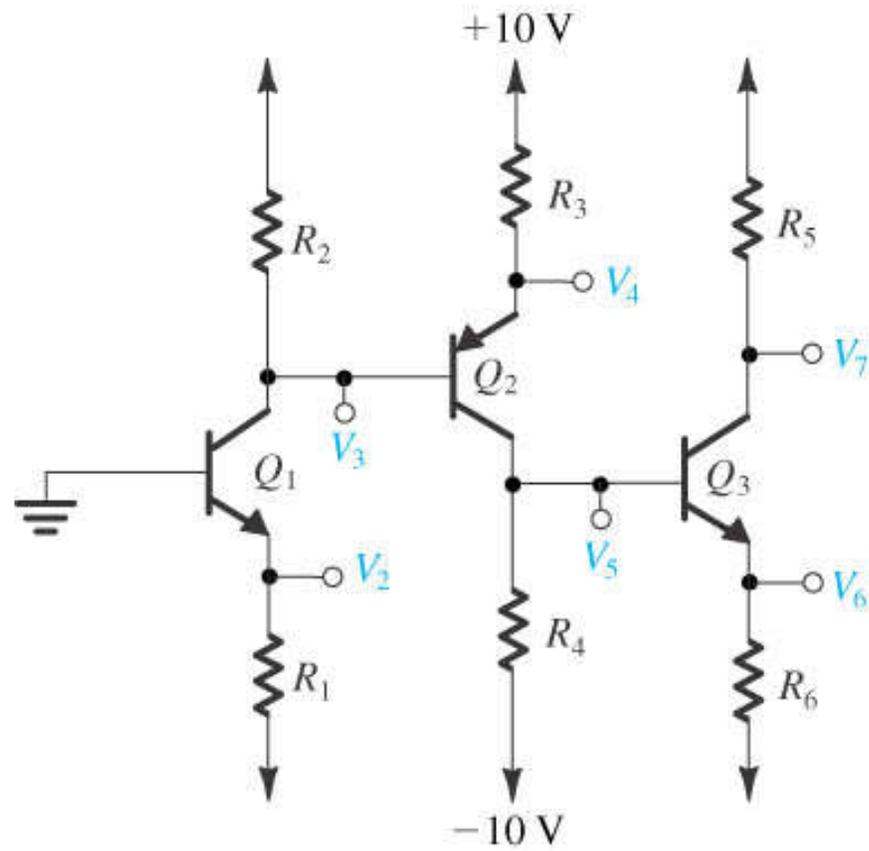
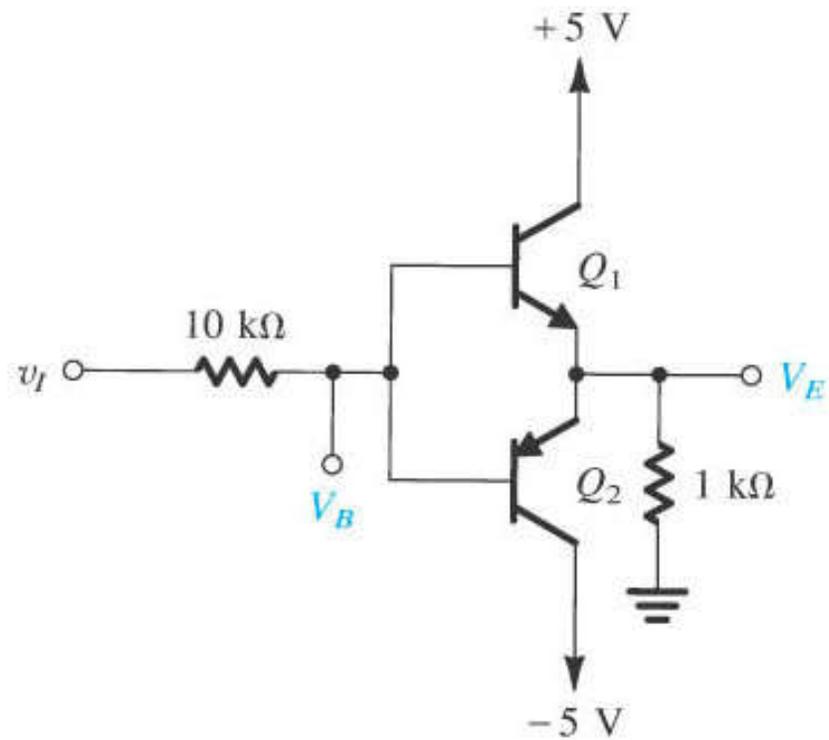


Figure P5.85



**Figure P5.86**

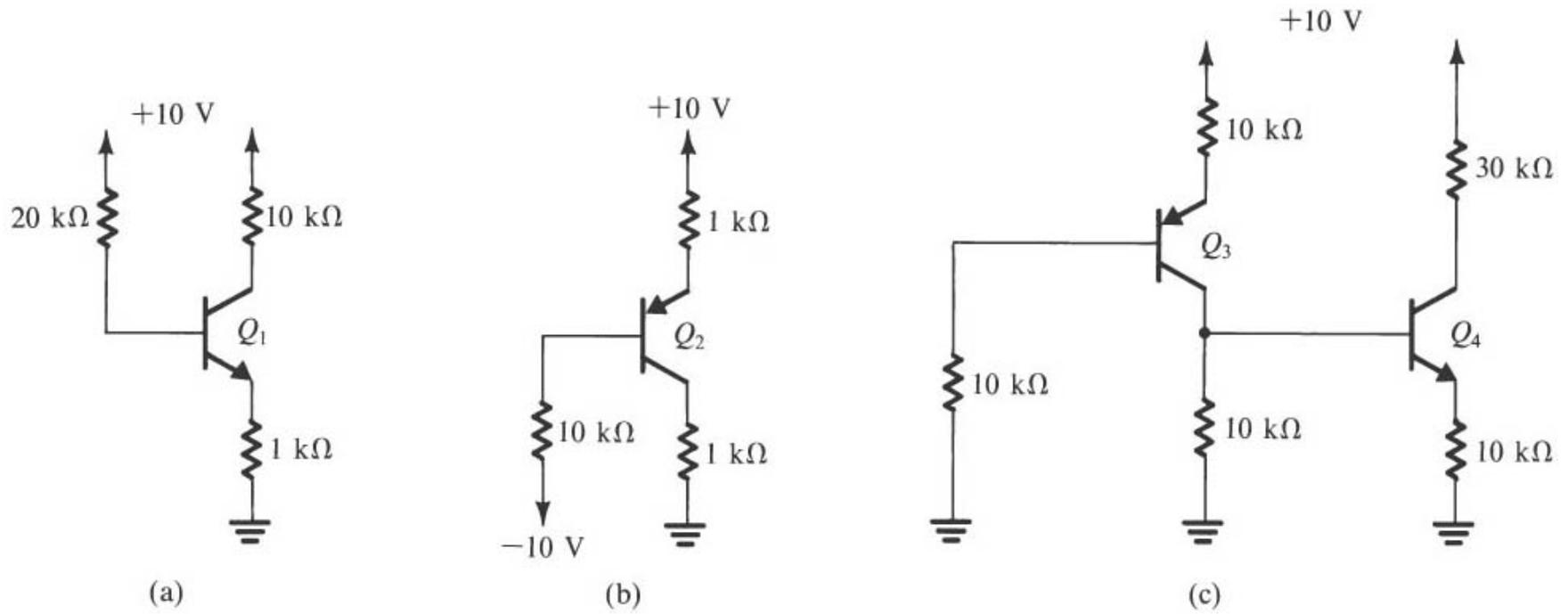
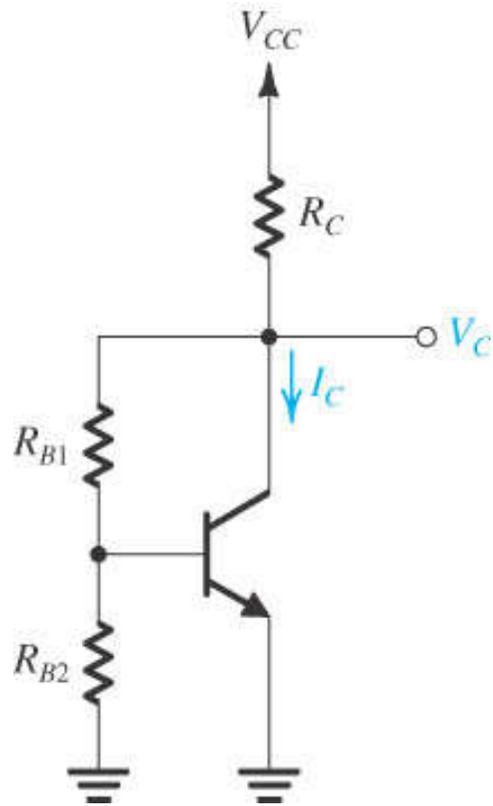
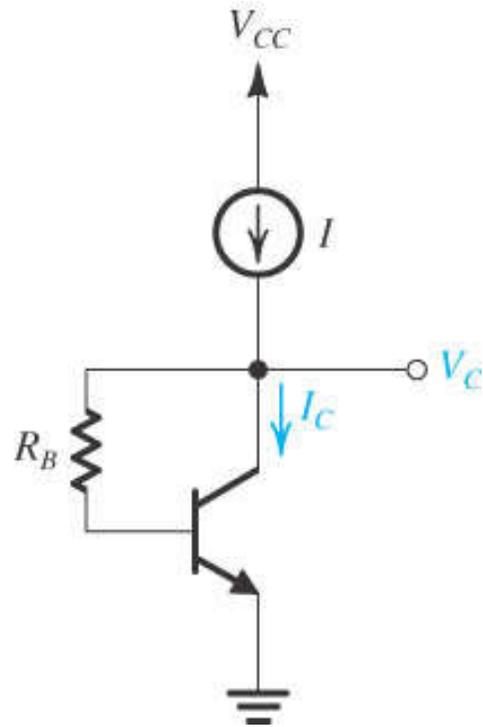


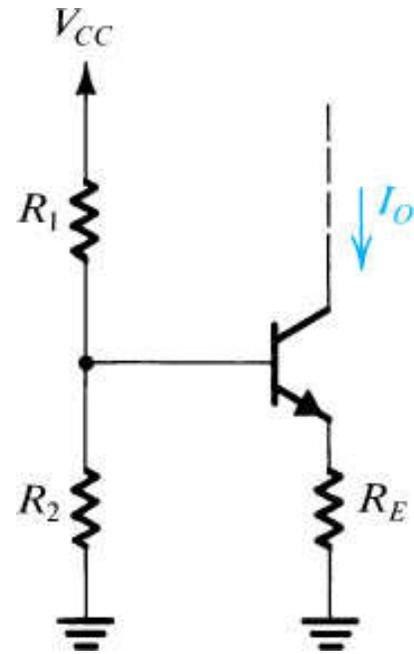
Figure P5.87



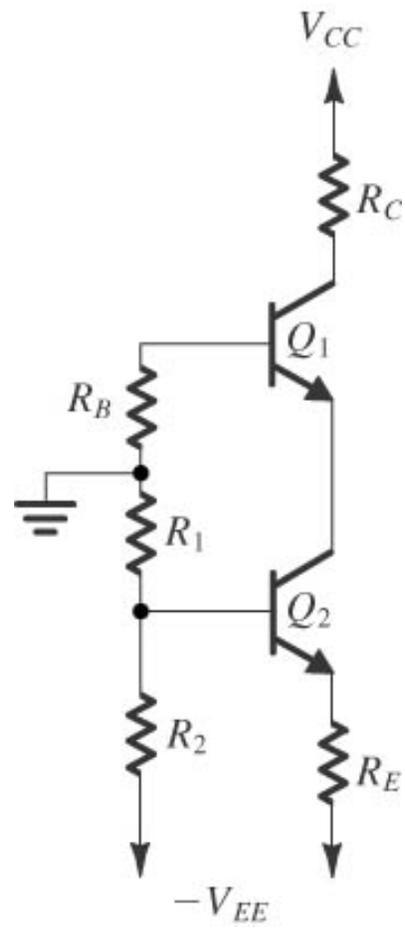
**Figure P5.96**



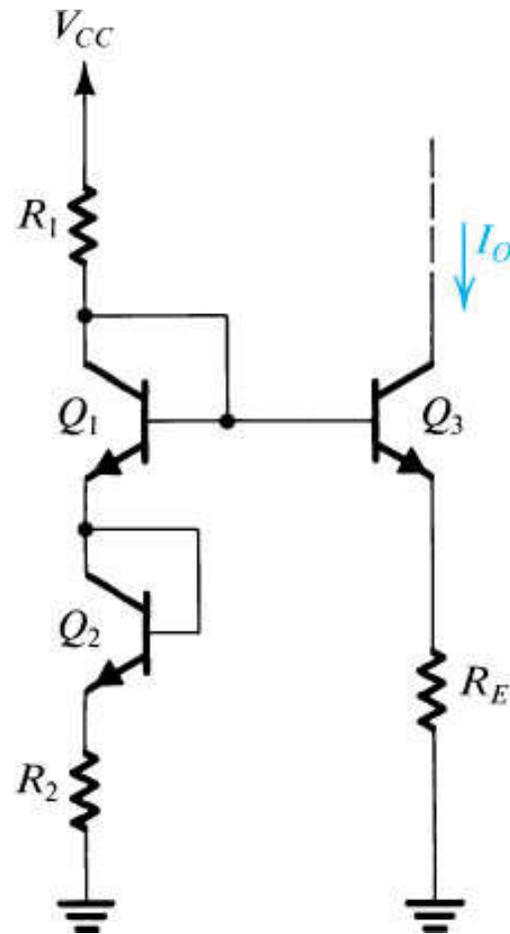
**Figure P5.97**



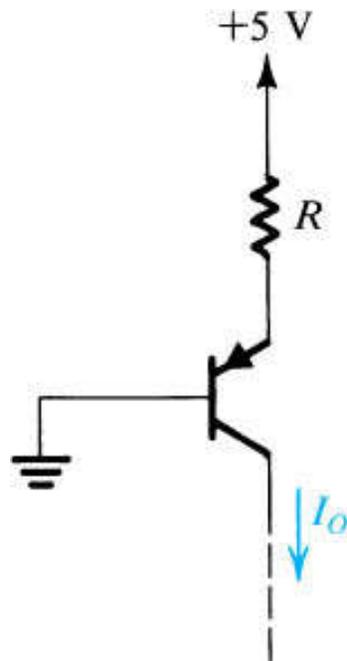
**Figure P5.98**



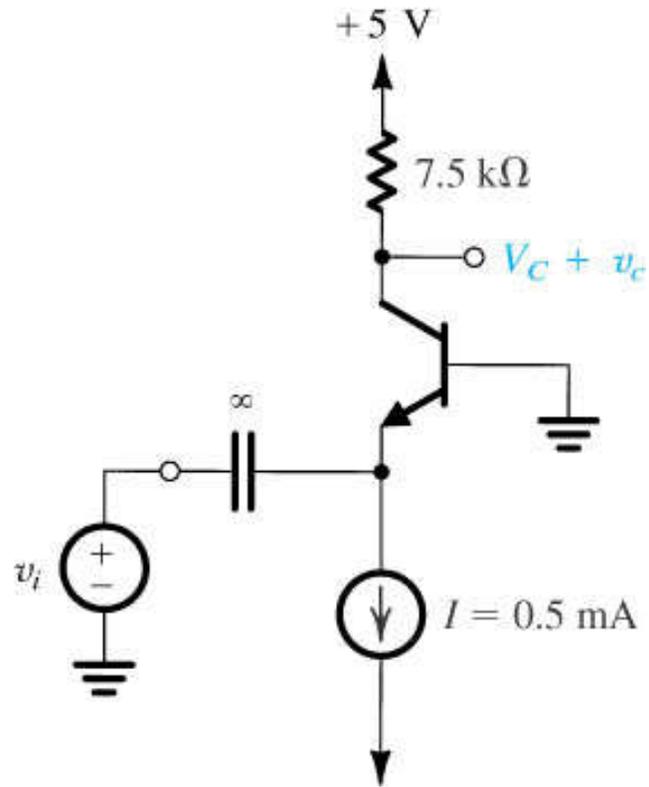
**Figure P5.99**



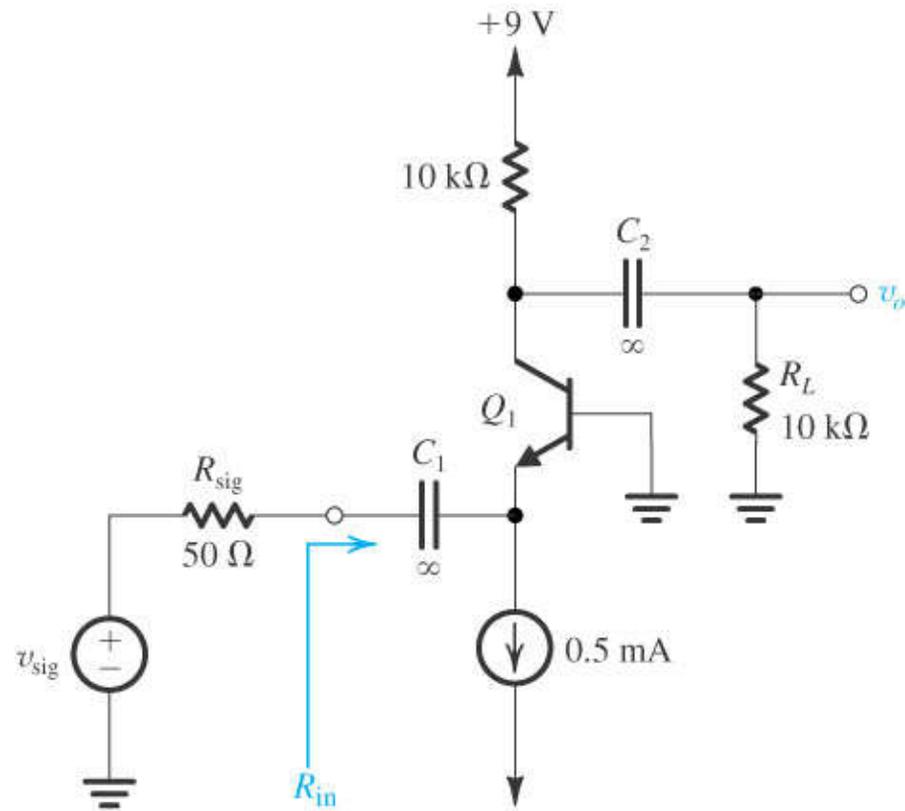
**Figure P5.100**



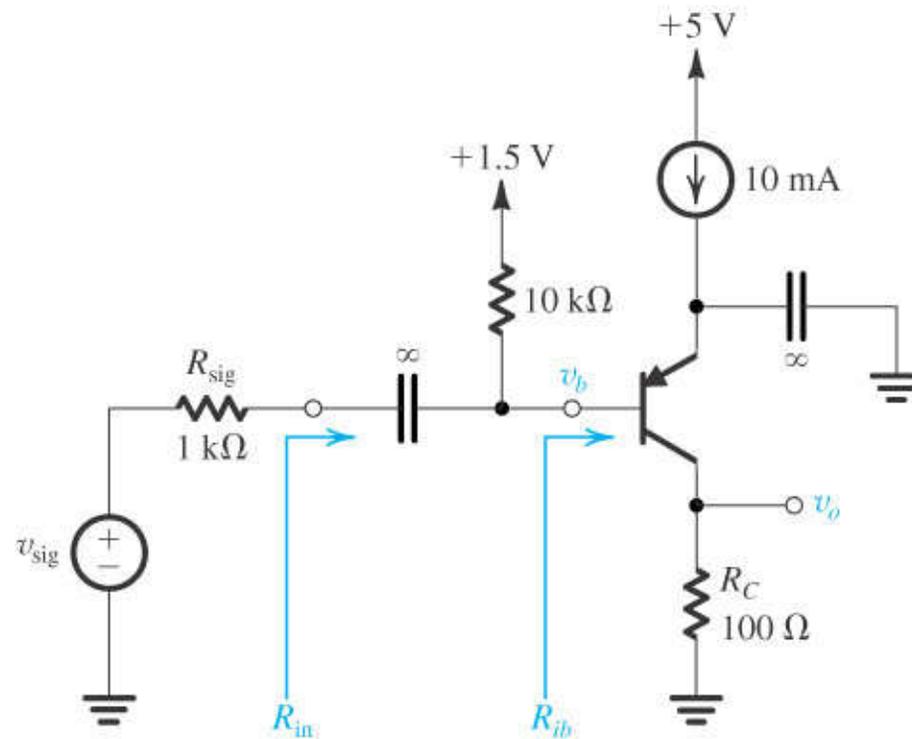
**Figure P5.101**



**Figure P5.112**



**Figure P5.115**



**Figure P5.116**

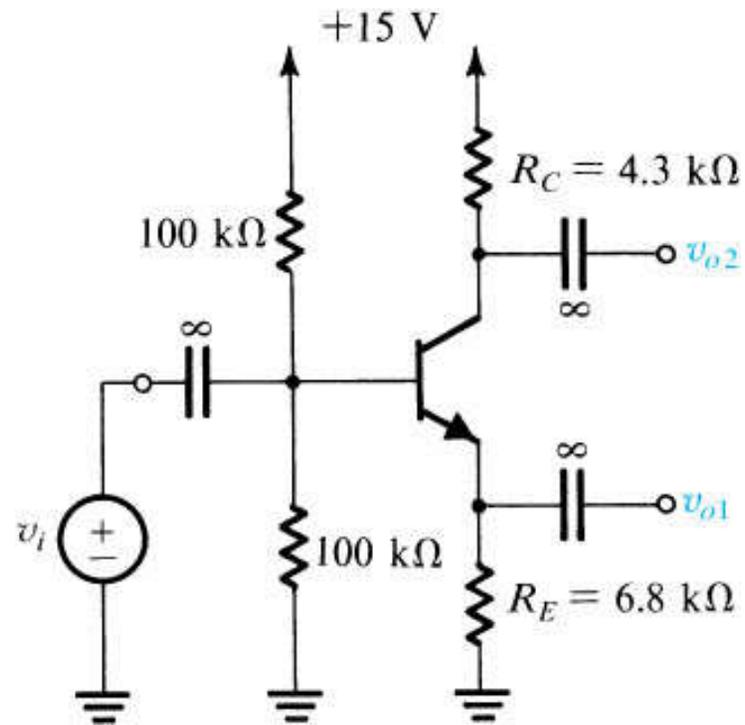
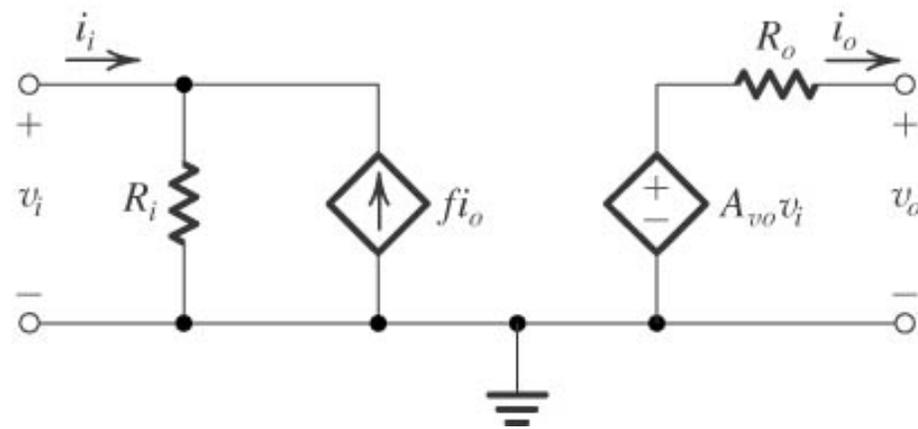


Figure P5.124



**Figure P5.126**

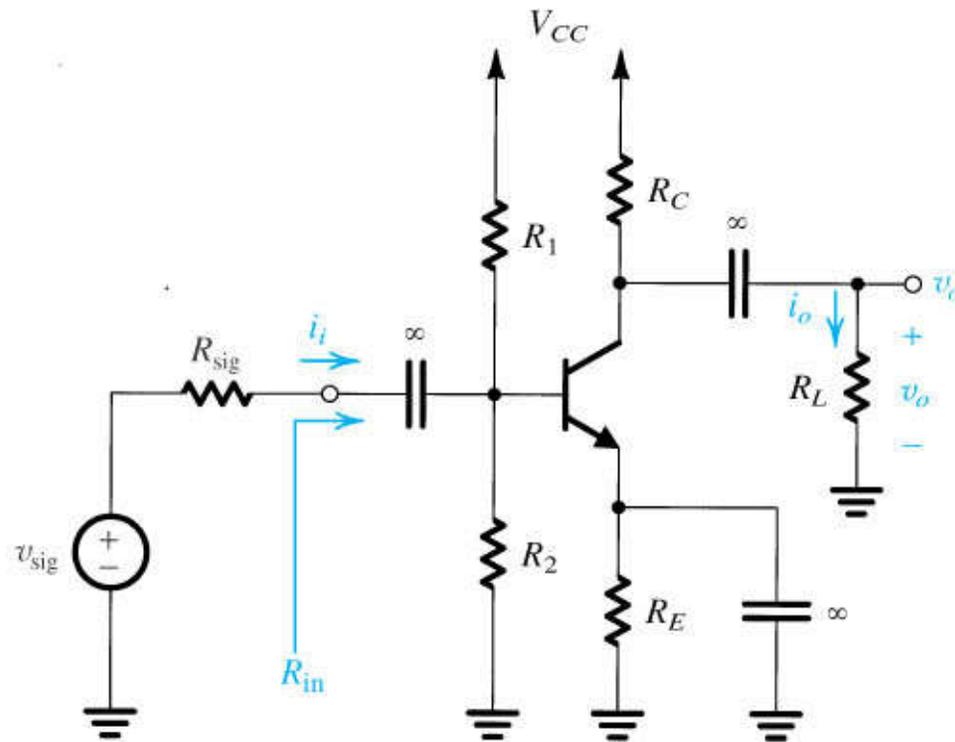
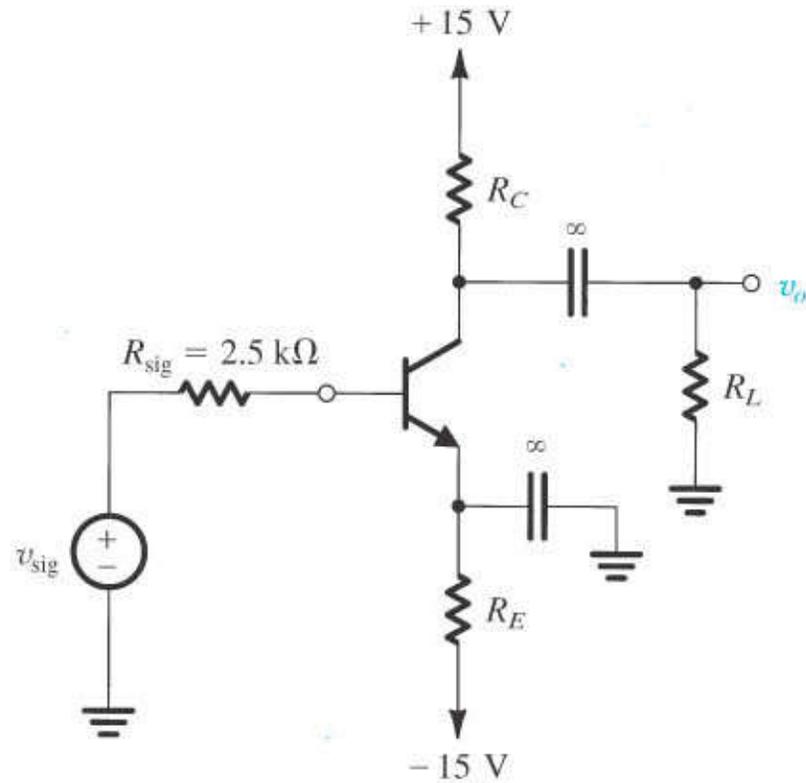


Figure P5.130



**Figure P5.134**

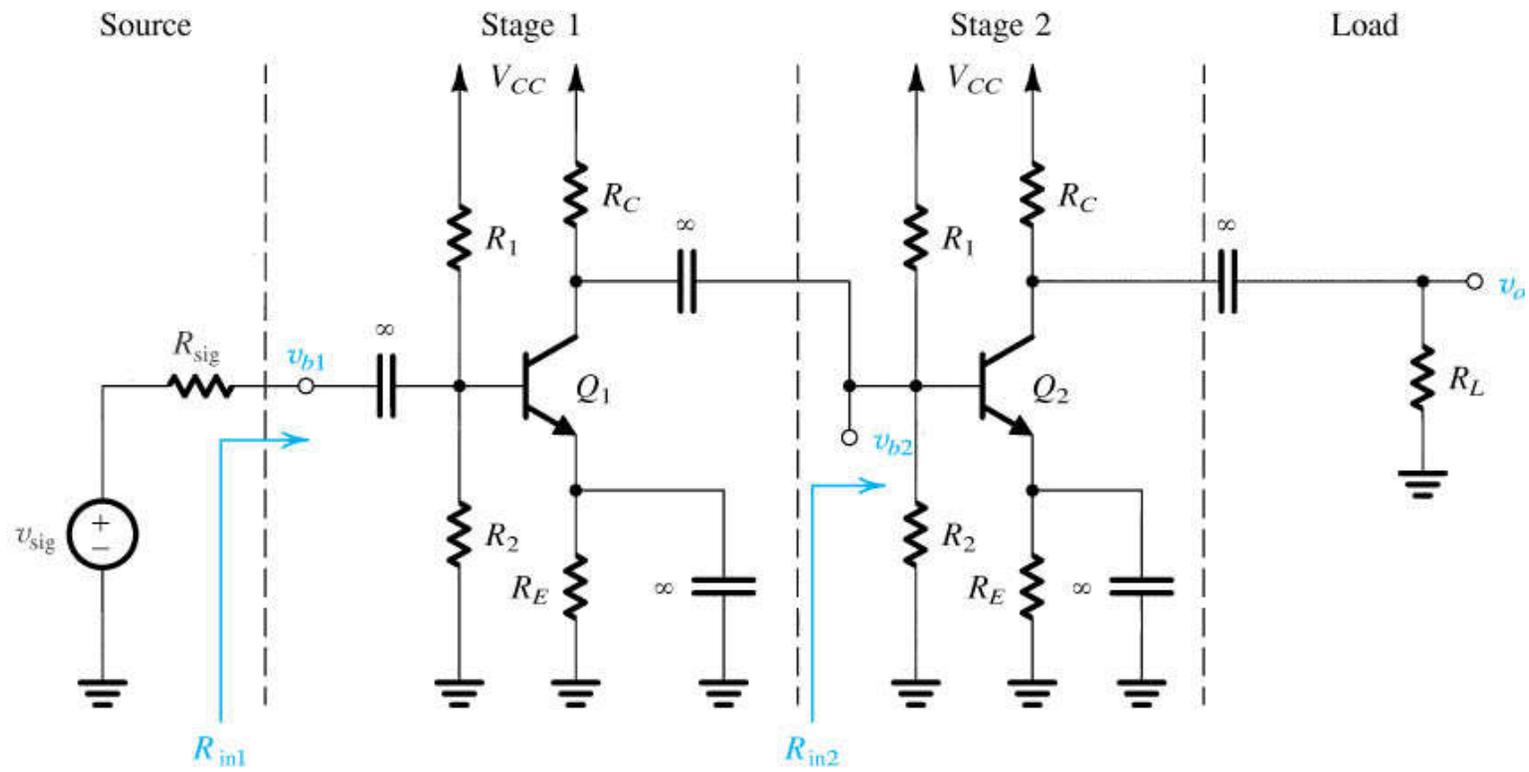


Figure P5.135

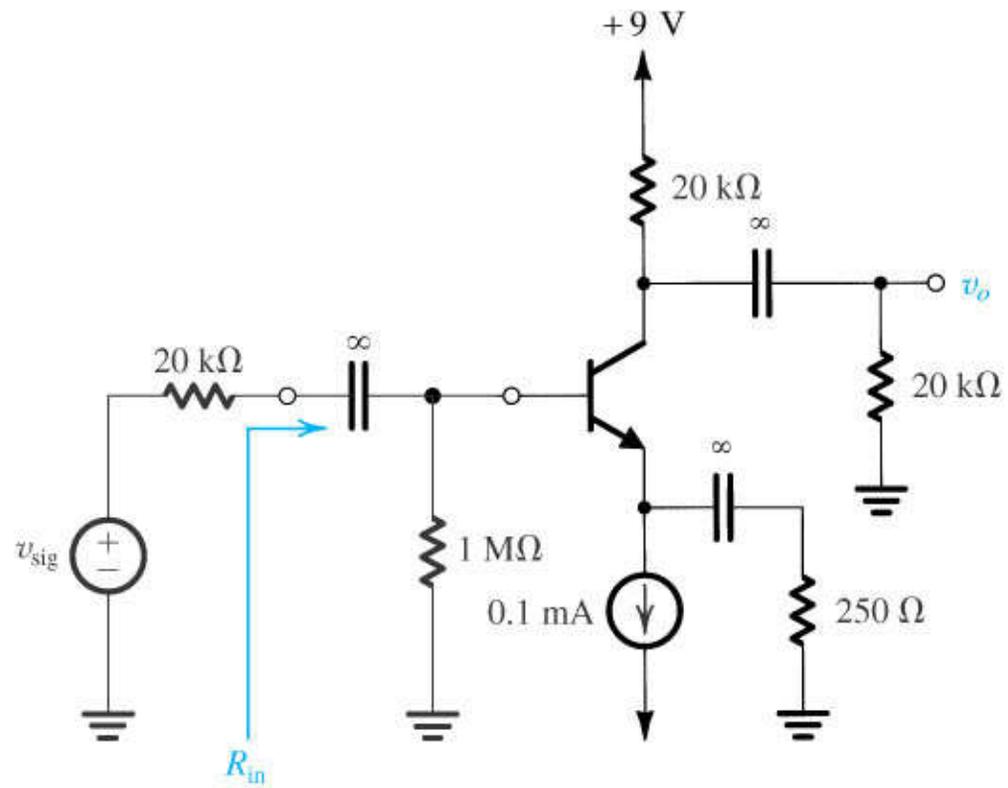
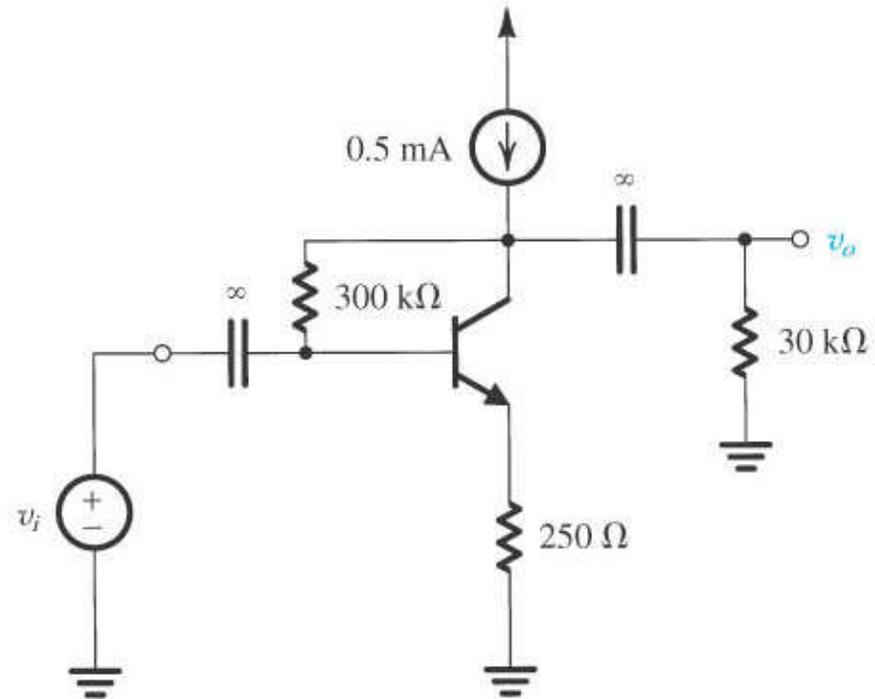


Figure P5.136



**Figure P5.137**

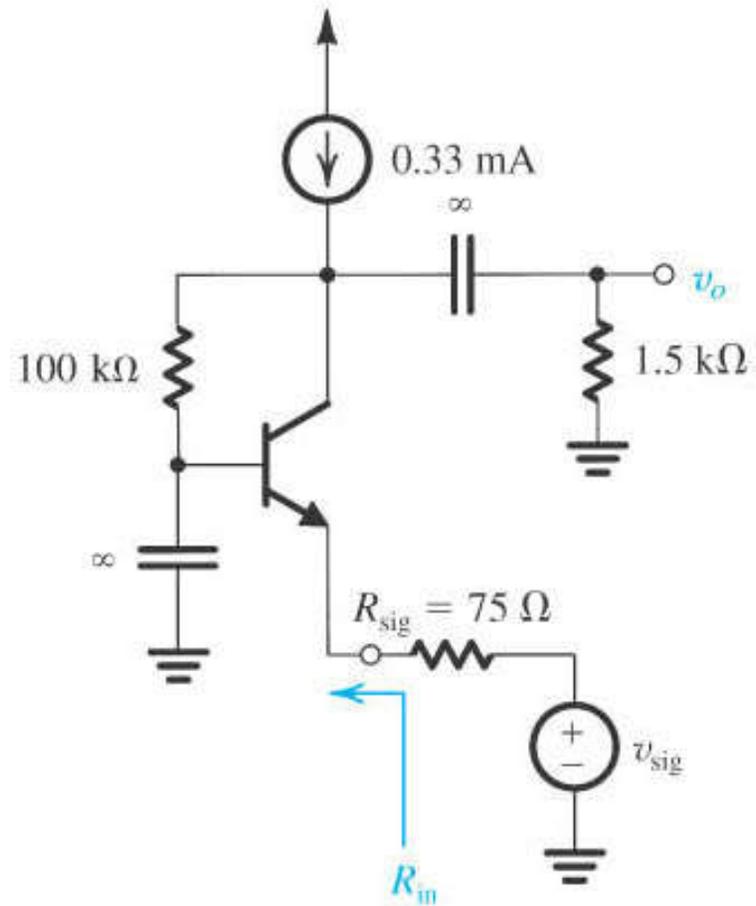


Figure P5.141

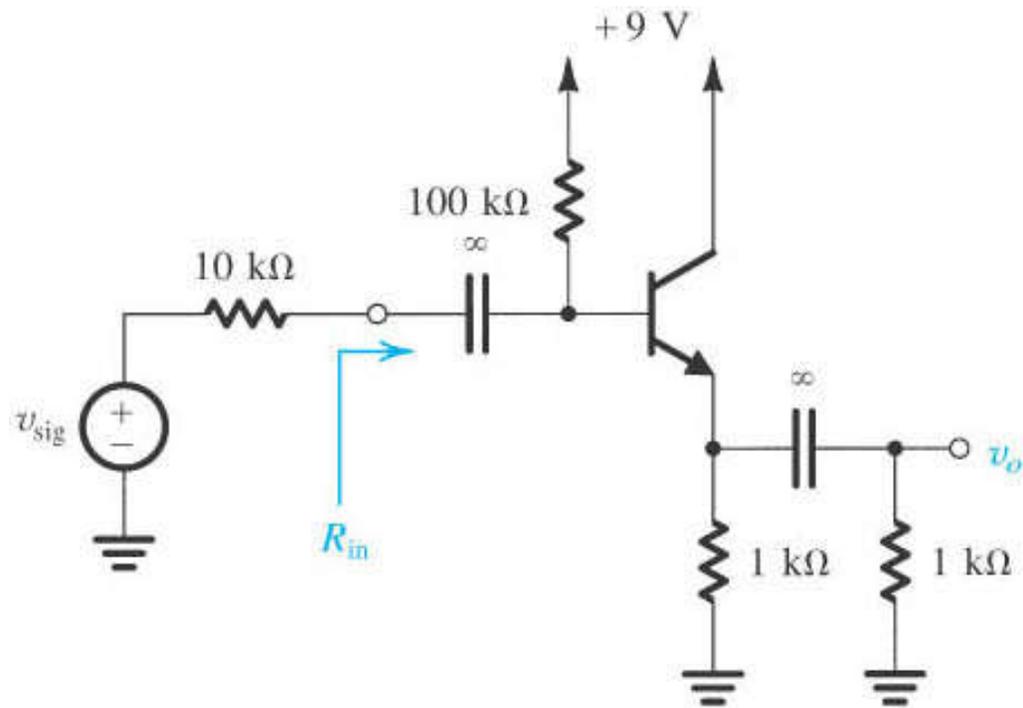


Figure P5.143

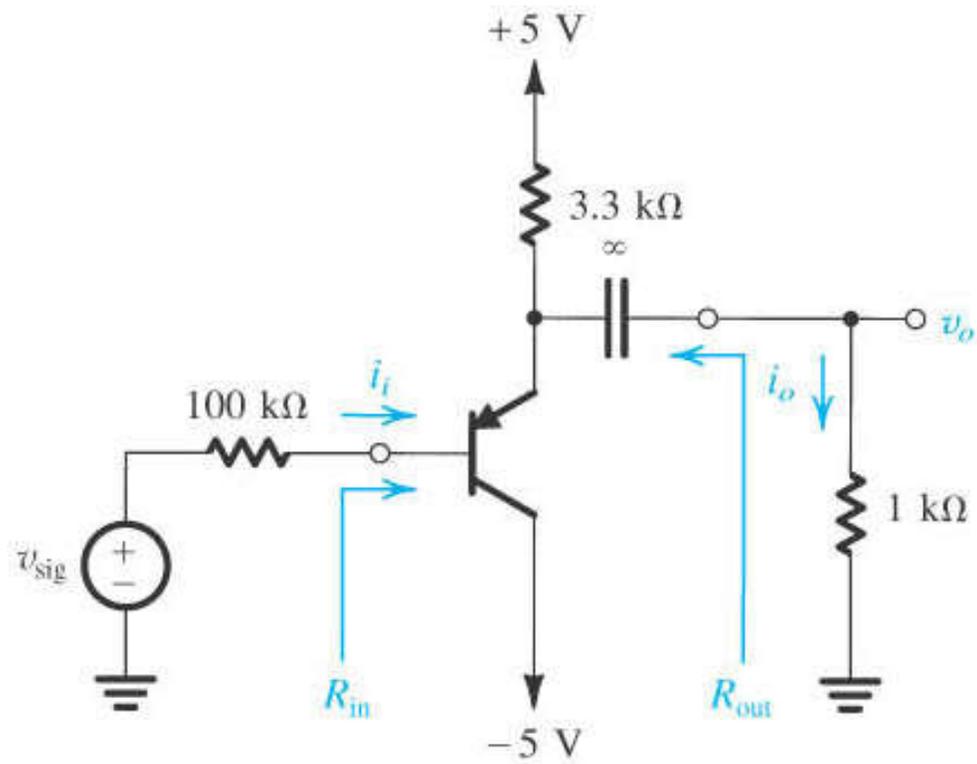


Figure P5.144

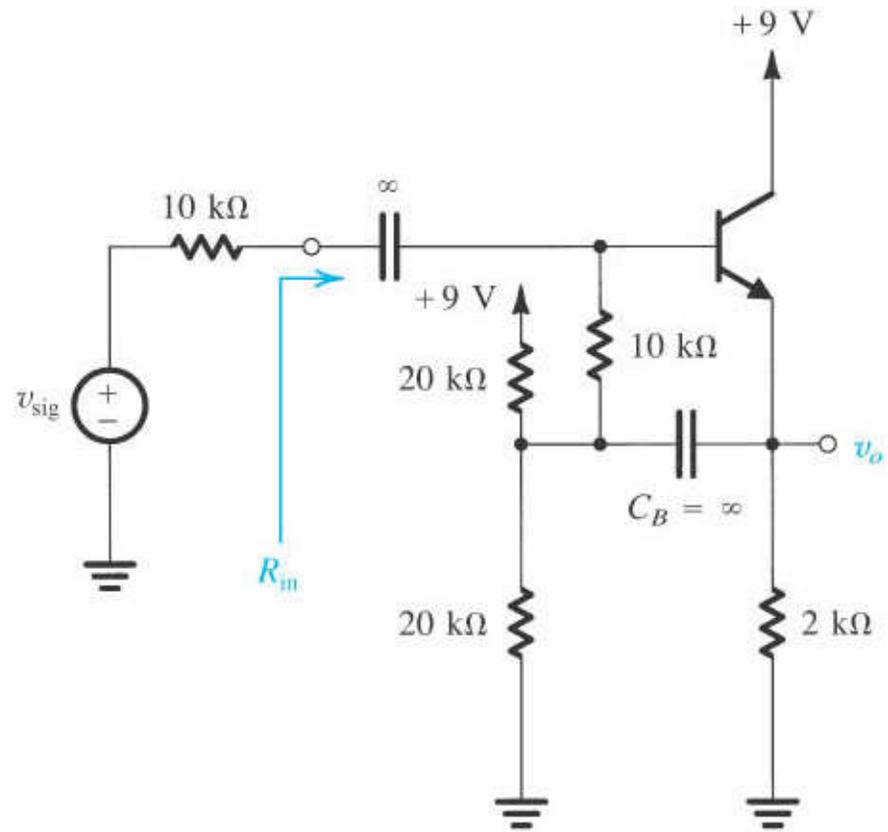


Figure P5.147

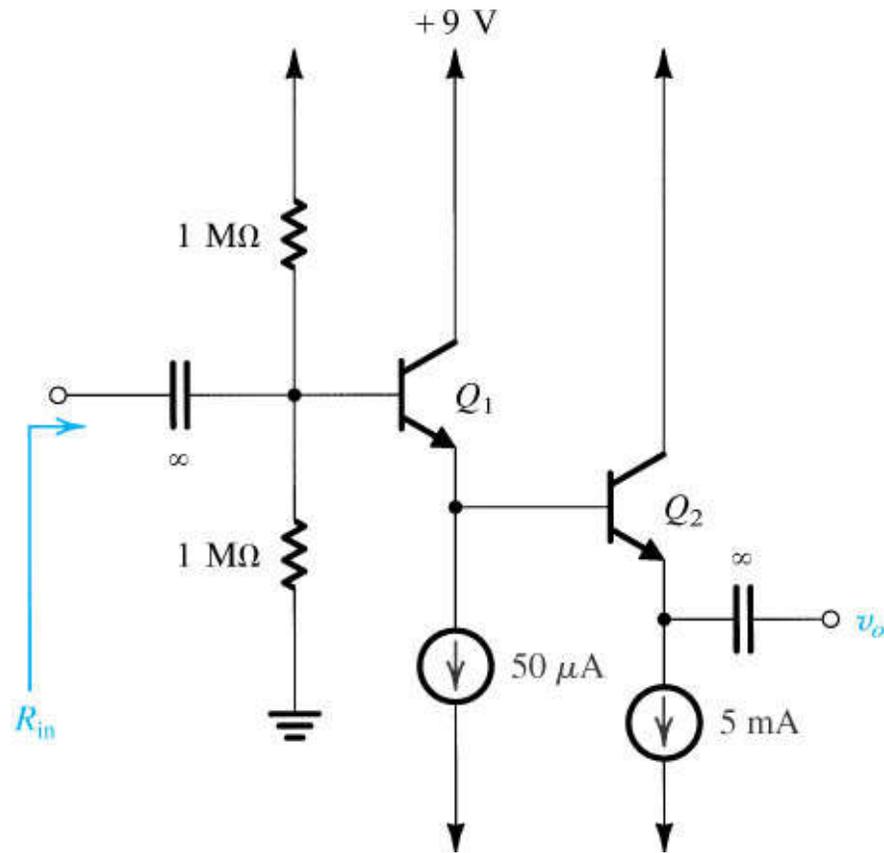
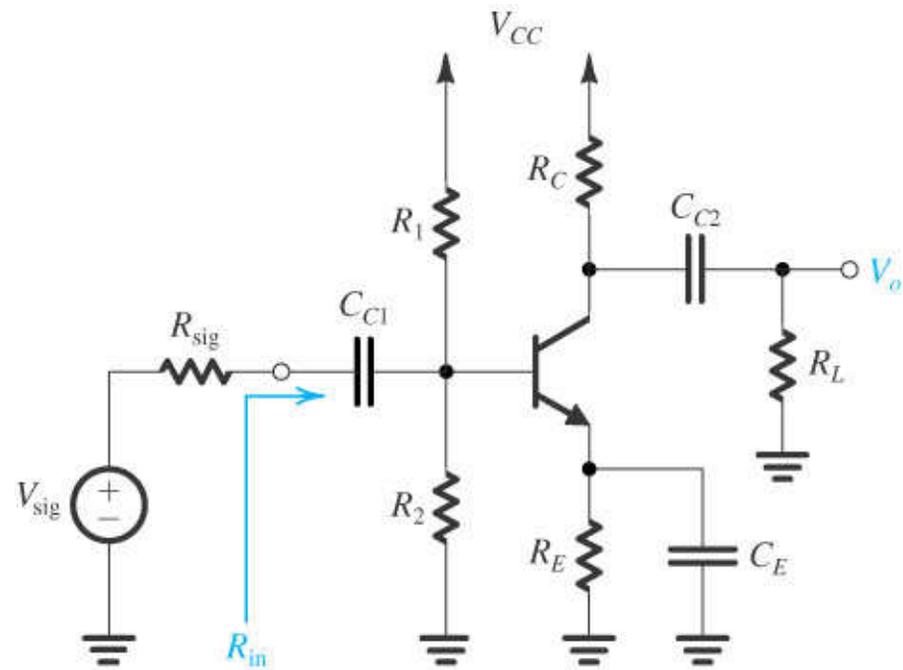
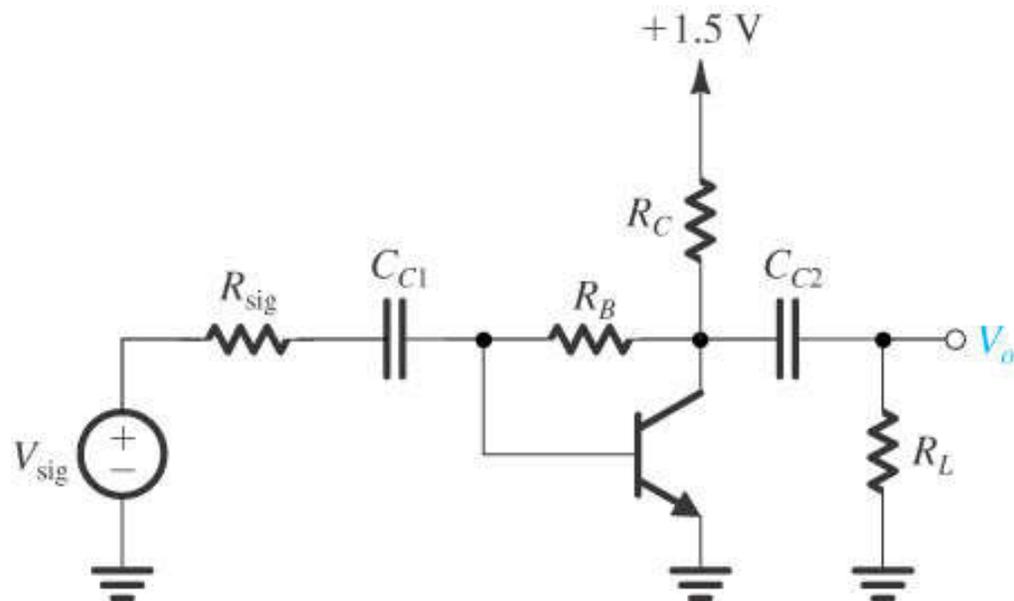


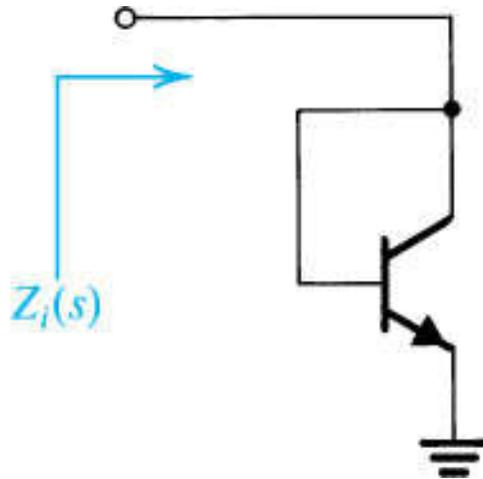
Figure P5.148



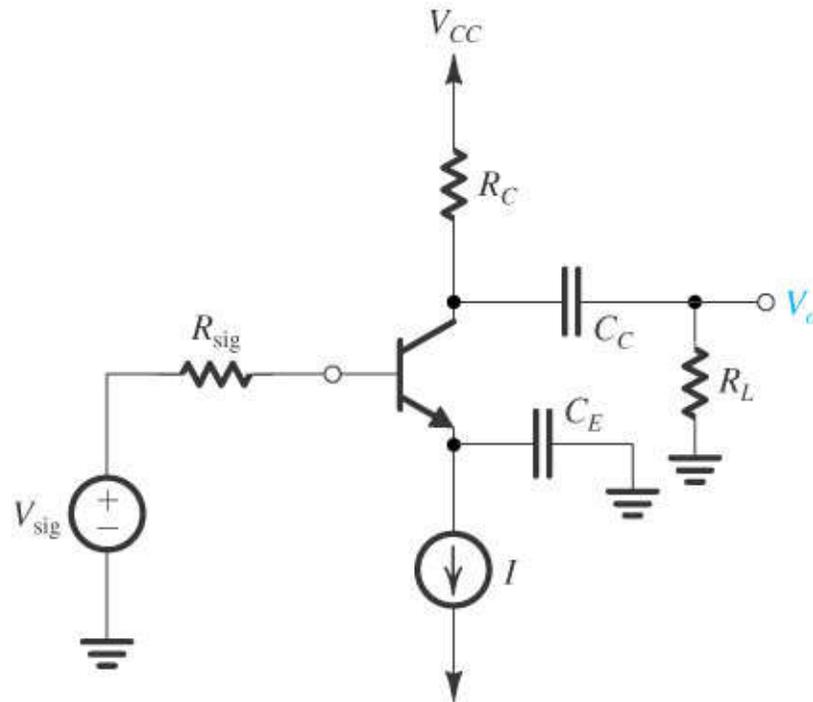
**Figure P5.159**



**Figure P5.161**



**Figure P5.162**



**Figure P5.166**

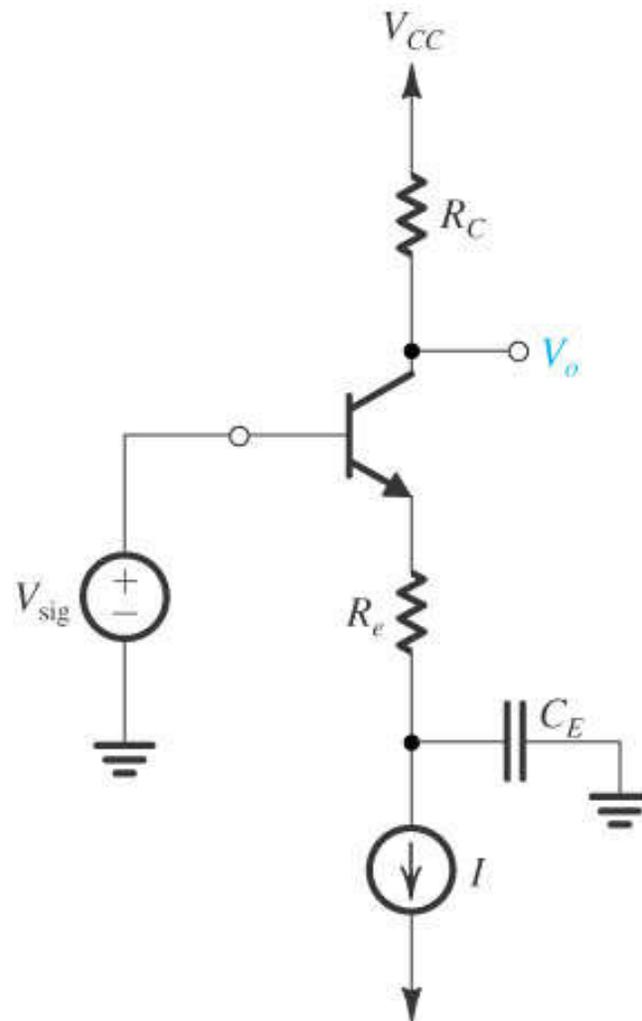


Figure P5.167

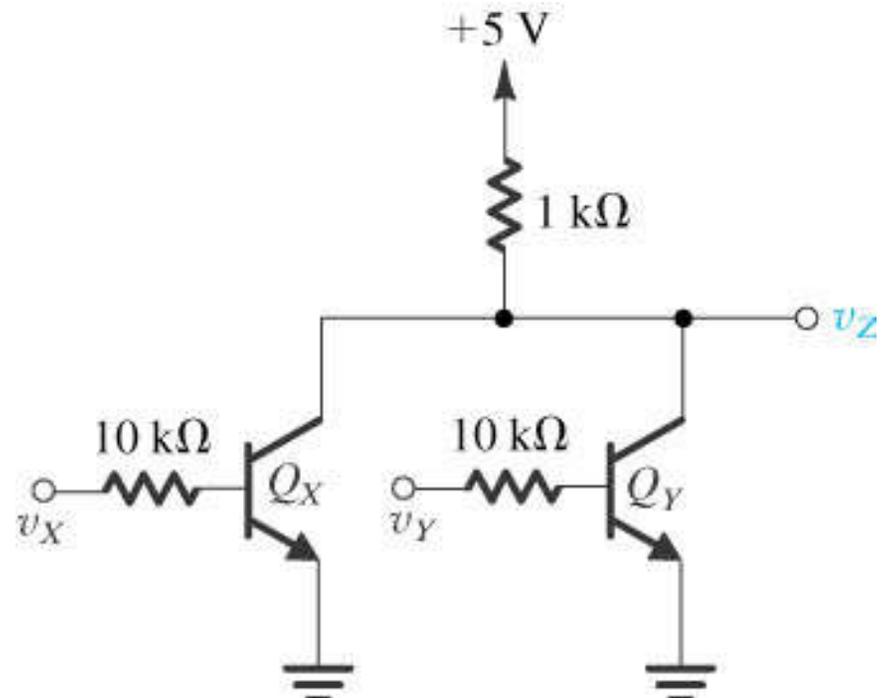


Figure P5.171